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NUSC Technical Report 4635

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**Long-Range Propagation Loss Measurements of
Project TRANSLANT I in the Atlantic Ocean
East of Bermuda**

[Unclassified Title]

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12 June 1974

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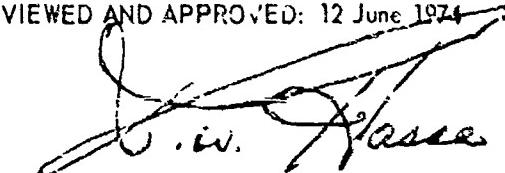
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PREFACE

This work was performed under NUSC Project A-650-15, "Long-Range Acoustic Transmission Experiments for Surveillance System Development" (U), Principal Investigator, R. W. Hasse, Code TA; and Subproject and Task No. R2408, Program Manager, Dr. R. D. Gaul, Code 102-OS, Office of Naval Research.

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REVIEWED AND APPROVED: 12 June 1974



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and topographic features, such as seamounts and the Mid-Atlantic Ridge. Besides providing a data base against which to check acoustic models for the subject area and climatic conditions, the data were to be compared with similar data taken in January and February 1971.

Considering all ranges and frequencies up to 200 Hz, propagation losses from 60-ft sources averaged about 6 dB greater than for 500-ft sources for hydrophones at depths of 10,900 and 4,650 ft. A similar difference between propagation losses for shallow as opposed to deep sources was found at 25 Hz for receivers at depths of 14,000 and 14,706 ft. For 50, 100, and 200 Hz, losses from both shallow and deep sources were about the same to the deep receivers. For sources detonated at the Mid-Atlantic Ridge (about 1300 nmi), the lowest loss was for the hydrophone suspended in the deep sound channel at 4,650 ft. Reduced propagation losses were also evident for sources detonated in the vicinity of Rockaway Seamount. The two deep hydrophones located at 14,000 and 14,708 ft indicated strong convergence gains for some frequencies for ranges as great as 900 nmi with losses somewhat greater for the deeper hydrophones.

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TR 4635

TABLE OF CONTENTS

	Page
LIST OF ILLUSTRATIONS	III
LIST OF TABLES	III
TECHNICAL NOTE	v
INTRODUCTION	1
DESCRIPTION OF EXPERIMENT	1
DATA ACQUISITION AND REDUCTION	3
Source Levels	3
System Calibrations	3
Data Processing System	4
Range Determination	4
FORMAT AND PRESENTATION OF THE DATA	4
Environmental Data	4
Propagation Loss	6
Ambient Noise Spectrum Levels	6
Signal-to-Noise Ratios	6
DISCUSSION OF EXPERIMENTAL RESULTS	7
General Comments on Environment	7
Ambient Noise Spectrum Levels	7
Propagation Loss and Signal-to-Noise Ratios for 500-ft Sources	11
Propagation Loss and Signal-to-Noise Ratios for 60-ft Sources	12
Comparison of 60- and 500-ft Propagation Loss Results	15
Propagation Loss for Track BCDE	17
COMPARISON OF TRANSLANT I AND PROJECT ATOE/NA MEASUREMENTS	17
CONCLUSIONS	23
REFERENCES	25

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TABLE OF CONTENTS (Cont'd)

	Page
APPENDIX A — TRANSLANT I BOTTOM TOPOGRAPHY PLOTS	A-1
APPENDIX B — TRANSLANT I SOUND VELOCITY PROFILES	B-1
APPENDIX C — TRANSLANT I MEASURED PROPAGATION LOSS	C-1
APPENDIX D — TRANSLANT I BACKGROUND NOISE SPECTRUM LEVELS . .	D-1
APPENDIX E — TRANSLANT I SIGNAL-TO-NOISE LEVELS	E-1
APPENDIX F — TRANSLANT I AND ATOE PROPAGATION LOSS COMPARISON.	F-1

UNCLASSIFIED

TR 4635

LIST OF ILLUSTRATIONS

Figure		Page
1	Location of Hydrophones for TRANSLANT I	2
2	Track for TRANSLANT I Measurements	2
3	Deep Sound Channel Axis and Critical Depth for TRANSLANT I Measurements	8
4	Comparison of Noise Spectrum Levels at TRANSLANT I Hydrophones (25, 50, 100 Hz)	9
5	Comparison of Noise Spectrum Levels at TRANSLANT I Hydrophones (200, 400 Hz)	10
6	TRANSLANT I Propagation Loss Composite	13
7	Propagation Loss Comparison at BB and E1 Hydrophones (25, 50, 100 Hz)	16
8	Propagation Loss at E1 Hydrophone (25, 50, 100 Hz) for a Source Depth of 500 ft.	18
9	Propagation Loss at E1 Hydrophone (200, 400 Hz) for a Source Depth of 500 ft	19
10	Propagation Loss at E1 Hydrophone (25, 50, 100 Hz) for a Source Depth of 60 ft	20
11	Propagation Loss at E1 Hydrophone (200, 400 Hz) for a Source Depth of 60 ft	21

LIST OF TABLES

Table		Page
1	Effective 1/3-Octave-Band Source Levels for TRANSLANT I	3
2	Surface Conditions From Log of USNS SANDS (T-AGOR-6)	5

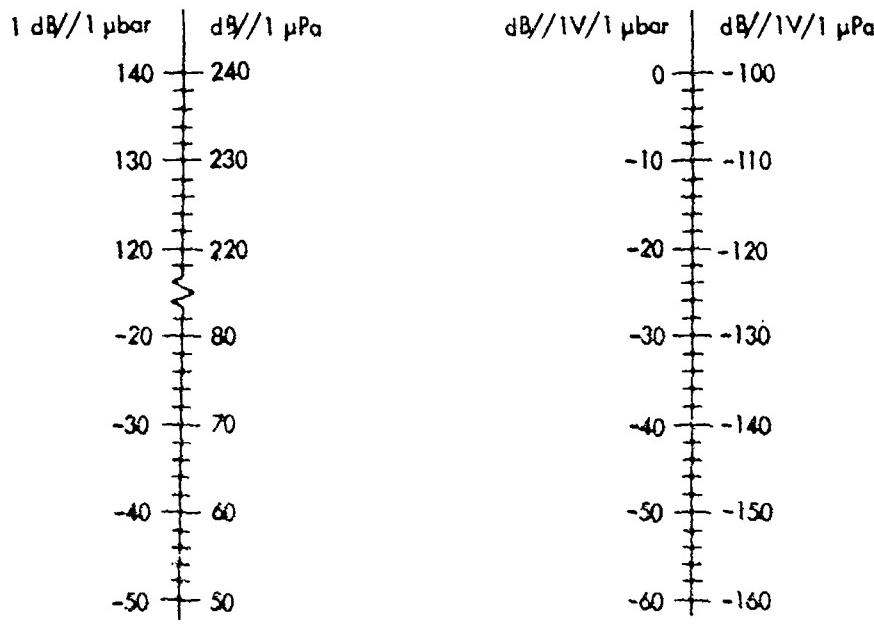
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TECHNICAL NOTE

The micropascal (μPa), one micronewton per square meter ($1\mu\text{N}/\text{m}^2$), has replaced the microbar (μbar), one dyne per square centimeter ($1\text{ dyne}/\text{cm}^2$), as the standard reference pressure used to express acoustic levels. One μPa is equal to $10^{-5}\mu\text{bar}$. The effect of this change in reference is a translation of 100 dB. For sonar parameters expressed in terms of $\text{dB}/1\mu\text{bar}$ (e.g., source level* and background noise), the level increases by 100 dB when expressed in $\text{dB}/1\mu\text{Pa}$, as shown by scale a. For sonar parameters expressed only in dB, which represent a difference of two acoustic levels (e.g., target strength and propagation loss), the value remains unchanged. The receiving sensitivity, which is expressed in $\text{dB}/1\text{V}/1\mu\text{bar}$, decreases by 100 dB when expressed in $\text{dB}/1\text{V}/1\mu\text{Pa}$, as shown in scale b.[†]



$$\text{a. } \text{dB}/1 \mu\text{Pa} = \text{dB}/1 \mu\text{bar} + 100 \text{ dB}$$

$$\text{b. } \text{dB}/1 \text{V}/1 \mu\text{Pa} = \text{dB}/1 \text{V}/1 \mu\text{bar} - 100 \text{ dB}$$

*In this report, source level is expressed in terms of $\text{dB}/(1\mu\text{Pa})^2$. See at 1 yd. Note that the source level will be 0.8 of a decibel lower for a reference of 1 m.

†Receiving sensitivity is a voltage reading at some specified location in the system which results when a standard pressure level is present at the transducer face. This standard reference pressure has been 0 $\text{dB}/1\mu\text{bar}$ at the transducer face. The new reference, 0 $\text{dB}/1\mu\text{Pa}$, represents a unit pressure level that has been decreased by a factor of 10^5 or 100 dB. Consequently, this 100-dB reduction in pressure level results in a 100-dB drop in the receiving sensitivity value.

LONG-RANGE PROPAGATION LOSS MEASUREMENTS OF
PROJECT TRANSLANT I IN THE ATLANTIC OCEAN
EAST OF BERMUDA

INTRODUCTION

(U) During 26 September to 14 October 1971, long-range underwater acoustic propagation loss measurements were made between Bermuda and the Mid-Atlantic Ridge. These measurements were part of project WESTLANT, which has been redesignated TRANSLANT I. Explosives detonated at 60 and 500 ft were used as sound sources. The signals were received at five widely separated hydrophones in the Bermuda area and recorded on magnetic tape at the Naval Underwater Systems Center's Tudor Hill Laboratory, Bermuda. The measurements were intended to (1) study the dependence of propagation loss and signal-to-noise ratios (SNR) on range, frequency, source depth, and receiver depth, (2) show the effects of seamounts and the Mid-Atlantic Ridge on propagation loss, (3) provide comparisons with similar experiments on a seasonal basis, and (4) provide measurements for the development and validation of acoustic models for this type of acoustic environment.

(U) Environmental information along the several tracks was obtained by USNS SANDS (T-AGOR-6), the source ship, in the form of sound velocity profiles, expendable bathythermograms (XBT's), and water depth recordings, as well as standard meteorological data.

DESCRIPTION OF THE EXPERIMENT

(U) Figure 1 gives the location of the Broadband (BB), Trident Vertical (TVA-1), and Coherence (C6) receivers used in this experiment. Two additional hydrophones — Easy 1 (E1) and Easy 40 (E40) of the Easy II Array were also used. The source ship SANDS traversed the track as shown in figure 2 starting within 2 nmi of the Broadband Array and proceeding on an easterly great circle route toward the Mid-Atlantic Ridge. At point "B" about 612 nmi from the start, a northerly diversion from the great circle course was made. This course change (designated in the track plot as BCDE) was made so that the source ship would traverse the area of the Rockaway Seamount. At point "E," SANDS again continued on the original great circle route to the Mid-Atlantic Ridge about 1400 nmi from the start of the track. Excursions were then made back and forth over the ridge as shown in figure 2.

(U) SANDS proceeded on the track at 10 knots and detonated explosive sound sources on the following schedule: Starting on the hour and every 7 min thereafter to 49 min, a 3-lb TNT block was detonated at 500 ft; 2 min after each 500-ft shot, a 3-lb TNT block was detonated at 60 ft. In addition, thermal observations of the water column in the form of 2500-ft XBT's were taken every 8 hr. Deep sound velocity profiles (3600 m) were scheduled daily and were taken when weather and schedule permitted. Primary navigation was provided by the satellite navigation system.

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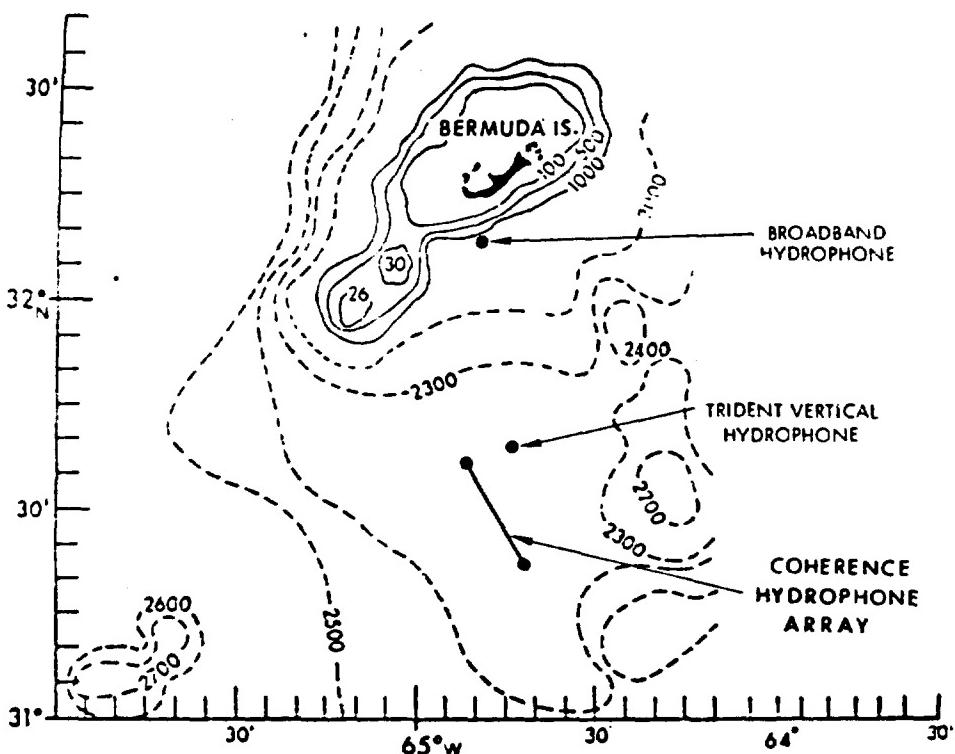


Figure 1. (U) Location of Hydrophones for TRANSLANT I (U)

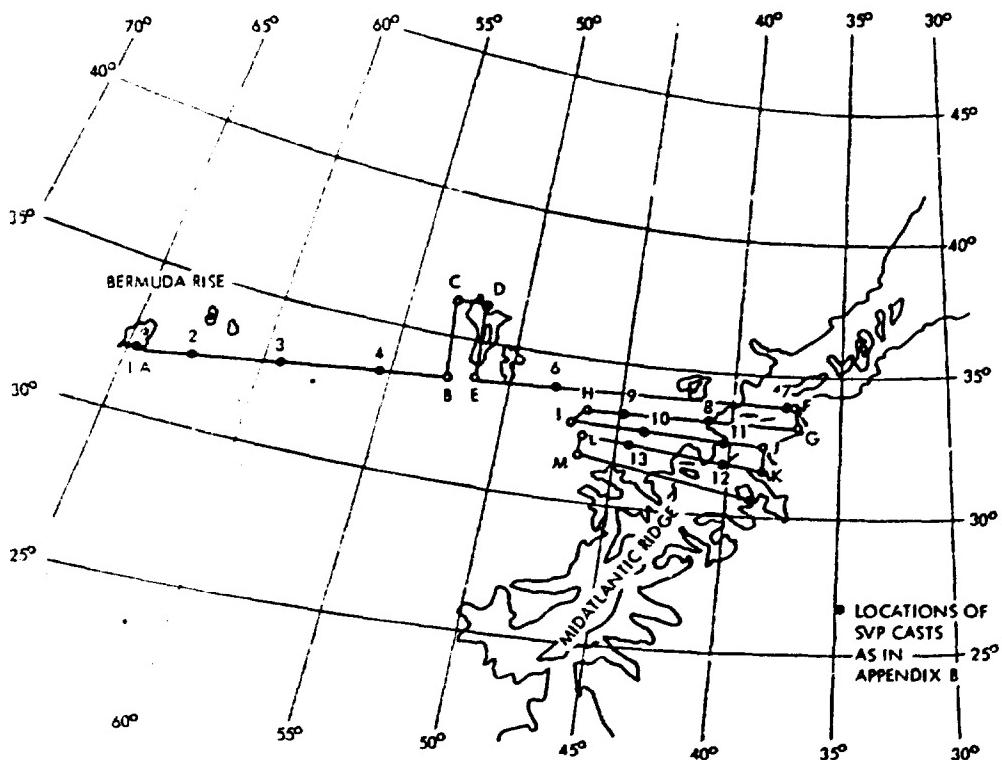


Figure 2. (U) Track for TRANSLANT I Measurements (U)

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DATA ACQUISITION AND REDUCTION

(C) The explosive acoustic signals were received on hydrophones E1 and E40 at 10,900 ft, BB at 4650 ft, TVA-1 at 14,000 ft, and C6 at 14,708 ft; E1, E40 and C6 are on the sea floor, whereas TVA-1 and BB are suspended at 300 and 2500 ft, respectively, above the bottom. The acoustic signals received at the hydrophones were recorded on 14-channel magnetic tape with each of the 5 hydrophones assigned a high and low gain channel. IRIG-B time code signals and voice were also recorded.

SOURCE LEVELS

(U) Table 1 lists the 1/3-octave-band source levels (energy) of the explosive detonation at the geometric mean frequencies (GMF) of 25, 50, 100, 200, and 400 Hz for the depths of 60 and 500 ft. They are from an unpublished memorandum.¹

Table 1. (C) Effective 1/3-Octave-Band Source Levels
for TRANSLANT I (U)

GMF (Hz)	3-lb TNT at 60 ft	3-lb TNT at 500 ft
25	213.5	219.3
50	214.5	219.7
100	215.5	217.1
200	216.5	219.2
400	217.5	219.4
Source Level (dB//(1 μ Pa) ² · sec at 1 yd.)		

SYSTEM CALIBRATIONS

(U) Calibration curves relating voltage output to a reference sound pressure of 1 μ Pa* versus frequency were available for each hydrophone. Sine wave electrical signals at 1/3-octave GMF were periodically injected at the hydrophone terminals to calibrate the receiving amplifiers and tape recorder.

(U) *See Technical Note on page v.

CONFIDENTIAL**DATA PROCESSING SYSTEM**

(U) A combination analog digital system was used to process the data. The magnetically recorded wideband signals for each hydrophone were reproduced and fed to the 1/3-octave-band analog filters with GMF of 25, 50, 100, 200, and 400 Hz. The filter outputs were envelope detected, serial sampled, multiplexed, and converted from analog to 12-bit digital words. The digital samples were then used as input to a Univac 1230 computer, where a program provided for the calculation of the received signal levels, background noise levels, SNR, and propagation losses (source level-received level). Automatic timing was included in the program to sense for the arrival of the acoustic signal in order to initiate the start of sampling. This feature is subject to manual override if false triggering occurs. A graphic recorder is used to display the received analog signal and the computer generated "window" in order to ensure proper time alignment. The computer program used to calculate the propagation loss and ambient noise values has been described previously.²

RANGE DETERMINATION

(U) A computer program was used to determine the great circle distances between the sources and the hydrophones for all the usable satellite navigational fixes, and the range for each detonation was then determined by interpolation using the associated detonation times.

FORMAT AND PRESENTATION OF THE DATA**ENVIRONMENTAL DATA**

(U) Bathymetry along the track traversed by SANDS is shown in appendix A. The data are plotted to the same range scale as the propagation loss curves presented in the following sections of this report. Bathymetry from the BB hydrophone is that from the actual depth sounding records taken by SANDS, whereas bathymetry from the other hydrophones was determined with the aid of hydrographic charts for the area. For the latter in the range to about 250 nmi, the topography is that best estimated from the charts, since for the geometry of the measurement track with respect to these hydrophones, the source-receiver signal path continually changes with each detonation. Thus, the topography is not an extension of that to the previous detonation, and therefore, a topography plot for each detonation would be required. Over 250 nmi, the topography presented is that obtained from the soundings taken by SANDS. Sound velocity versus depth profiles (SVP) taken by SANDS along the track as indicated in figure 2 are shown in appendix B. A summary of the daily sea state and weather conditions from the SANDS' log is presented in table 2.

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Table 2. (U, Surface Conditions From Log of USNS SANDS (T-AGOR-6) (U)

Date	Sea		Wind		Swell		(in. of Hg - Average)	Barometer Range (nmi) at Start of Day (From Point A)
	Height (ft)	Direction (deg)	Speed (knots)	Direction (deg)	Height (ft)	Direction (deg)		
9/26	3-2	130-155	15-10-15	130-155	6	210	30.00 →	0
9/27	2	180-190	18-10	180-190	6-7	210-230	30.00 →	138
9/28	2	210-360-340	12-10	210-360-340	4-6	220-340	30.07 ↑	333
9/29	2-4	020-060	8-16-12	020-060	4-12-3	020-060	30.16 ↑	534
9/30	1	180-230	8-14	190-230	4	000-010	30.16 ↓	628
10/1	3	240-310	16-22	240-310	3-4	240-310	29.66 ↓	663
10/2	5-6	280-330-310	24-26-12	280-330-310	8-12-8	310-330-210	29.90 →	824
10/3	3-5	300-220	12-22	300-220	4-12	310-350	29.90 →	848
10/4	3-8	220-240-210	20-25-20	220-240-210	8-20-12	350-310	29.90 →	1055
10/5	6-2	210-330	20-12	210-330	12-6-15	300	29.98 ↑	1295
10/6	2-6	330-080	14-16	330-080	8-15-6	310-350	30.17 ↑	1333
10/7	2-1	080-050-090	15-8-15	080-050-090	5	350-360	30.23 →	1142
10/8	3-1	090-050	15-10	090-050	4-2-6	360-050	30.26 →	956
10/9	2-4	050-010	12-14	050-010	6	060-070	30.22 ↓	1121
10/10	3	030-040-020	12	030-040-020	6	070-050	30.18 →	1321
10/11	1-2	030-320-000	10-6-12	030-320-000	6-3-6	050-310-070	30.21 →	1179
10/12	1-4	030-040	8-18	030-040	4-8	070-050	30.22 →	972
10/13	3-6	030	14-24	030	8-15	050	30.13 ↓	1078
10/14	7-6	030-010	20-24	030-010	15-6	050-045	30.03 →	1289

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UNCLASSIFIED**PROPAGATION LOSS**

(U) Point sets representing propagation loss as a function of range or shot number are contained in appendix C. They are arranged in order according to hydrophone, source depth, ship track, and frequency. These plots have been edited to eliminate data that were invalid because of overloading, noise contamination, incomplete detonation of the source, or low SNR on an energy basis, i.e., when the estimated signal energy is equal to or less than the estimated noise energy for an equivalent time interval. Propagation loss was obtained to both the E1 and E40 hydrophones, which are horizontally separated by 1800 ft. Only E1 data are presented inasmuch as there was essentially no discernible difference between the results for the two units.

(U) For the purpose of exhibiting propagation loss and SNR results, the ship track is divided into several segments, namely ABEF, HG, IJ, LK, and MN. For the portion of the track labeled BCDE, there was only a slight change in the ranges to Bermuda receivers, and thus plotting propagation loss and SNR versus shot number proved to be the most convenient way of indexing measured results to topography.

(U) For each hydrophone/track segment/source depth combination, two figures are used to present the results for all five frequencies. The first figure includes results for 25, 50, and 100 Hz; the second gives results for 200 and 400 Hz. In these and later figures, the enclosed numbers with signs following the frequency labeling indicate the adjustment necessary for each curve to give the proper ordinate value.

AMBIENT NOISE SPECTRUM LEVELS

(U) A noise sample is taken just before each signal arrival and the average noise spectrum level is computed for the GMF of each 1/3-octave-band filter by applying a 10-log bandwidth correction to the calculated band level. These levels are presented in appendix D as points in a format compatible with the propagation loss plots and thus give the ambient noise levels at the time the source ship is at a given range from the receivers. For track BCDE, the points are plotted versus shot numbers. Much of the initial background noise was that of the measuring system when low gain or large signal attenuation was used. In order to obtain a true representative level of the ambient sea noise, the gain was increased periodically during the experiment for each hydrophone with the exception of E1. The levels obtained are plotted as connected triangles on the noise spectrum plots, which were first edited to remove points representing system noise.

SIGNAL-TO-NOISE RATIOS

(U) The SNR using the received signal band levels and the band noise levels are shown in appendix E. The format used in the propagation loss plots was also used for the SNR plots.

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DISCUSSION OF EXPERIMENTAL RESULTS**GENERAL COMMENTS ON ENVIRONMENT**

(U) Referring to figure 3, except for areas at 273 and 680 nmi from the start of the track (locations of velocity profiles 3 and 5), a surface duct having a depth variable from 40 to 80 m is indicated by the velocity profiles. Thus, it is likely that for most of the run, the 60-ft sources were in the surface duct. Below the surface duct, a sub-surface channel forms between the origin of the track and 107 nmi (the range to velocity profile 2). This channel extends to between 680 and 847 nmi, as evidenced by velocity profiles 5 and 6. Since the upper (lower) boundary of this channel ranged between 80 and 105 m (400 and 550 m), it always contained the 500-ft sources. The dotted line in figure 3 indicates that the deep sound channel axis lies between 1175 and 1275 m. Critical depths are marked with x's in figure 3. Note that only over the interval from 400 to 800 nmi was there any appreciable depth excess and this stretch was interrupted by high ground at 600 nmi. Over the remainder of the track, the deep sound channel is essentially bottom limited.

AMBIENT NOISE SPECTRUM LEVELS

(U) Referring to appendix C note that a low wind speed condition is evident from the low ambient noise spectrum levels at TVA-1 at 400 Hz for the period during which the ship was at ranges between 650 and 700 nmi.³ The TVA-1 and C6 hydrophone ambient noise spectrum levels at this period agree reasonably well (within 2 to 3 dB) with the average values presented by Perrone for 2400 and 2500 fm and a wind speed of 0 knots.⁴ There is no direct comparison available for the BB noise spectrum levels, but if they are compared with Perrone's values for 1100 fm, the major difference is at 400 Hz where the value here is about 8 to 10 dB lower.

(U) The noise spectrum levels for the different hydrophones are compared in figures 4 and 5 for the ship range EF. In the range AB, system noise associated with some of the hydrophones prevents a similar comparison. Neglecting peaks resulting from local shipping, note that for the frequencies where the noise levels are independent of wind speed (25 and 50 Hz), the spectrum levels for TVA-1 are higher than those for E1 by almost 10 dB. At 25 Hz, C6 and BB noise values range from 5 to 10 dB less than those of TVA-1 with the C6 values higher than those for the BB. At 50 Hz, C6 and BB are within 5 dB of TVA-1 and are within about 3 dB of each other. At 100 and 200 Hz, the general tendency is for the noise levels of TVA-1 to be highest, but the overall spread is reduced to about 5 dB. At 400 Hz, the background noise was that of system noise for E1, and thus no comparison is included. SNR for a given propagation loss could be expected to be lowest at TVA-1 and highest at E1 with a maximum difference of about 10 dB at 25 and 50 Hz.

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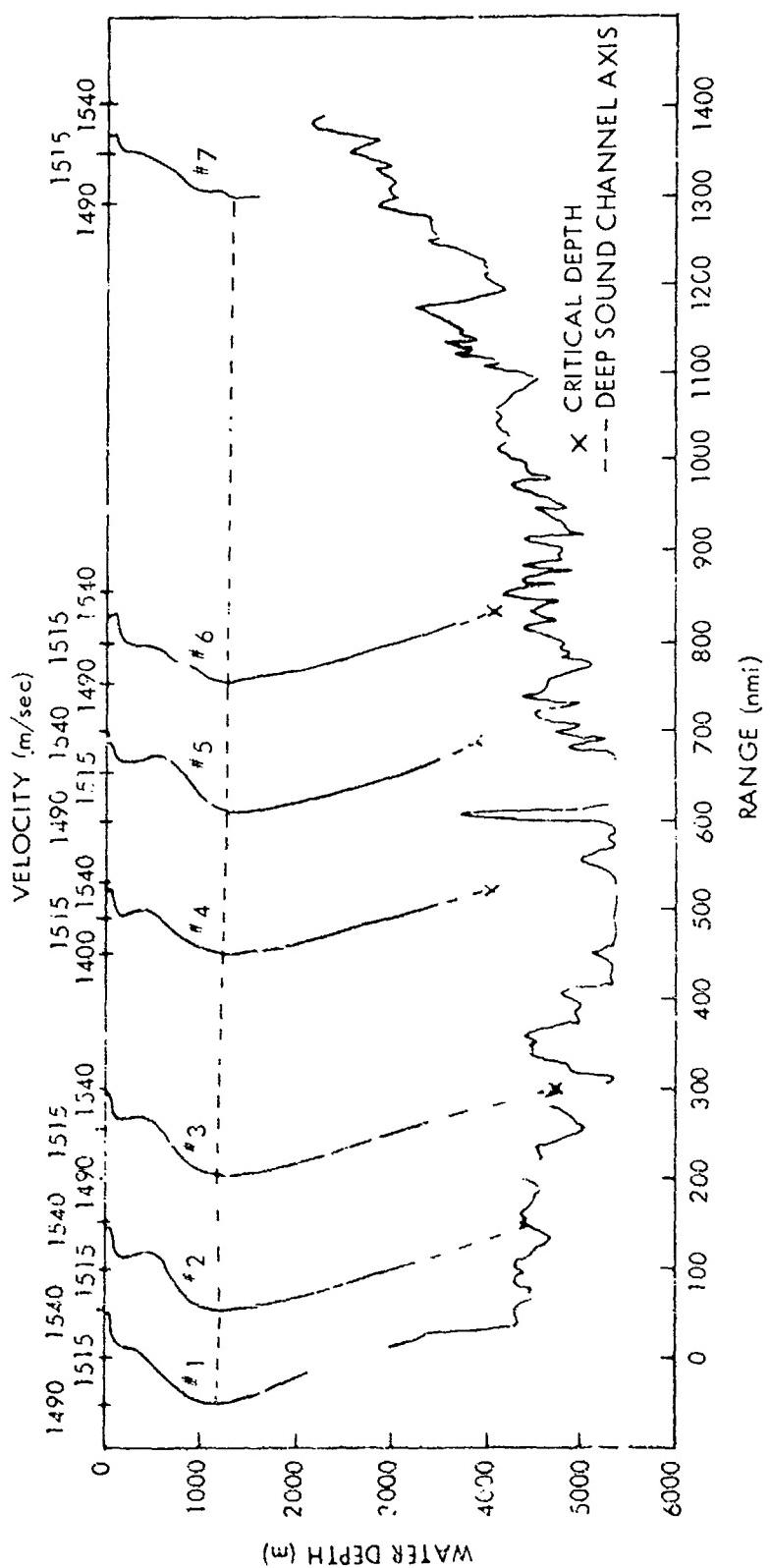


Figure 3. (U) Deep Sound Channel Axis and Critical Depth for TRANSLANT I Measurements (U)

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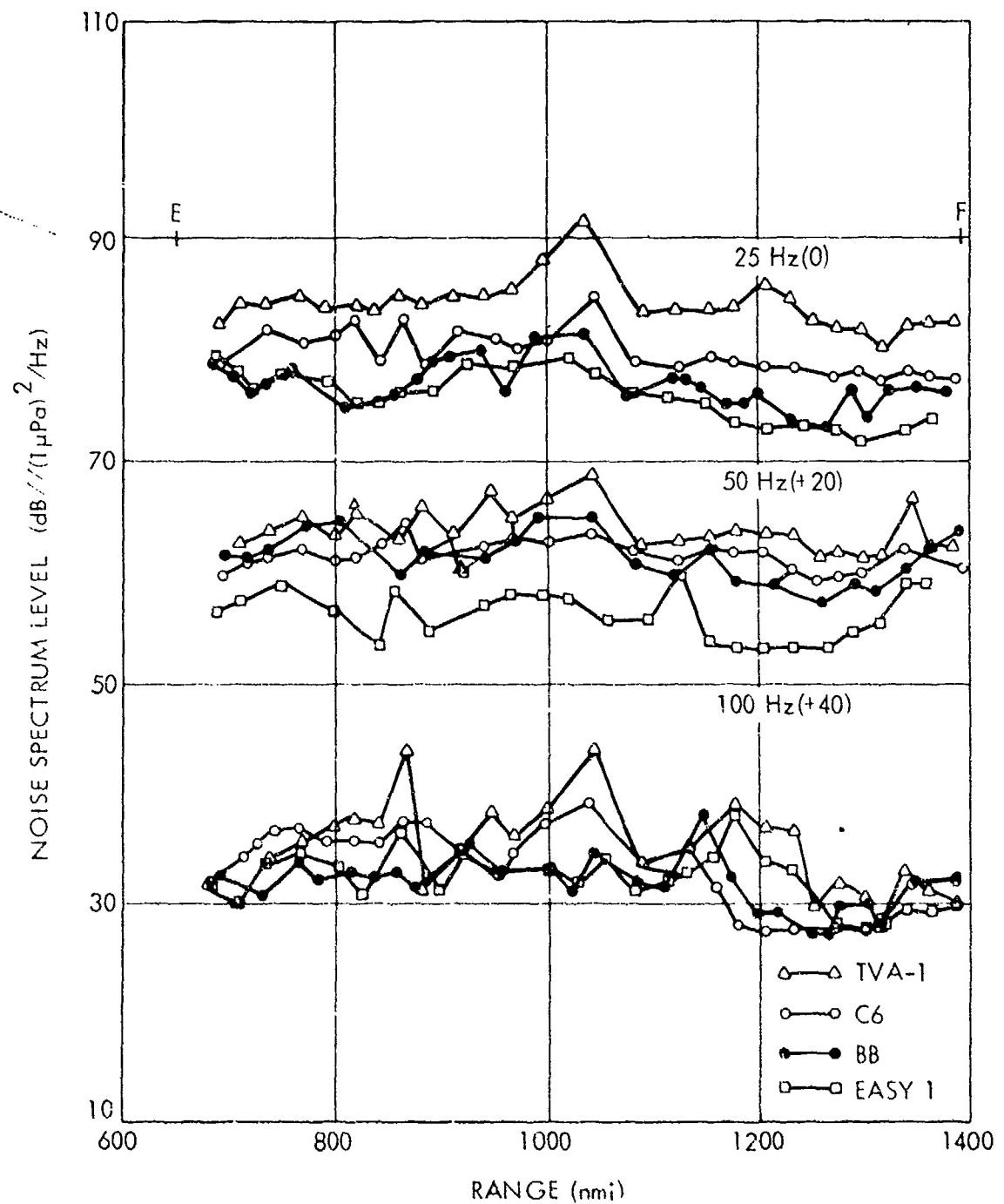


Figure 4. (U) Comparison of Noise Spectrum Levels at TRANSLANT I Hydrophones (25, 50, 100 Hz) (U)

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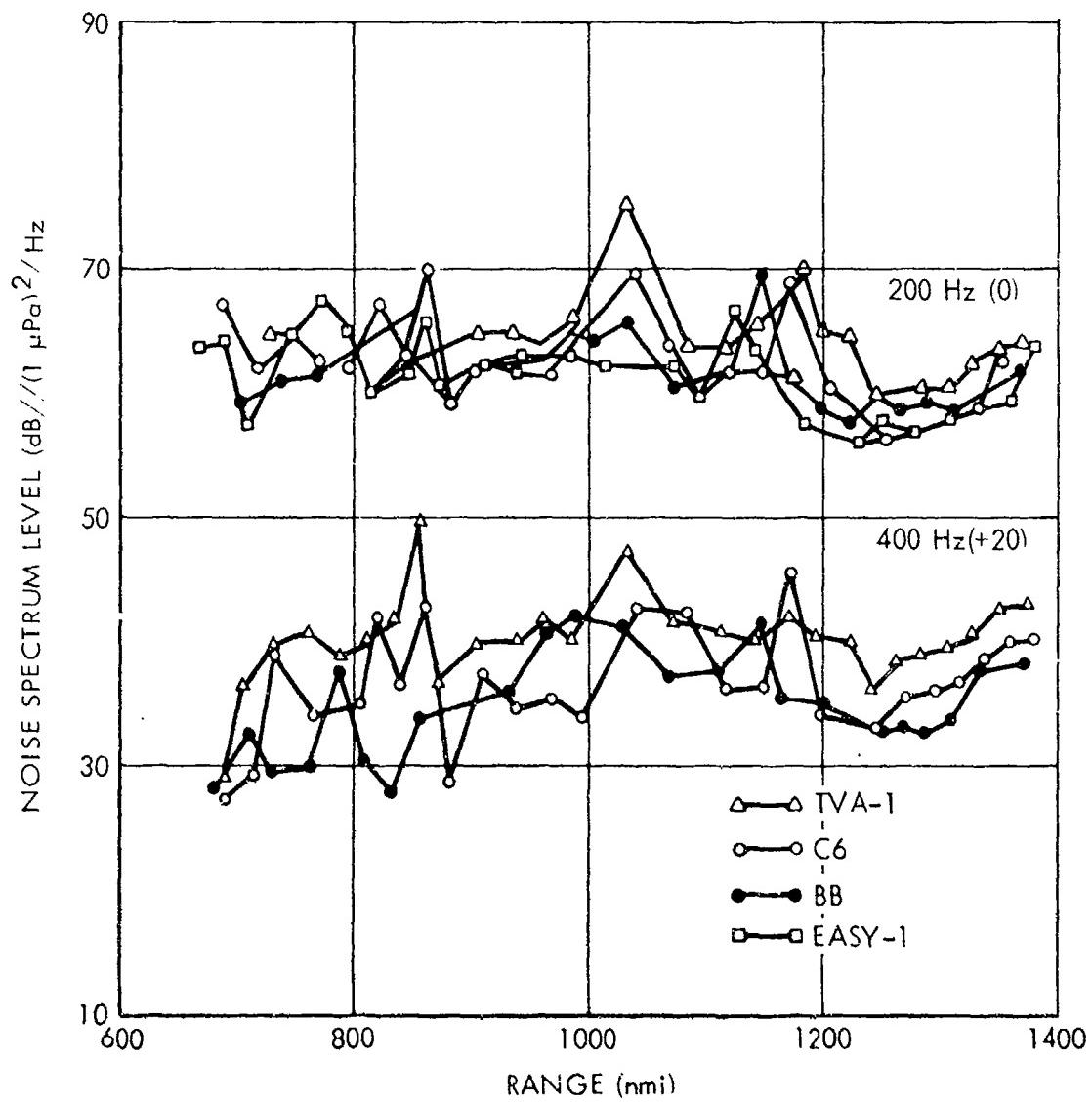


Figure 5. (U) Comparison of Noise Spectrum Levels at TRANSLANT I Hydrophones (200, 400 Hz) (U)

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PROPAGATION LOSS AND SIGNAL-TO-NOISE RATIOS FOR 500-ft SOURCES

(U) For each frequency (25, 50, 100, 200, and 400 Hz), figure 6 contains a plot for the ABEF track, which exhibits (1) average propagation loss to all four hydrophones from the 60-ft sources, (2) average propagation for the 500-ft sources, and (3) a bottom profile, all of which are plotted as a function of range. The average values were obtained by drawing lines of best fit through the appropriate scatter diagrams of appendix C. Since the use of average values hides the scatter in the data and obscures the effects of zonal propagation, figure 6 is presented only as a continuing guide for use while reading the following sections. For details, the reader is directed to the figures in appendix C that actually contain the point sets.

(C) From the long-range propagation loss curves for track ABEF, it is seen that the loss curves for TVA-1 and C6 (figure 6) are very similar in shape. Convergence zone gains are quite evident in the point set plots shown in appendix C. The average propagation loss for TVA-1 is 2 to 5 dB less than that for C6 for frequencies up to 100 Hz. At 200 and 400 Hz, large convergence gains (20 dB or more) at TVA-1 overshadow similar gains for C6. However, from the previous discussion, as a result of higher ambient sea noise at TVA-1 for 25, 50, and 100 Hz, the received SNR would be about the same as C6. At 200 and 400 Hz, the SNR at TVA-1 would be higher as a result of the higher convergence gain and lower loss. This is reasonably confirmed by comparing the SNR for the two hydrophones in appendix E.

(C) The propagation loss curves at 25, 50, and 100 Hz extend to approximately 900 to 1100 nmi for both hydrophones. Subsequent tracks of HG, IJ, LK, and MN give values compatible with the ABEF track for the same range, and any effect at ranges over 1100 nmi due to topographical features is not evident.

(C) Losses are greater to BB than to E1 for 25 through 200 Hz out to about 200 nmi. The sudden decrease of losses for BB that appears for all frequencies just beyond 200 nmi has been checked and rechecked to determine if a processing error existed. However, this does not seem to be the case, and beyond this range BB losses approach those of E1 and are in general agreement from approximately 250 to about 1100 nmi. The loss values at 400 Hz for E1 were limited as a result of high system noise and are essentially not usable beyond 150 nmi. Loss values to BB for this frequency are available out to a range of about 800 nmi. Convergence type gains are evident for both hydrophones at lower frequencies but are slightly more noticeable for E1. Considering 25- through 200-Hz results, note that curves for both BB and E1 show a marked increase in loss at about 1200 nmi. This is at the range where an approximate 100-nmi-wide trench exists in the Mid-Atlantic Ridge, as indicated in the bottom topography. Beyond this range, the loss to E1 gradually increases out to a maximum at 1300 nmi. On the other hand, for BB the losses beyond the trench decrease again to near their earlier values. For still greater ranges (over 1280 nmi), there is a diminution of propagation loss to BB, especially at 25 and 50 Hz followed by complete cutoff of the signal corresponding to the ship's actual traverse of the ridge.

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(C) At approximately 1300 nmi, which is the most distant range for which losses could be measured to E1, loss values to E1 are about 10 dB greater than are the losses to BB. Here, the energy from the sources, which normally follows paths to E1, is reflected from the upper slopes of the ridge toward the channel axis thus favoring propagation to BB.

(C) For the excursions (GH, IJ, LK, and MN) back and forth across the ridge, it is seen from the bathymetry (appendix A) and track plot (figure 2) that the peak of the Mid-Atlantic Ridge decreases in range with subsequent crossovers. Again, there is up to 10 dB lower propagation losses to BB than to E1 in the vicinity of the ridge. Just as for the ABEF track, propagation losses to BB increase rapidly as the ship crosses the ridge.

(U) The SNR curves (appendix E) reflect the different propagation loss values to BB and E1 in the vicinity of the Mid-Atlantic Ridge. Thus, around the 1300-nmi range where the loss to BB becomes lower than that to E1, the SNR is greater for BB by about 5 to 10 dB at 25 Hz and somewhat less at other frequencies.

(C) The average propagation loss to TVA-1 at 25 Hz is less than that to E1 and BB out to about 800 nmi. For frequencies of 50 Hz and above, the crossover range lowers to about 250 nmi or less, and for ranges beyond the crossover, the average loss is greater to TVA-1. The average loss above 250 nmi at 400 Hz is about the same to TVA-1 and BB. For E1 there are no corresponding loss values as a result of a high 400-Hz system noise.

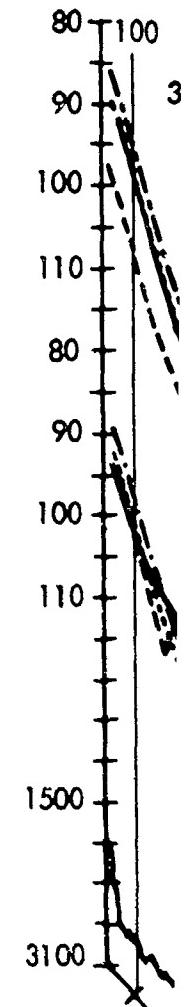
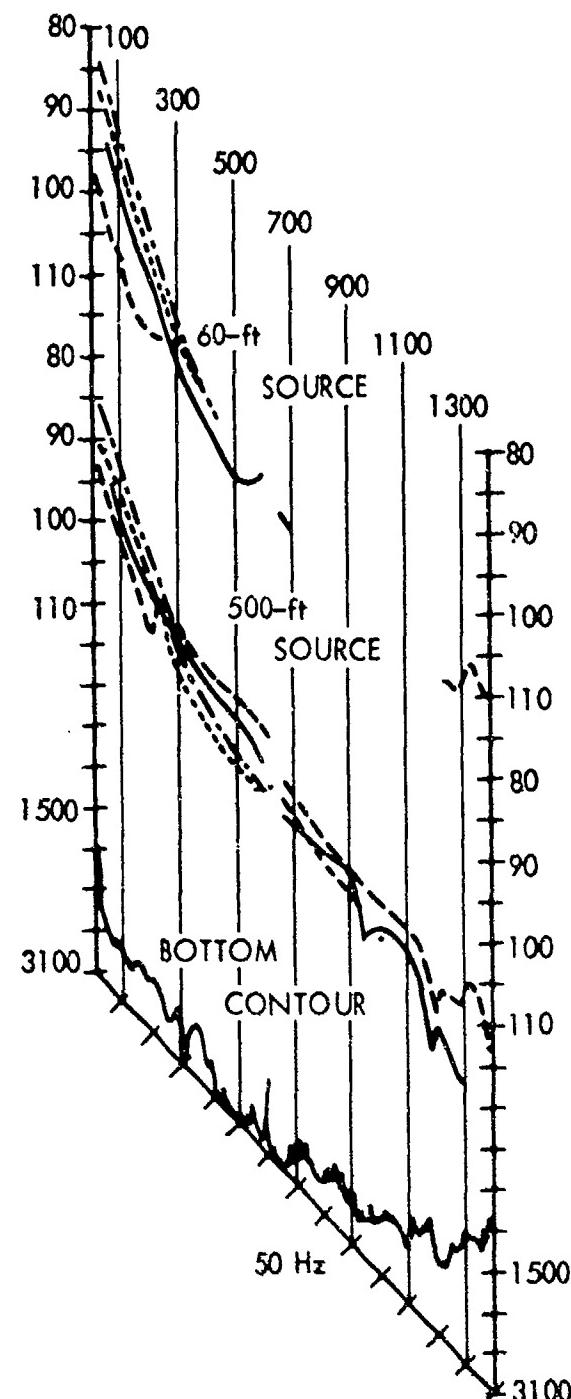
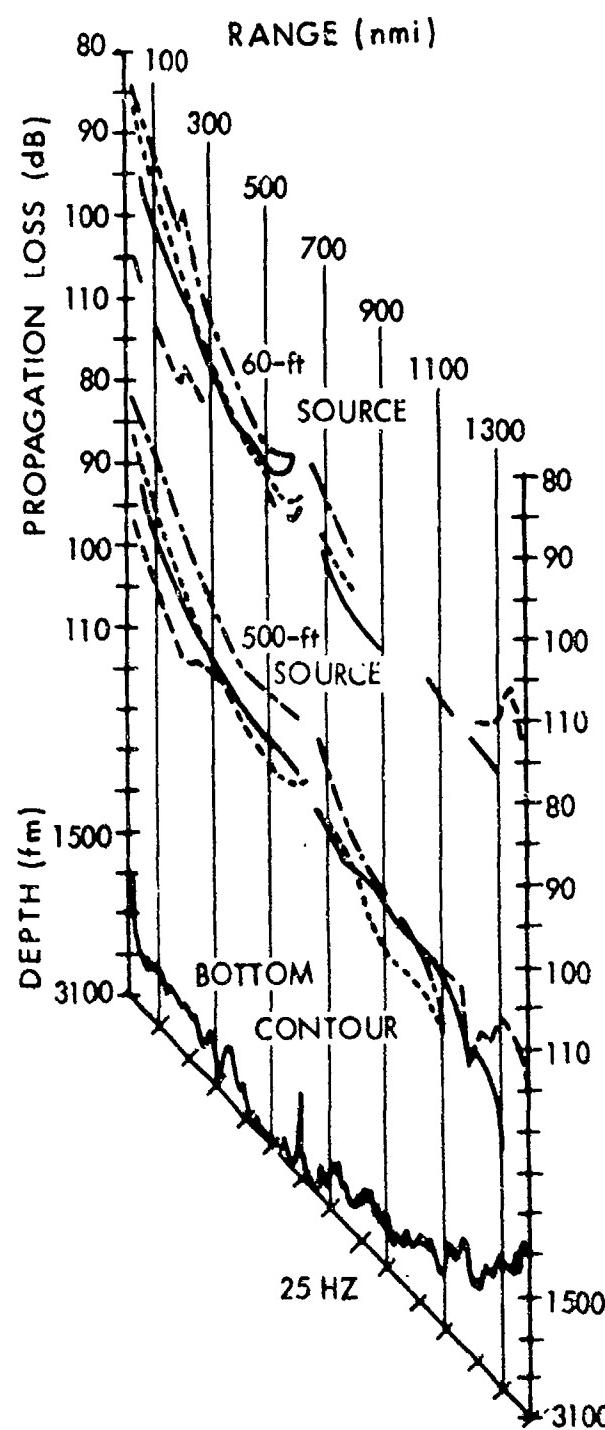
(C) In figure 6, the southern part of the high ground of the Rockaway Seamount appears at a range of 600 nmi. This high ground is reflected in the lower propagation losses and higher SNR at 25 and 50 Hz to the deep hydrophones C6 and TVA-1.

PROPAGATION LOSS AND SIGNAL-TO-NOISE RATIOS FOR 60-ft SOURCES

(C) The propagation loss from the 60-ft sources to TVA-1 for all frequencies and ranges is similar to but lower than that to C6 (figure 6). At 25, 50, and 100 Hz, the lower loss at TVA-1 is equalized by higher ambient noise so that the SNR is about the same as C6 (appendix E). Higher convergence gains at TVA-1 at 200 and 400 Hz result in a higher SNR than for C6. The results are similar to those obtained for the 500-ft sources.

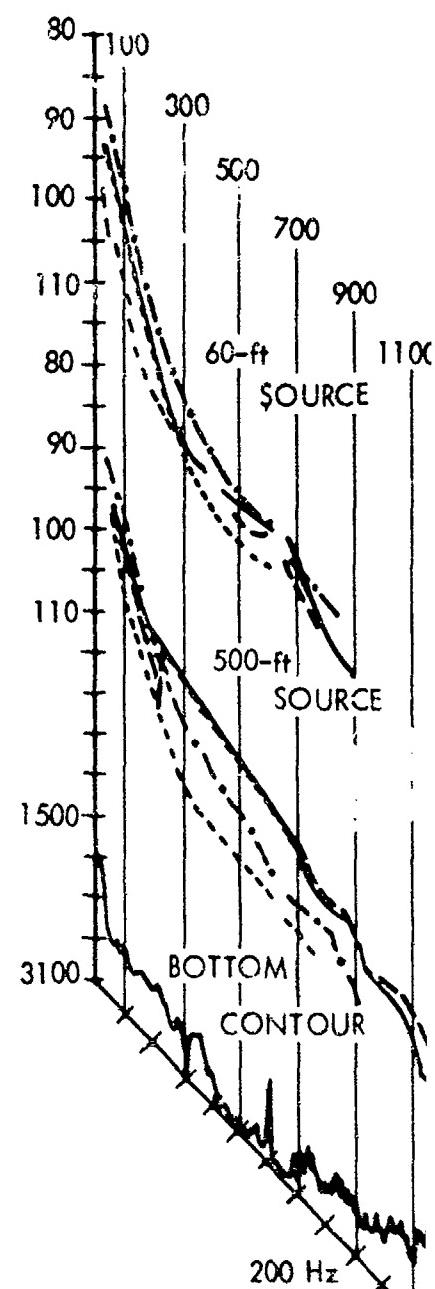
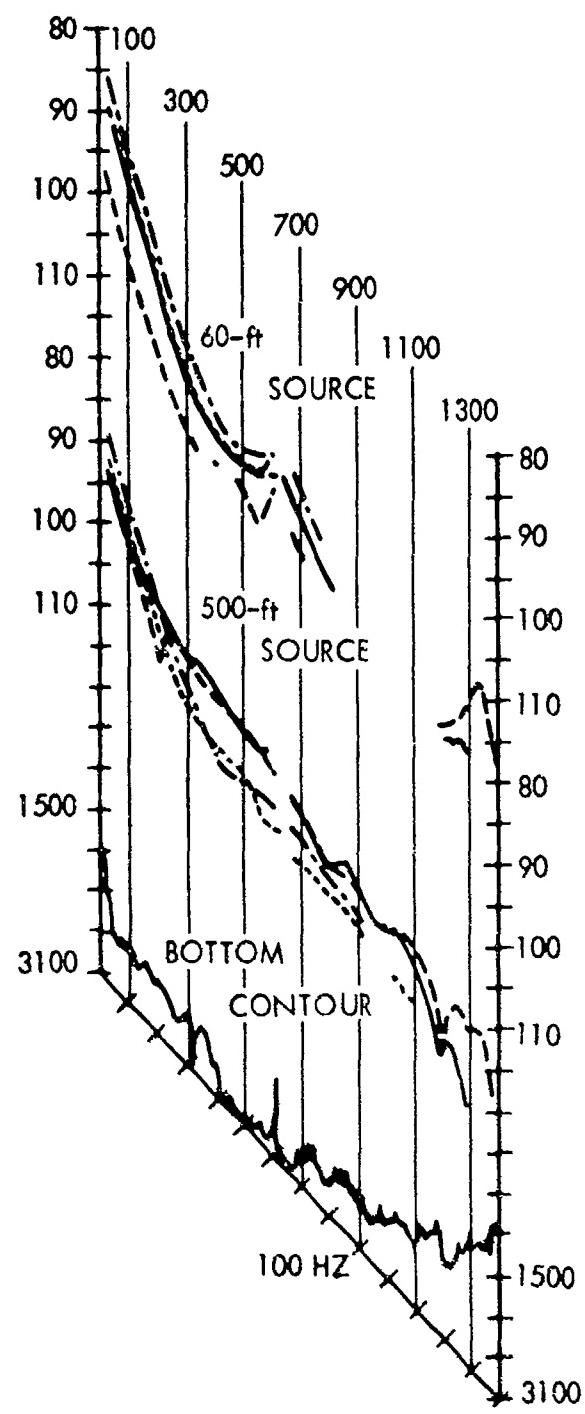
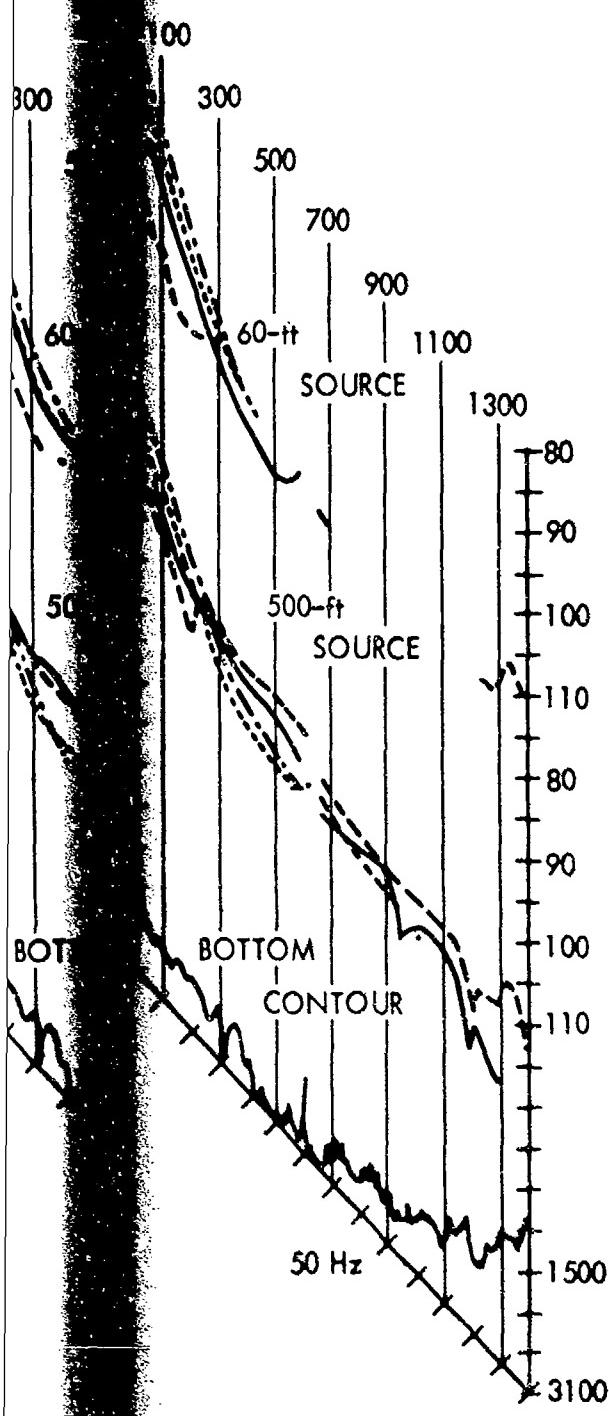
(C) Out to the range where they can be compared (approximately 600 to 800 nmi), the average propagation loss to TVA-1 generally is lower than that to E1 at all the frequencies. Here again, as in the case of the 500-ft sources, the lower loss to TVA-1 for 25, 50, and 100 Hz is somewhat offset by higher ambient noise so that one may expect the SNR to be about the same as for E1. TVA-1 indicates a slight advantage in SNR at 200 Hz in the 200- to 400-nmi range as a result of convergence gains. For 25, 50, 100, and 200 Hz beyond 800 nmi where essentially there are no propagation loss values for TVA-1 because of low SNR, some values are still available at E1 to a range of about 1200 nmi.

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HYDROPHONE KEY

- EASY 1 ——————
- BROADBAND -----
- LOWER ----- ·····
- TVA-1 ----- ·····
- COHERENCE 6 ----- ······



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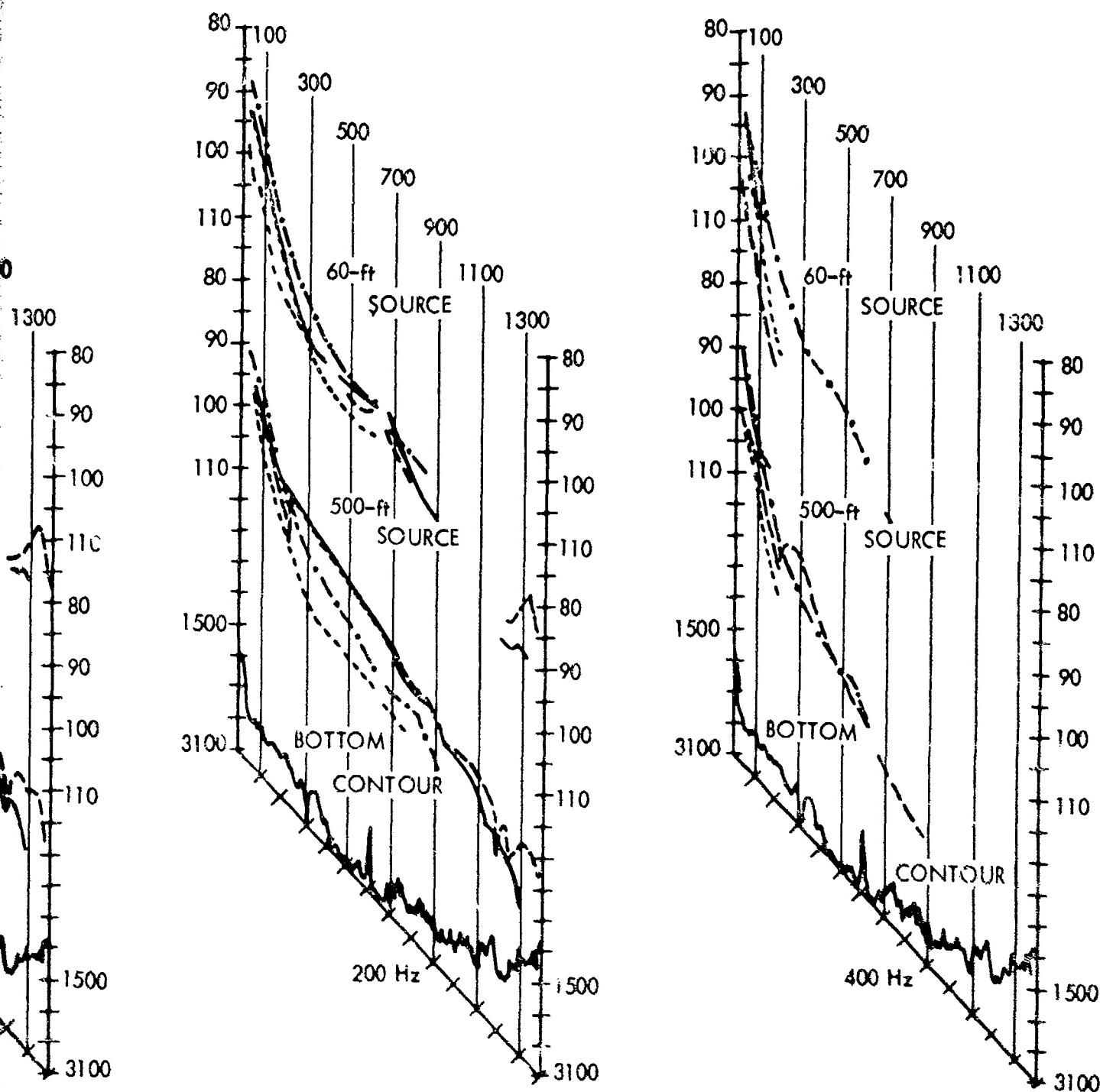


Figure 6. (C) TRANSLANT I Propagation Loss Composite (U)

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13/14

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(C) Out to 1200 nmi and for the frequencies measured, the propagation loss is greater and the SNR generally lower at BB than for any of the other hydrophones. At 25 and 50 Hz, the loss is about 10 to 20 dB greater than for TVA-1 for ranges out to about 200 nmi. In the range from near 600 to almost 1200 nmi, only a relatively few received signals exceeded the background noise at the hydrophones. Above 1200 nmi, however, there is a substantial increase in signal level and corresponding lower propagation loss at BB to about 1375 nmi, after which the loss increases rapidly. This diminution of propagation loss is even more pronounced than for the case of 500-ft sources. The propagation loss for BB and E1 in this region is compared in figure 7 for 25, 50, and 100 Hz. In the vicinity of 1300 nmi where E1 curves terminate, the propagation loss to BB is from 5 to about 15 dB lower. For the 60-ft sources the effect of the seamount at about 630 nmi reduces the propagation loss at all hydrophones and is more noticeable than for the 500-ft sources.

(C) The effect of the Atlantic Ridge on the propagation loss for 60-ft sources for tracks HG, IJ, LK, and MN is similar to that noted for the 500-ft sources. The propagation loss decreases to BB as the source approaches the ridge and increases rapidly after passing over the peak. Increases in loss to BB are also noted at the ranges where troughs or depressions exist in the ridge. In track HG where the forward wall of the trench or depression is very steep and about 950 fm deep, the propagation loss values cut off sharply. At track IJ where the depression is only about 600 fm deep and the forward wall not very steep, the propagation loss is seen to increase but at a slower rate with increasing range.

COMPARISON OF 60- AND 500-ft PROPAGATION LOSS RESULTS

(C) With the exception of some increased zonal enhancement at 25 Hz for the 500-ft sources, the propagation loss to TVA-1 is about the same for both the 500- and the 60-ft sources. This is also true for C6. Furthermore, for most ranges and frequencies, losses to the deeper receiver, C6, are typically 3 or 4 dB greater than are losses to TVA-1.

(C) Although scarcely measurable in the first 200 nmi, the loss to E1 at all frequencies is progressively less with increasing range for the 500-ft sources than for the 60-ft sources. The propagation loss to BB is clearly source-depth dependent out to near the Atlantic Ridge, with that for the 500-ft source having less loss. This source-depth dependency is consistent with the view that a large part of the signal at the hydrophone is due to totally refracted paths and the deeper source involves a proportionally greater number of the more nearly axial rays. At the Atlantic Ridge, energy from sources at both depths is reflected into refraction paths near the channel axis, and thus the propagation loss is lower to BB than to any other hydrophone. However, this reflective mechanism appears slightly more efficient in the case of 60-ft sources as indicated by the slightly lower losses to BB in the 1300- to 1400-nmi region for the shallow charges.

(U) It should also be noted that there was a greater increase in signal level to all hydrophones due to the Rockaway Seamount for 60-ft sources than for 500-ft sources.

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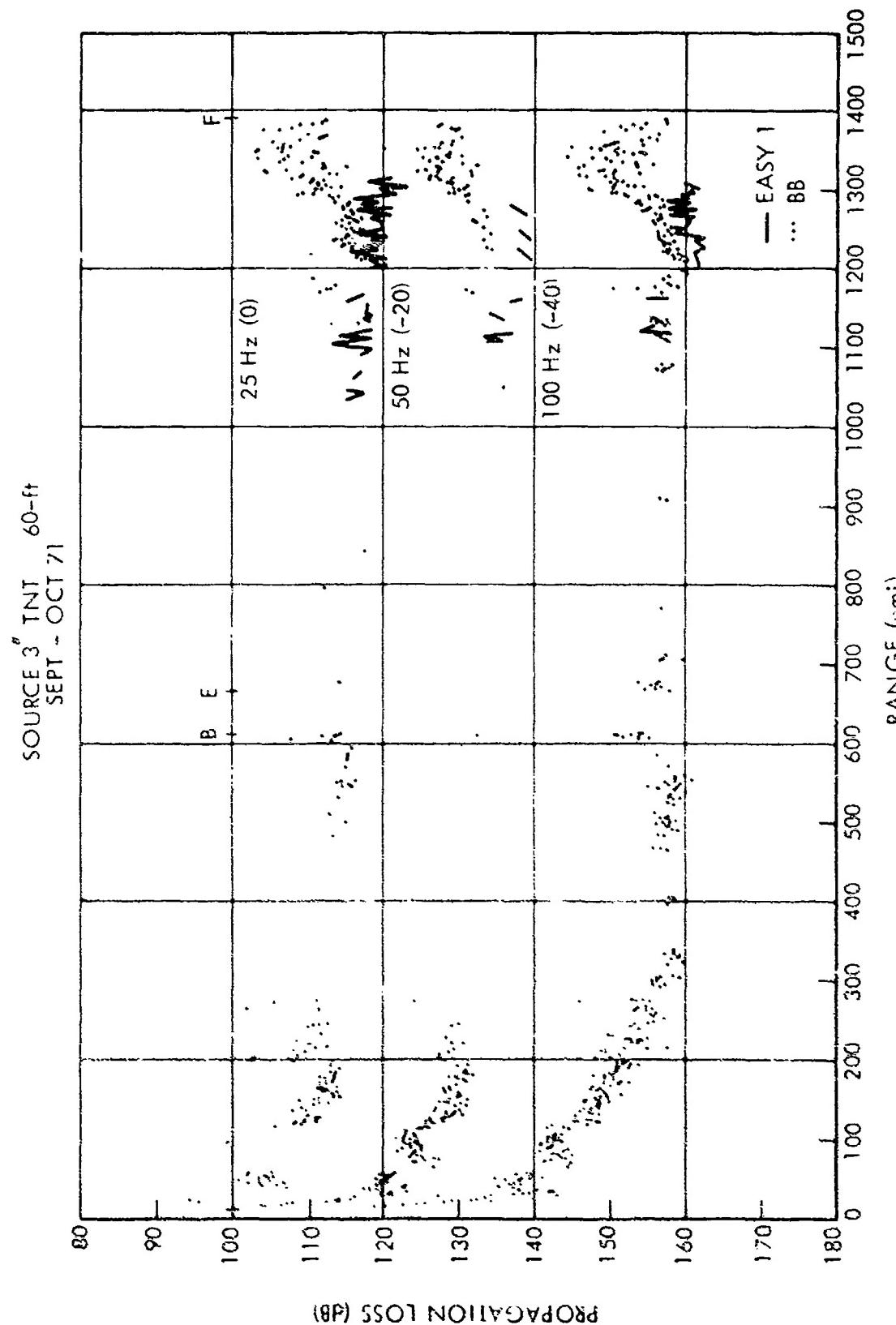


Figure 7. (C) Propagation Loss Comparison at 3B and E1 Hydrophones (25, 50, 100 Hz) (U)

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PROPAGATION LOSS FOR TRACK BCDE

(U) The propagation loss values versus shot number for the track BCDE are presented in appendix C for the various frequencies, hydrophones, and source depths. The bottom contour along this track is shown in appendix A. The most pronounced feature of the contour is the double peak in the Rockaway Seamount area extending upwards to almost 400 fm from the surface for the highest peak and to about 1200 fm for the lower peak. The peaks are in the DE section of the track near shot 1500. Two minor peaks to 2400 and 2600 fm are near shots 1100 and 1700, respectively.

(C) For the 500-ft source, the propagation loss values for E1 and BB agree closely in shape and level. At about shot 1200 or shortly after passing the first minor peak in the topography plot, the losses increase until near the first large peak at about shot 1500, and then decrease rapidly. The effect of the high peaks on the propagation loss is more evident in the plots for the 60-ft source, since the propagation loss is greater and there are fewer values. Decreases in propagation loss amounting to 10 dB or more occur in the region of the highest peak. For TVA-1 and C6, the spread and variability of the propagation loss data do not lend themselves to an easy interpretation of the effects of the seamount. However, both TVA-1 and C6 show a gap in the data for the shot numbers covering the regions between the two major peaks.

COMPARISON OF TRANSLANT I AND PROJECT
ATOE/NA MEASUREMENTS

(U) A long-range propagation measurement from Bermuda to the Mid-Atlantic Ridge was made in the winter months of January and February 1971, under Project ATOE/NA⁵ (Acoustic Transmission and Oceanographic Experiment, North Atlantic). Source depths were 60, 500, 2000, and 4000 ft, and the receiving hydrophones were the same as those used in the TRANSLANT I measurement. The track followed the great circle route that intersected and passed over the Rockaway Seamount. At this point the course went due south to where the seamount was not in the transmission path and then proceeded along approximately the same great circle route as that for TRANSLANT I to the Mid-Atlantic Ridge where the measurements ceased. The sound velocity profiles indicated a surface channel of about 150-m depth for the first 900 nmi. During the final 500 nmi, the vertical extent of the layer decreased and was quite variable but always contained the 60-ft source. Over the entire test track the velocity minimum or deep sound channel axis was between 3100 and 4400 ft.

(C) Reduced propagation loss near the seamount was evident at BB with a substantial reduction in received signal when the track went behind the mount. When the course was changed to avoid having the seamount in the transmission path, the signals were again received. Disregarding seamount effects at BB, the lowest propagation loss for 50 through 200 Hz for the 60- and 500-ft sources are to BB and E1 (designated Easy II in ATOE/NA) followed by increasing loss to TVA-1 and C6, respectively. At 25 Hz, the propagation loss was slightly lower to TVA-1 than to E1 for both source depths and also slightly lower than that to BB for the 500-ft depth. For 25 Hz, the loss is greatest to BB for the 60-ft source.

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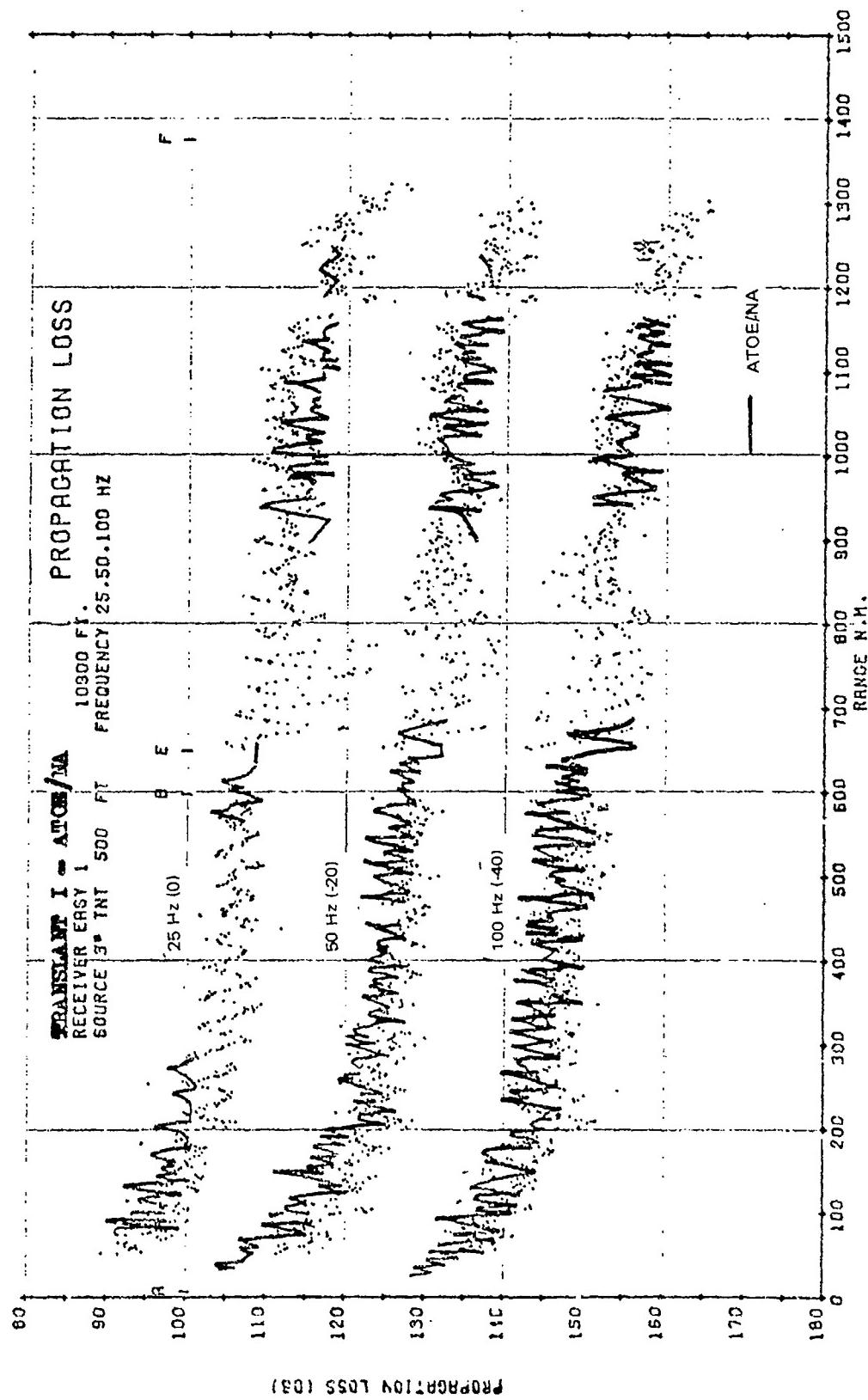


Figure 8. (C) Propagation Loss at E1 Hydrophone (25, 50, 100 Hz) for a Source Depth of 500 ft (U)

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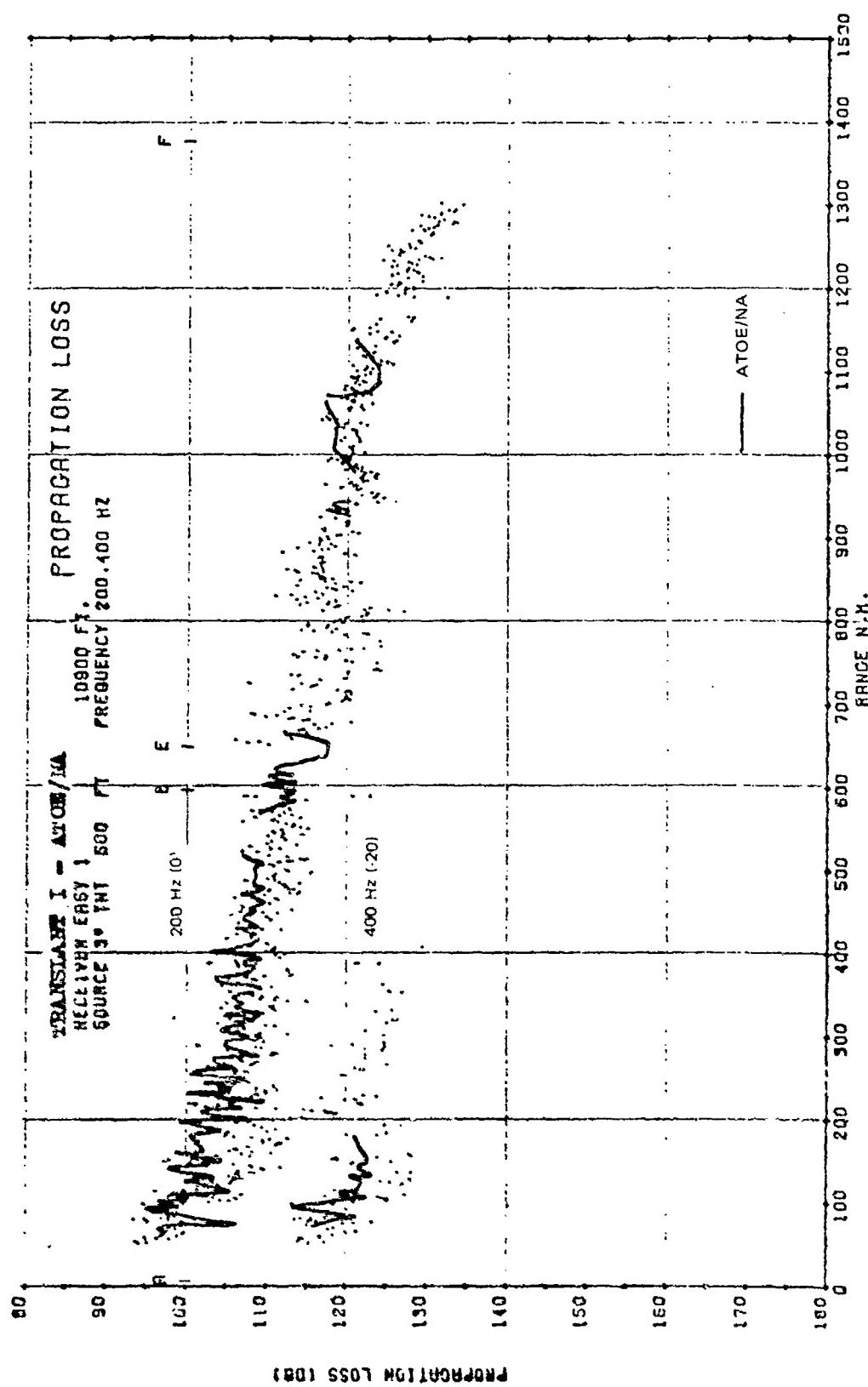


Figure 9. (C) Propagation Loss at E1 Hydrophone (200, 400 Hz) for a Source Depth of 500 ft (U)

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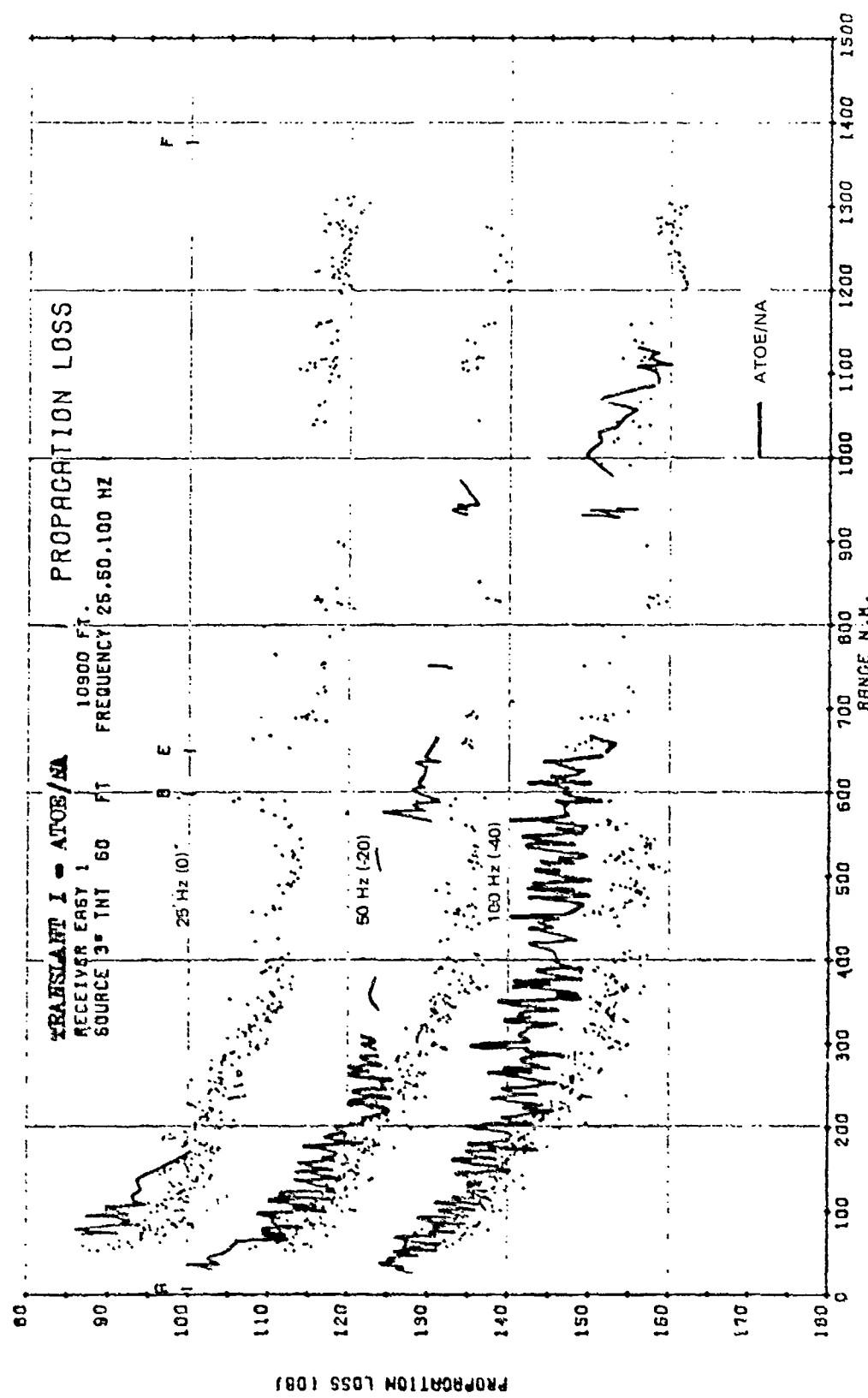


Figure 10. (C) Propagation Loss at E1 Hydrophone (25, 50, 100 Hz) for a Source Depth of 60 ft (U)

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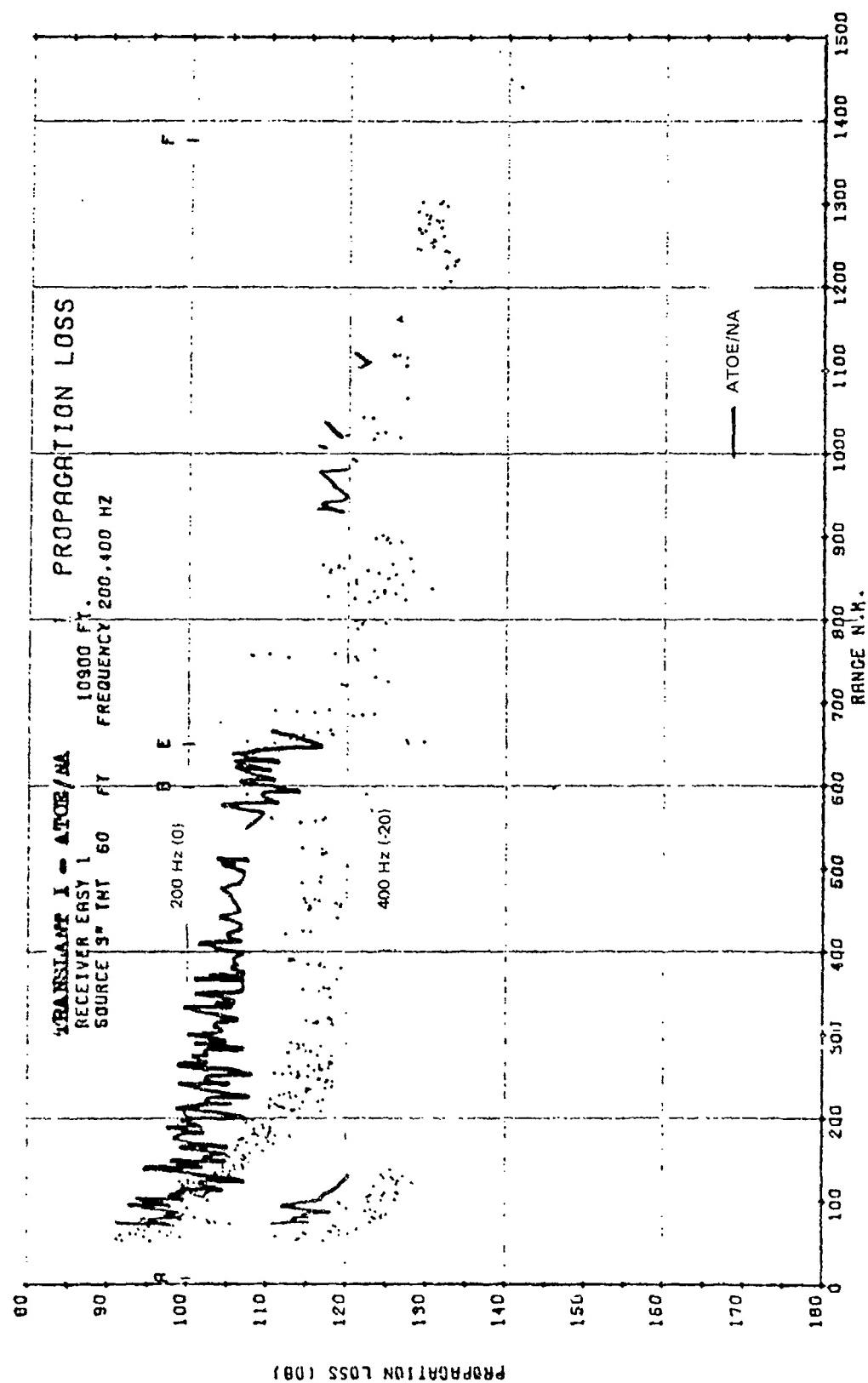


Figure 11. (C) Propagation Loss at E1 Hydrophone (200, 400 Hz) for a Source Depth of 60 ft (U)

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(C) Values of propagation loss versus range for TRANSLANT I and ATOE/NA are compared for the E1 receiver for 500-ft sources in figures 8 and 9. The solid lines representing the ATOE/NA data are eye sketched from the individual values of the measurements. For ranges out to 700 nmi and for frequencies up to 200 Hz, propagation loss averages about 2 dB more for TRANSLANT I than for ATOE/NA. Figures 10 and 11 present a similar comparison except that here the source depth is 60 ft. Again, for ranges out to about 700 nmi and for frequencies up to 200 Hz, the available data indicate that the ATOE/NA losses averaged about 6.5 dB less than the TRANSLANT I propagation loss values. Comparisons of propagation loss values versus range for the two exercises for the remaining hydrophones are contained in appendix F. Neglecting the effects of the Atlantic Ridge, the major difference for the 500-ft source at BB is for frequencies at and below 100 Hz where the TRANSLANT I losses are 5 to 10 dB greater than ATOE/NA losses. For the 60-ft sources, the losses were 5 dB or greater for all frequencies above 25 Hz for the TRANSLANT I measurements for all ranges where data were available for comparison. For the 500- and 60-ft sources the average loss to TVA-1 and C6 for frequencies above 25 Hz are alike for both of the measurements. At 25 Hz the loss is 4 or 5 dB lower for the TRANSLANT I measurements at both hydrophones.

(C) In summary, neglecting the effects of the Atlantic Ridge and seamounts, there is no single hydrophone that indicates the lowest average propagation loss at all frequencies and ranges for both source depths for both the ATOE/NA and TRANSLANT I measurements. Both measurements indicate that the lowest average loss at 25 Hz is to TVA-1 for ranges where they can be compared for both sources. For the 500-ft source and the frequencies 50, 100, 200, and 400 Hz the lowest average loss for the ATOE/NA measurements is to BB except for the range to 125 nmi at 400 Hz where that to E1 is slightly lower. For TRANSLANT I and for the same source depths and frequencies, the average loss to TVA-1 is equal to or lower than that to the other hydrophones to about 250 nmi. Above this range, BB and E1 are about equally low. The noise spectrum levels of TRANSLANT I indicate that the advantage of lower loss at TVA-1 is somewhat nullified so that from a detection standpoint E1 may be equal to or have a slight advantage over TVA-1. TRANSLANT I gives the lowest loss for the 60-ft source for all frequencies to TVA-1; however, again considering the background noise, E1 and C6 would be suitable from a detection standpoint. From ATOE/NA for the 60-ft source, the lowest average loss at 50, 100, and 200 Hz is most consistent to BB. At 400 Hz over the first 100 nmi, E1 indicates slightly lower loss than BB. There is no comparison of ambient noise at the various hydrophones in the ATOE/NA report, because of the large amount of local ship interference. However, occasional comparisons of ambient noise that were possible appear to indicate that the advantage in detection resulting from lower loss at TVA-1 at 25 Hz is reduced by the higher ambient noise so that detection is similar to that at BB. A similar ambient noise increase for BB at 200-Hz would result in a better advantage in detection at E1.

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CONCLUSIONS

(C) From the TRANSLANT I measurements, considering both propagation losses and ambient background noise, the best reception of acoustic signals from both the 60- and 500-ft sources and for frequencies of 25, 50, 100, and 200 Hz is the bottom mounted hydrophone E1 for ranges up to but not exceeding the Mid-Atlantic Ridge (about 1300 nmi). Near and at the peak of the ridge, energy is received only at the BB hydrophone with the propagation loss values lowest for the 60-ft source. The loss at this range (about 1400 nmi) for the 60-ft source is approximately equal to that at about 100 nmi and the SNR reaches almost 20 dB. The transmission path is effectively blocked by the ridge for both source depths for ranges past the ridge.

(U) The propagation loss for the 60-ft source only is lowest to TVA-1. However, the lower propagation loss is offset by higher ambient sea noise, and thus from a detection standpoint, E1 and TVA-1 are alike. For this source depth, the poorest results (except as noted above at the Ridge) are at BB because of its large propagation loss.

(U) For the 500-ft sources only, the lowest propagation loss is to E1 with that at BB being about the same. The greatest propagation loss and lowest SNR are at C6.

(U) The propagation loss is lower at any hydrophone for the 500-ft source than for 60-ft sources. In addition to the decrease in propagation loss to BB resulting from the ridge, propagation loss is also influenced by other topographical features, such as seamounts and the trench in the ridge. In the latter case, the propagation loss increases to BB and E1 for the 500-ft source.

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1. L. C. Maples, unpublished memorandum.
2. R. W. Hasse and R. L. Martin, "PARKA I — Acoustic Processing and Results," NUSL Technical Memorandum 2210-015-69, 28 July 1969 (CONFIDENTIAL).
3. A. J. Perrone, "Deep-Ocean Ambient Noise Spectra in the Northwest Atlantic," Journal of the Acoustical Society of America, vol. 46, no. 3, September 1969, pp. 762-770.
4. A. J. Perrone, "Ambient Noise Level as a Function of Water Depth," Journal of the Acoustical Society of America, vol. 48, no. 1, July 1970, pp. 362-370.
5. R. F. LaPlante, F. C. Friedel, W. H. Thorp, and P. D. Koenigs, Low-Frequency Propagation Loss Measurements of the Acoustic Transmission and Oceanographic Experiment (ATOE) in the Atlantic Ocean East of Bermuda (U), NUSC Technical Report 4473, 14 June 1973 (CONFIDENTIAL).

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Appendix A
TRANSLANT I BOTTOM TOPOGRAPHY PLOTS

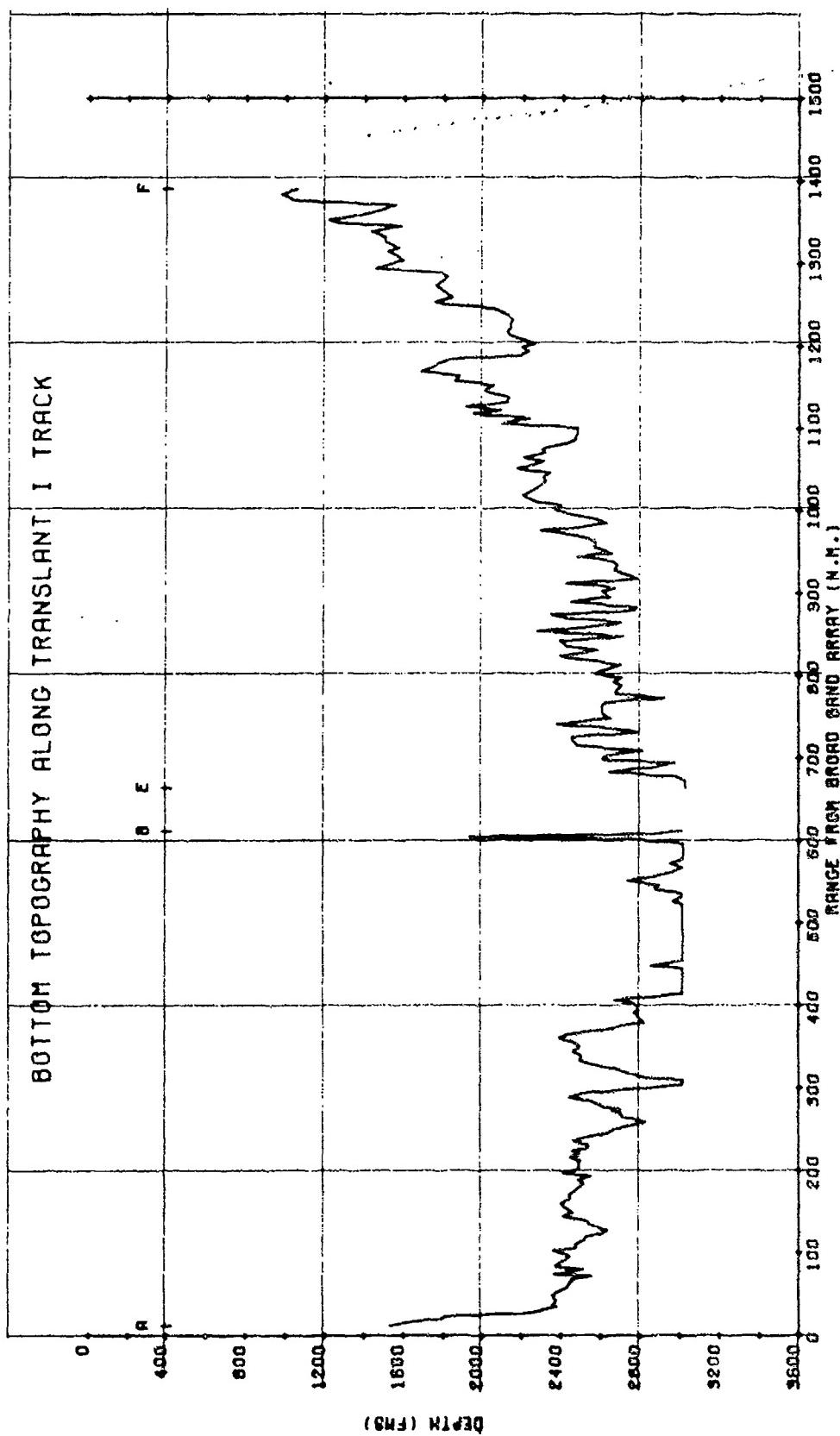
Bottom topography plots along the TRANSLANT I track are presented on the following pages.

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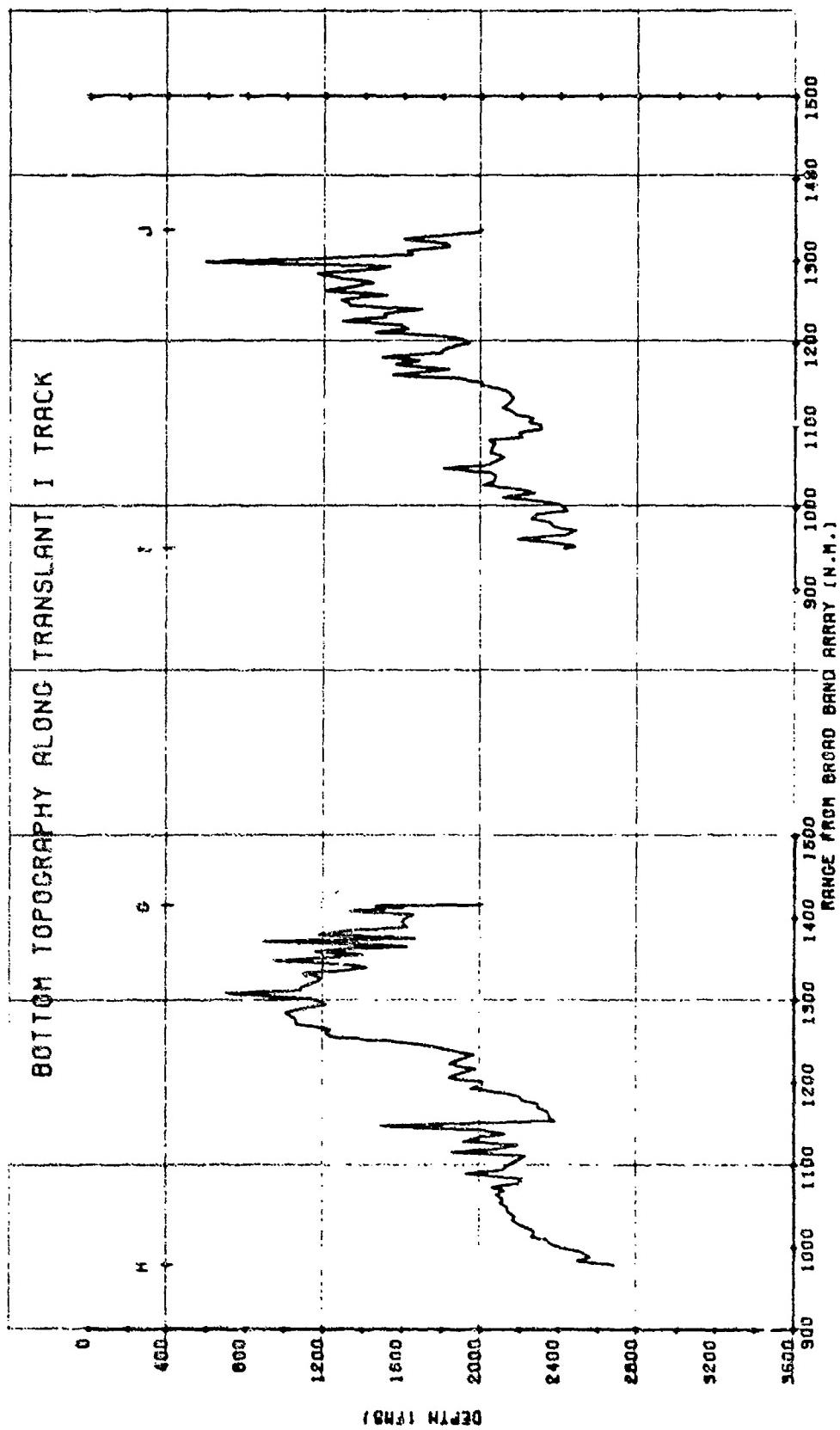


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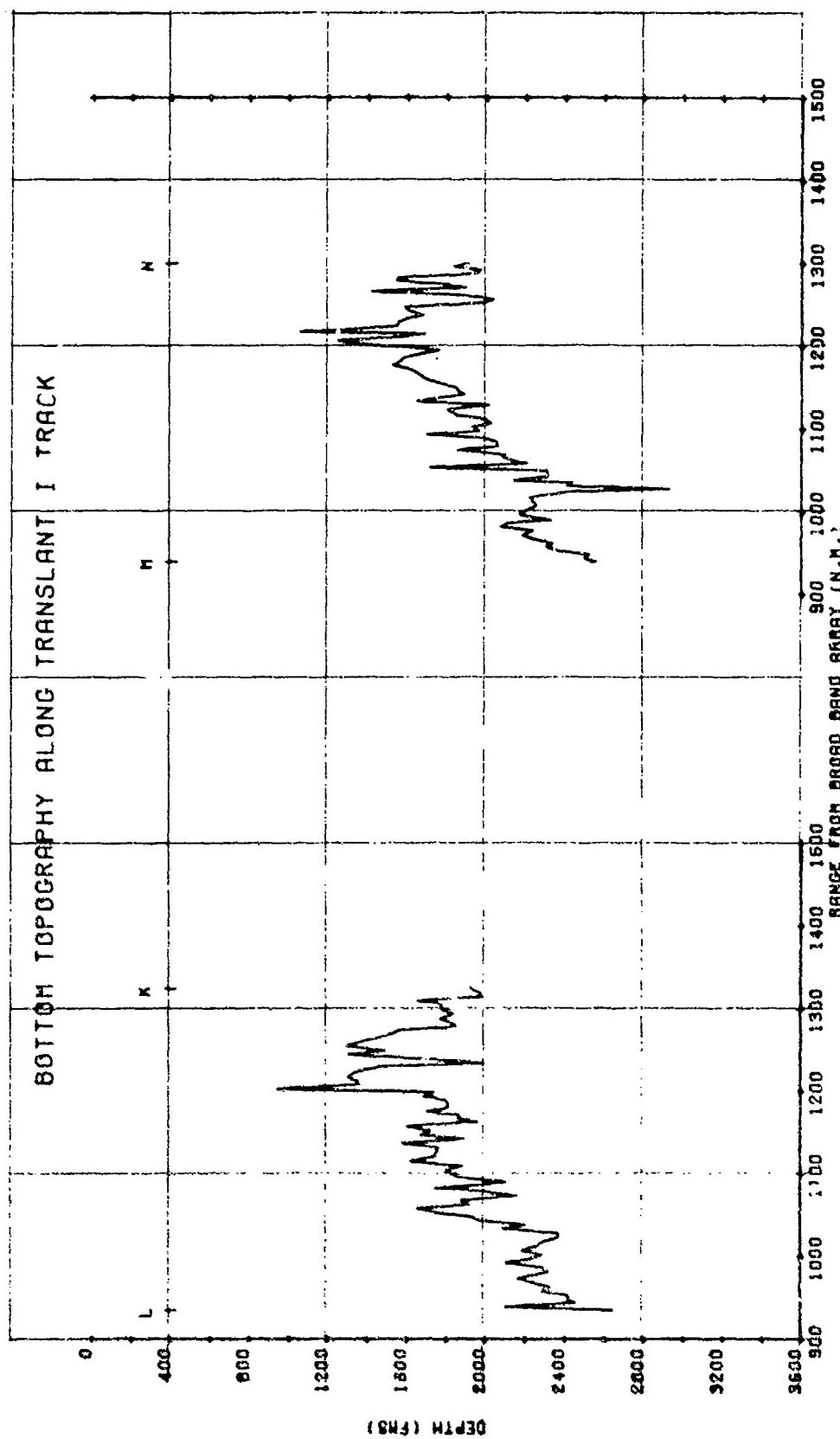


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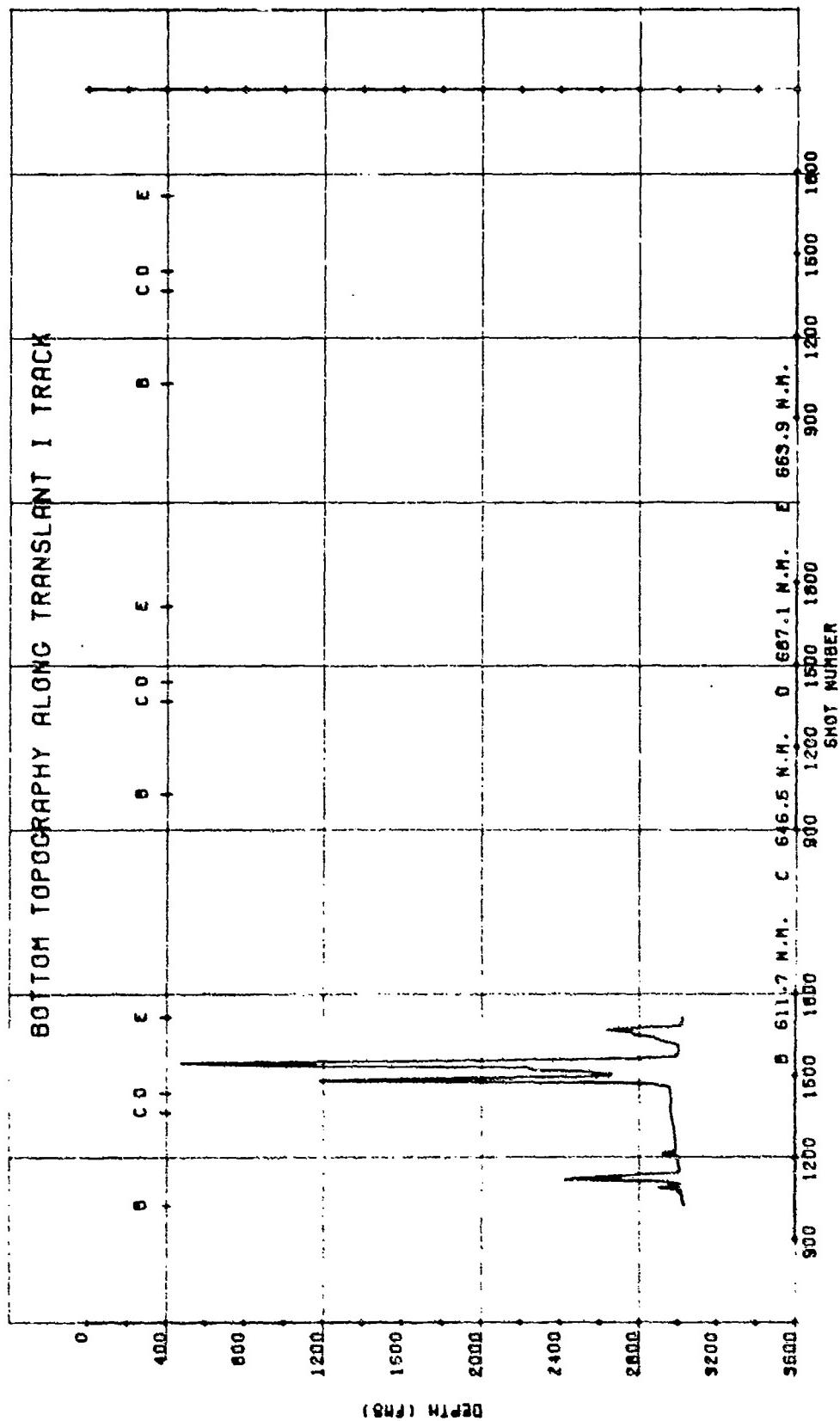


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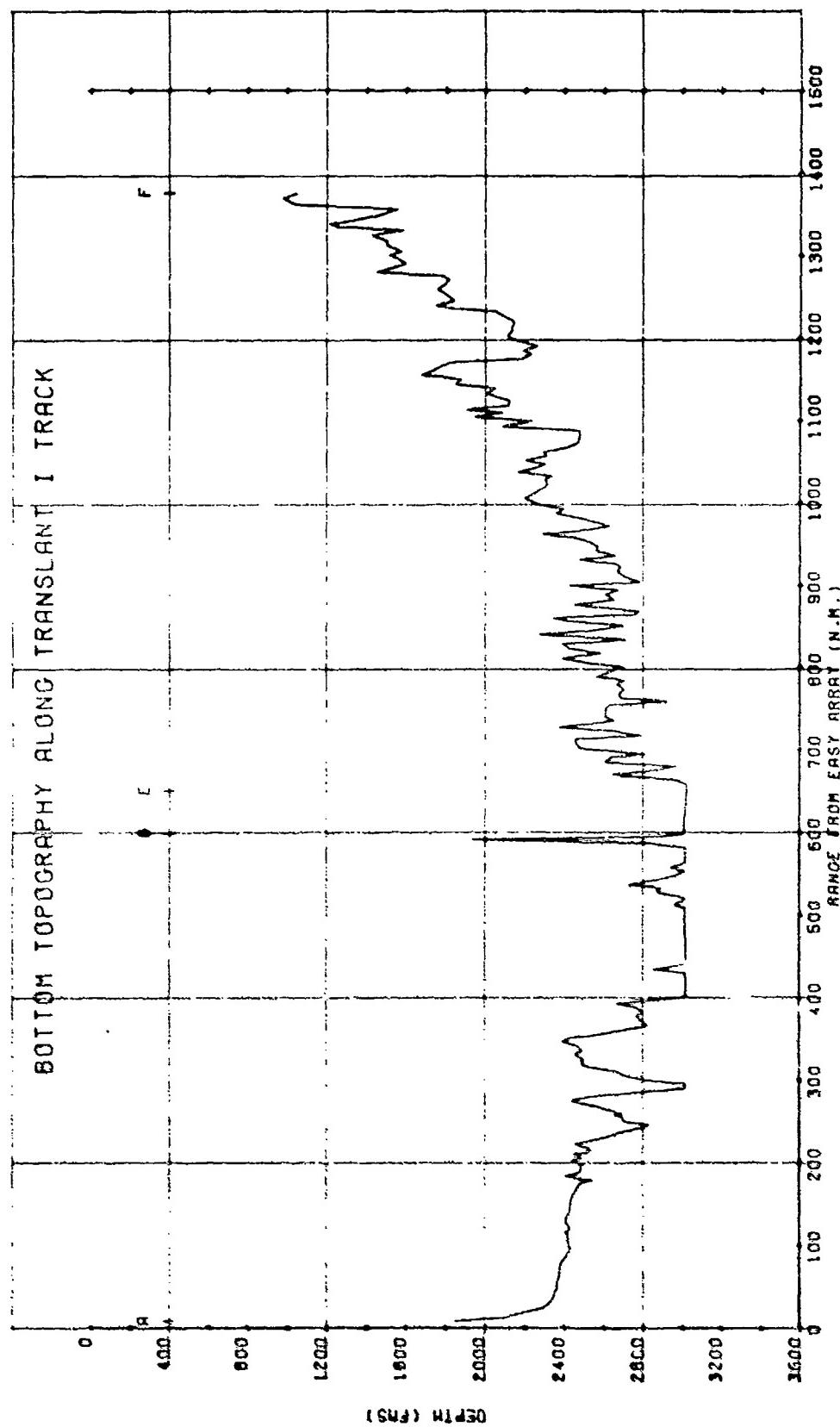
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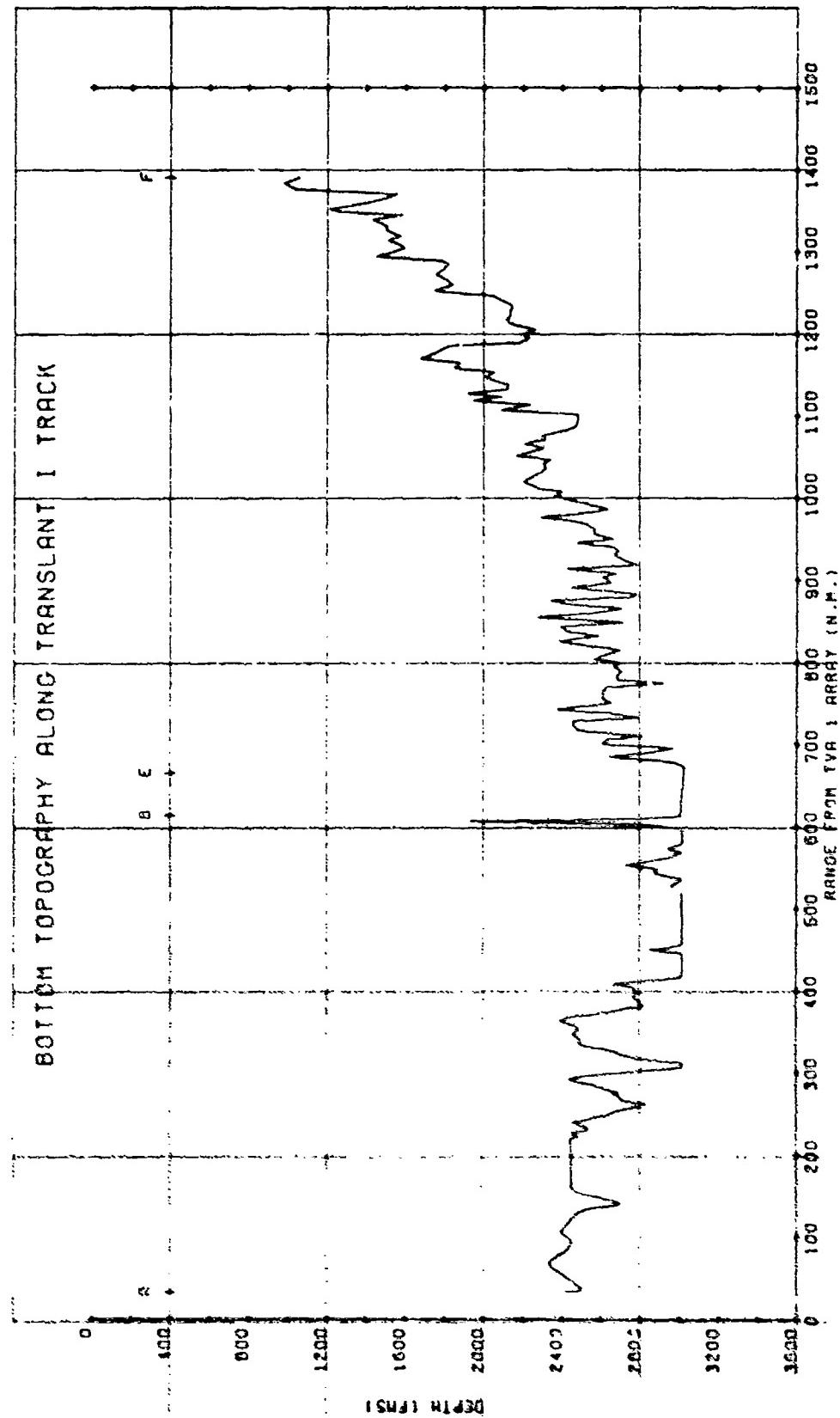


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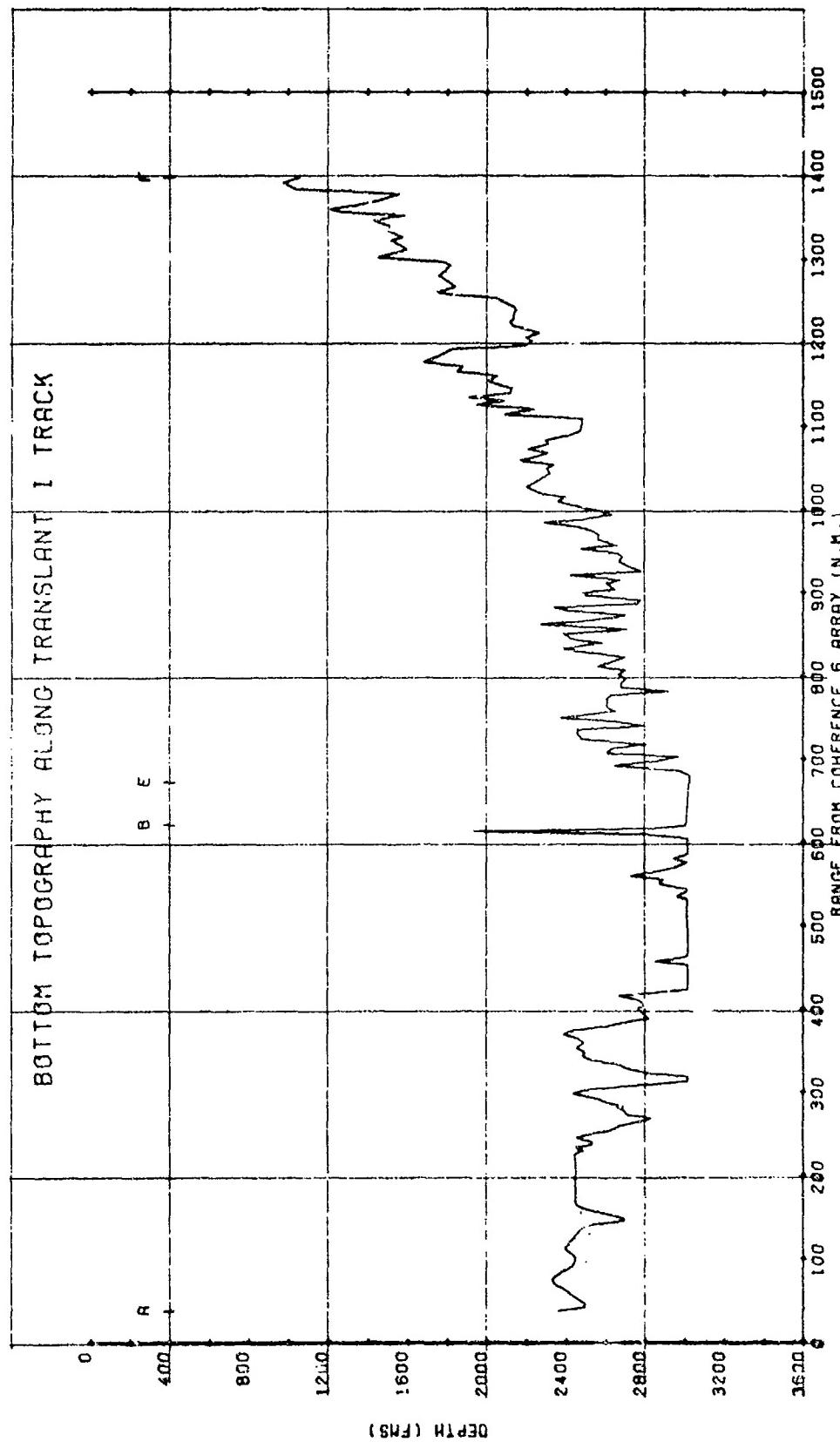


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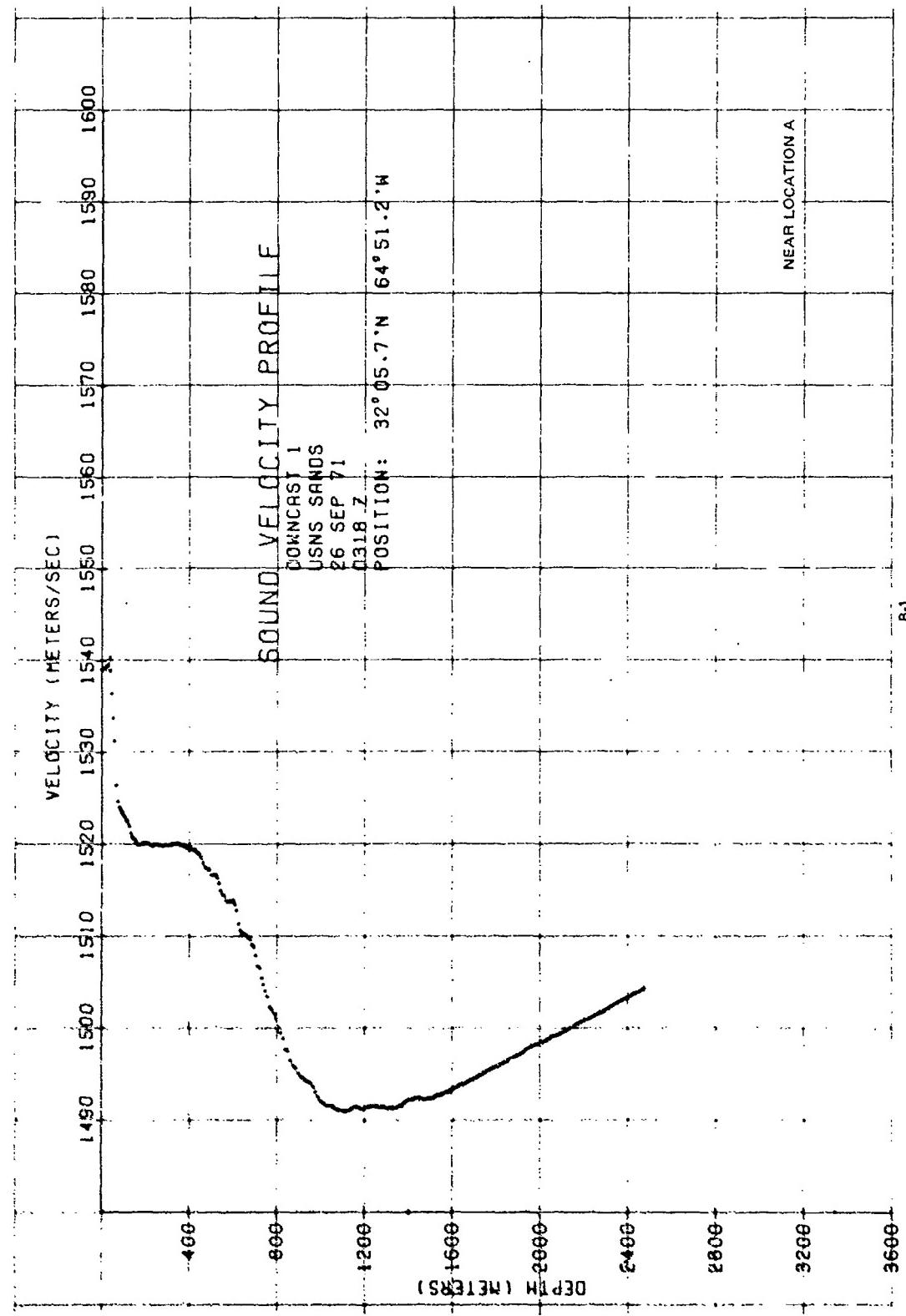
Appendix B
TRANSLANT I SOUND VELOCITY PROFILES

Sound velocity profiles along the TRANSLANT I track are presented on the following pages.

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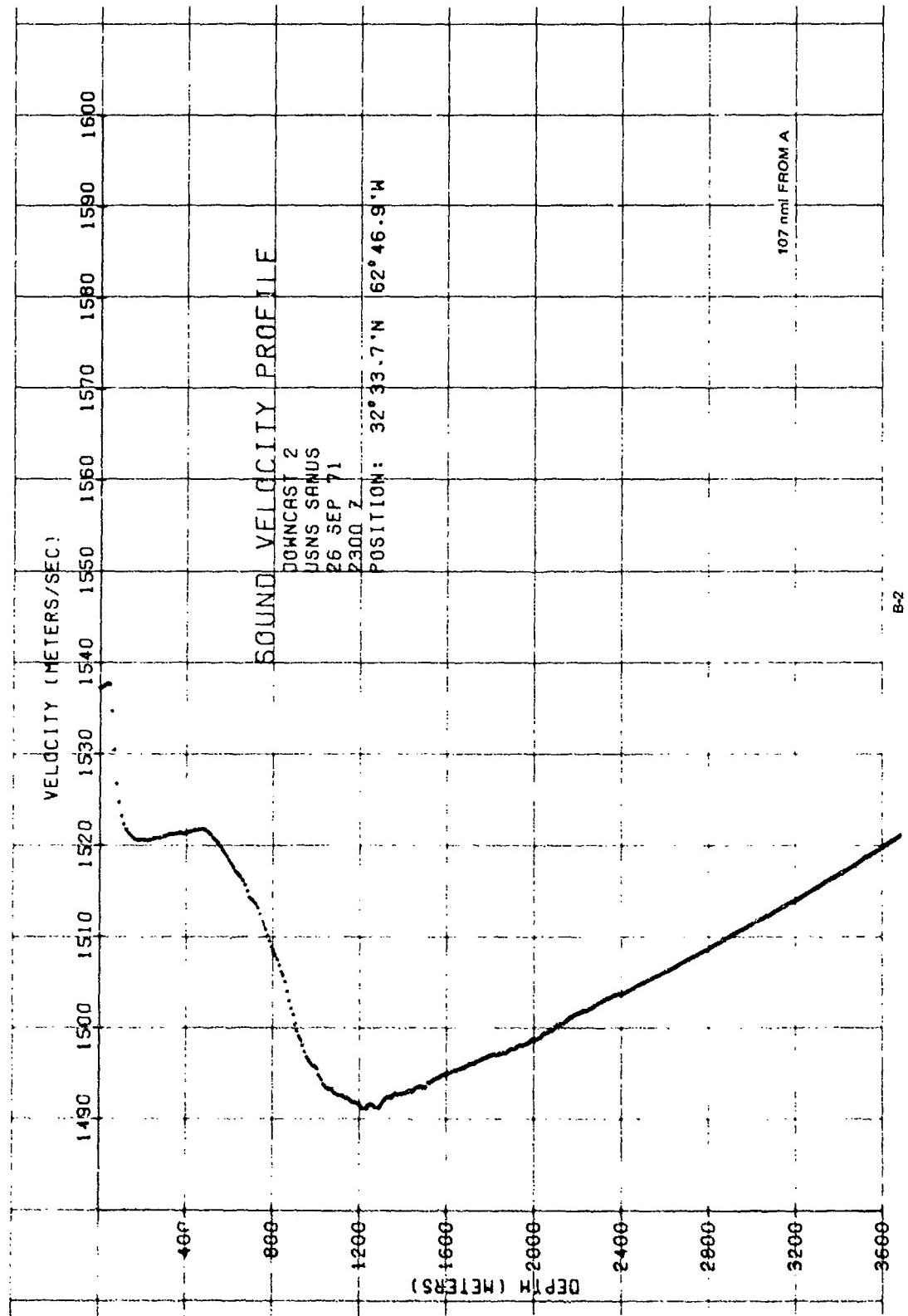
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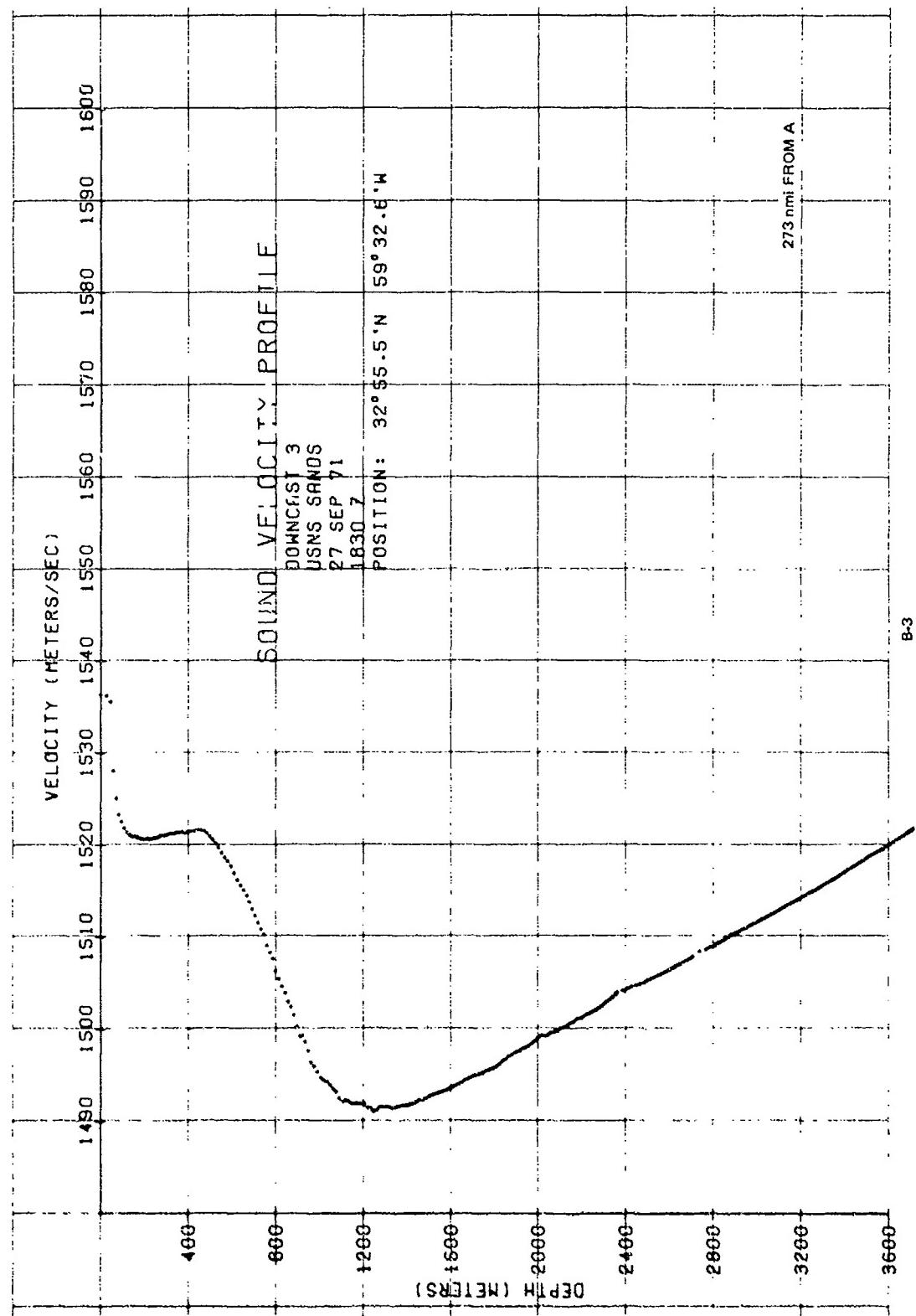
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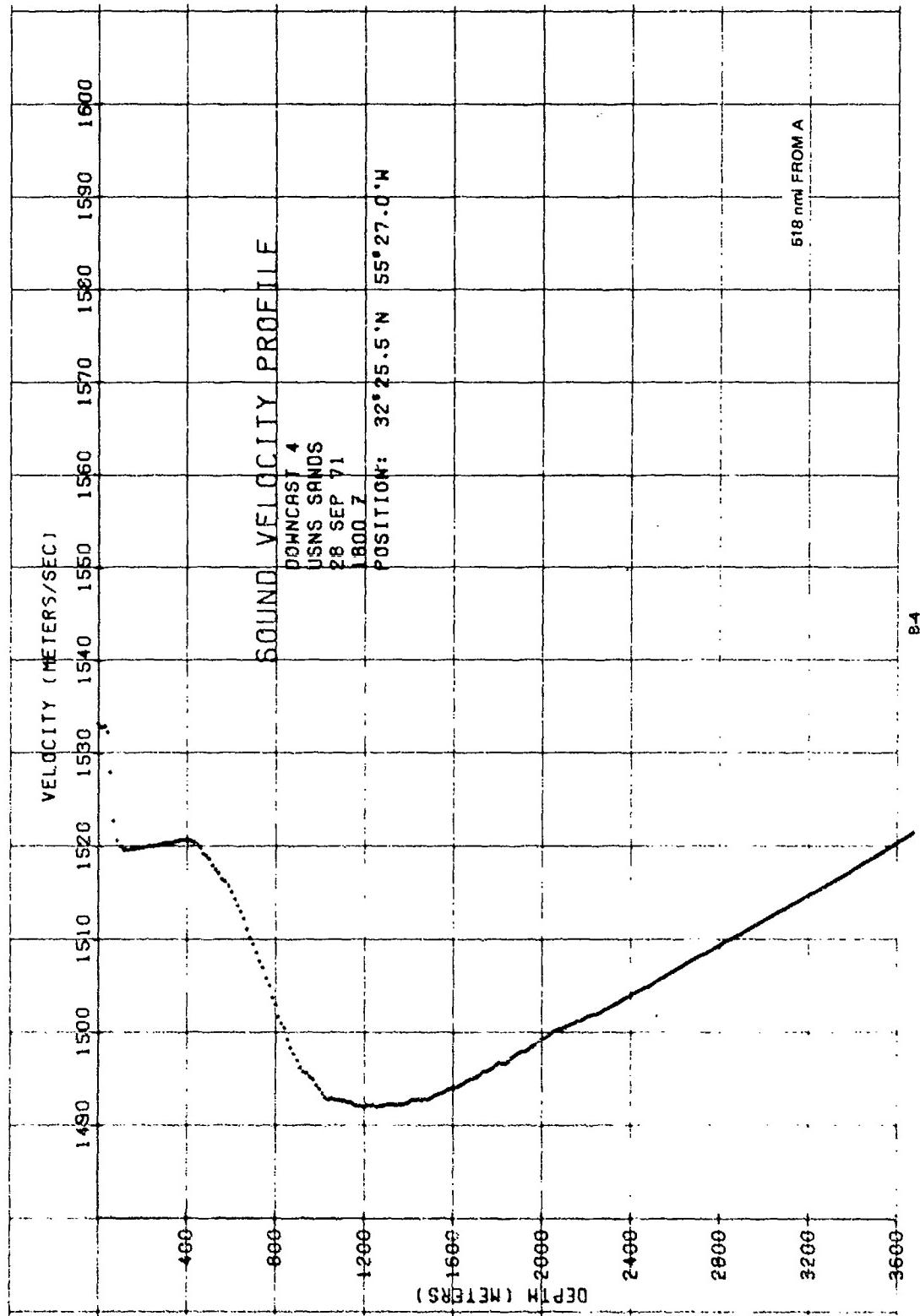
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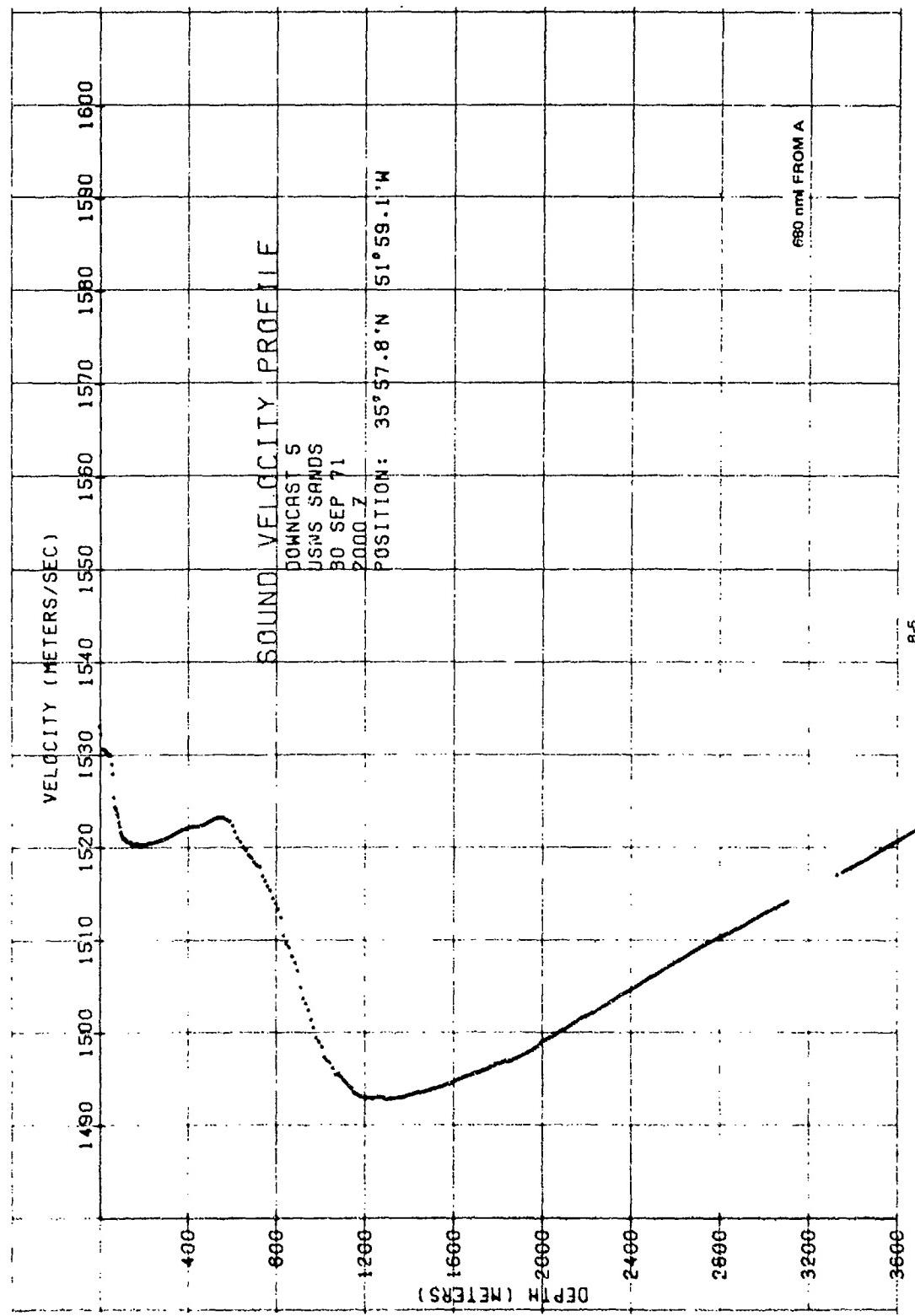
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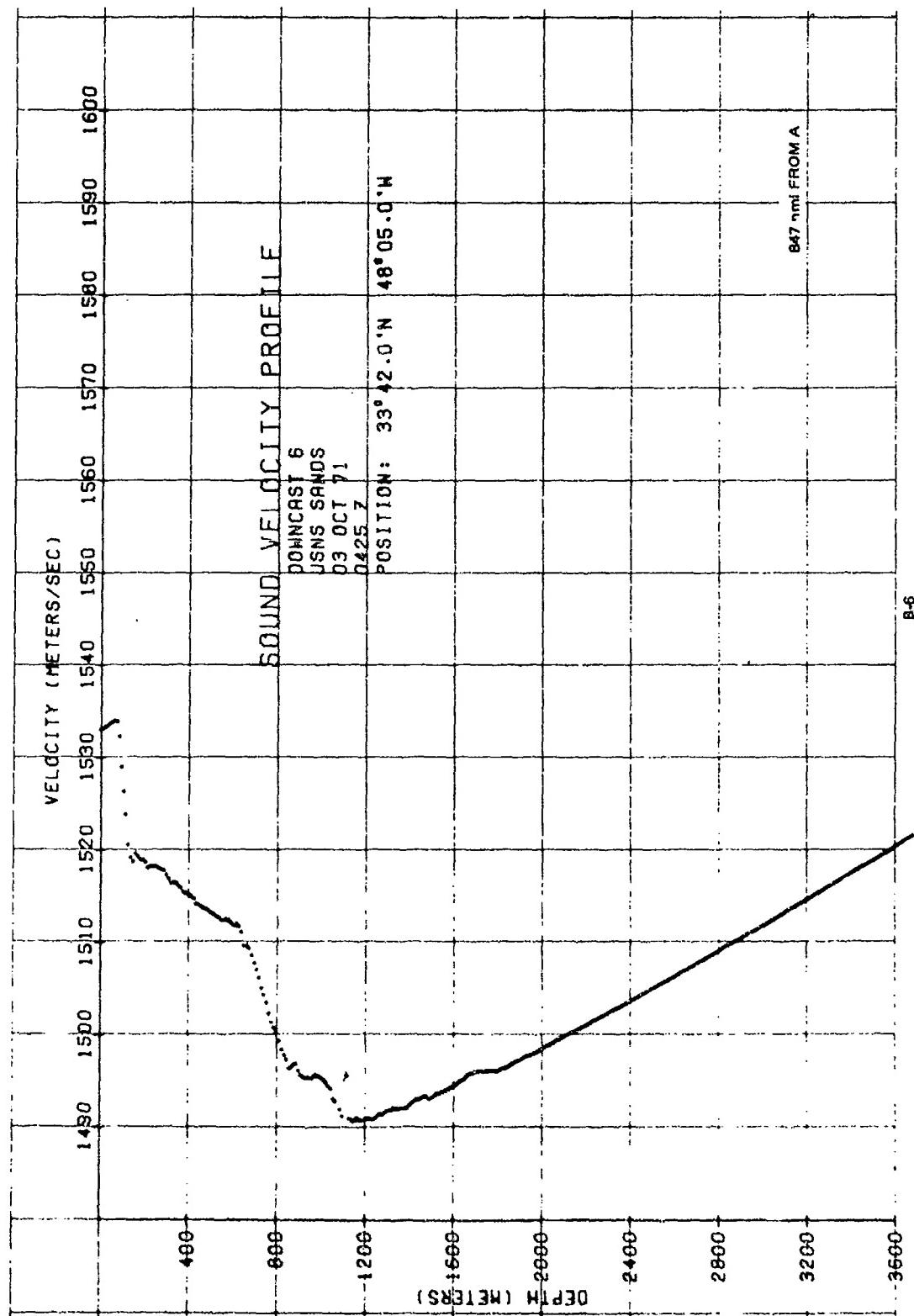
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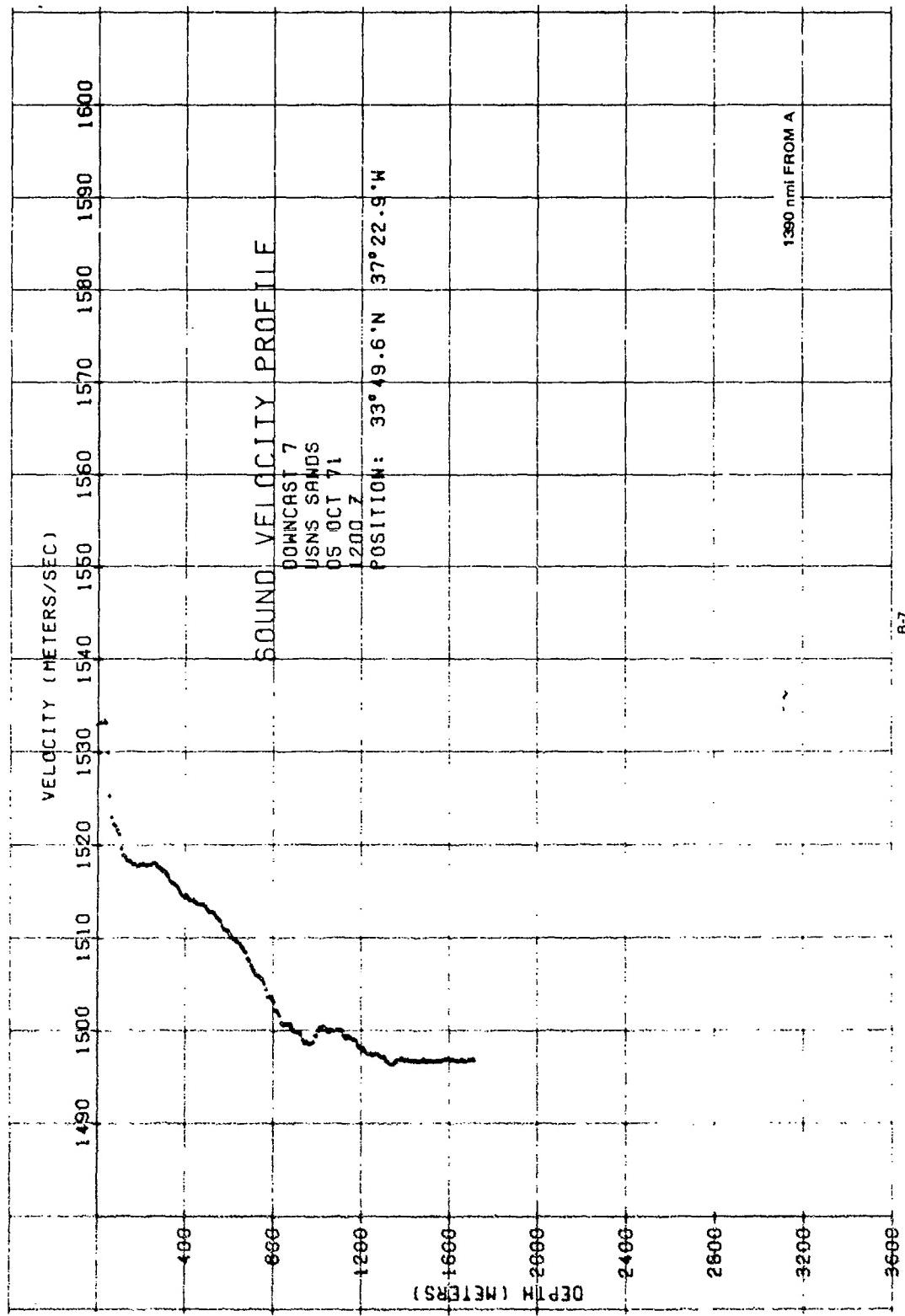
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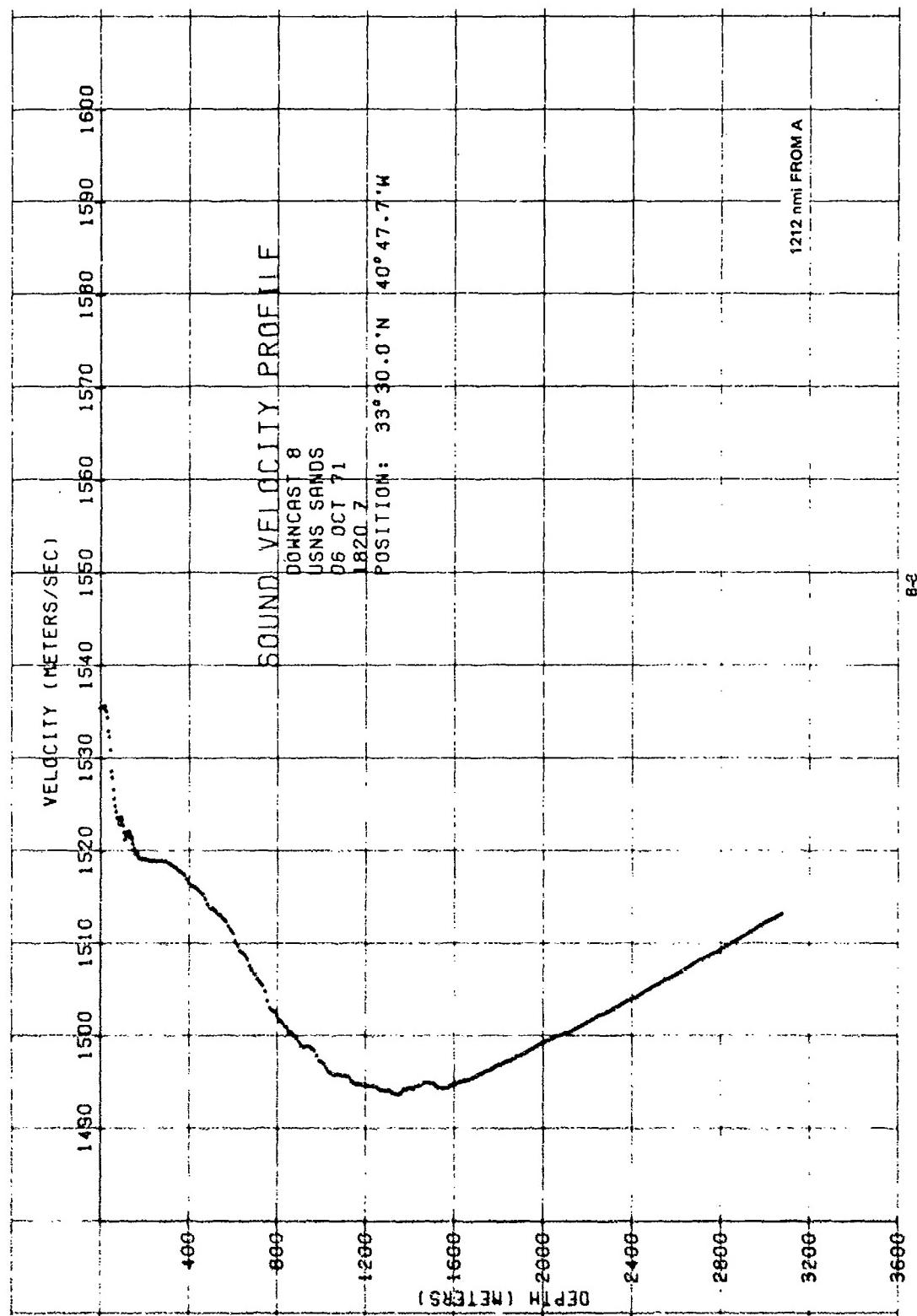
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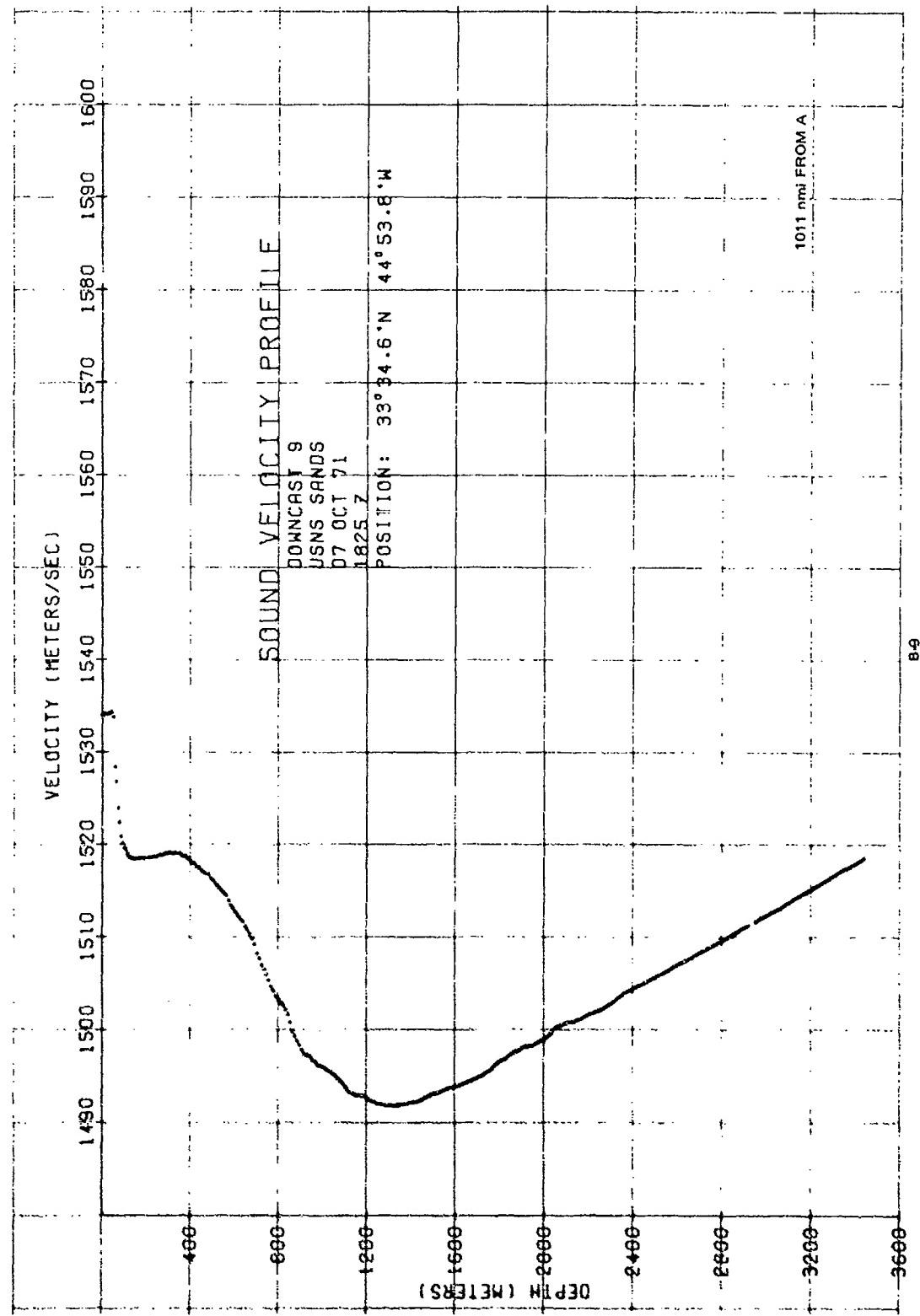
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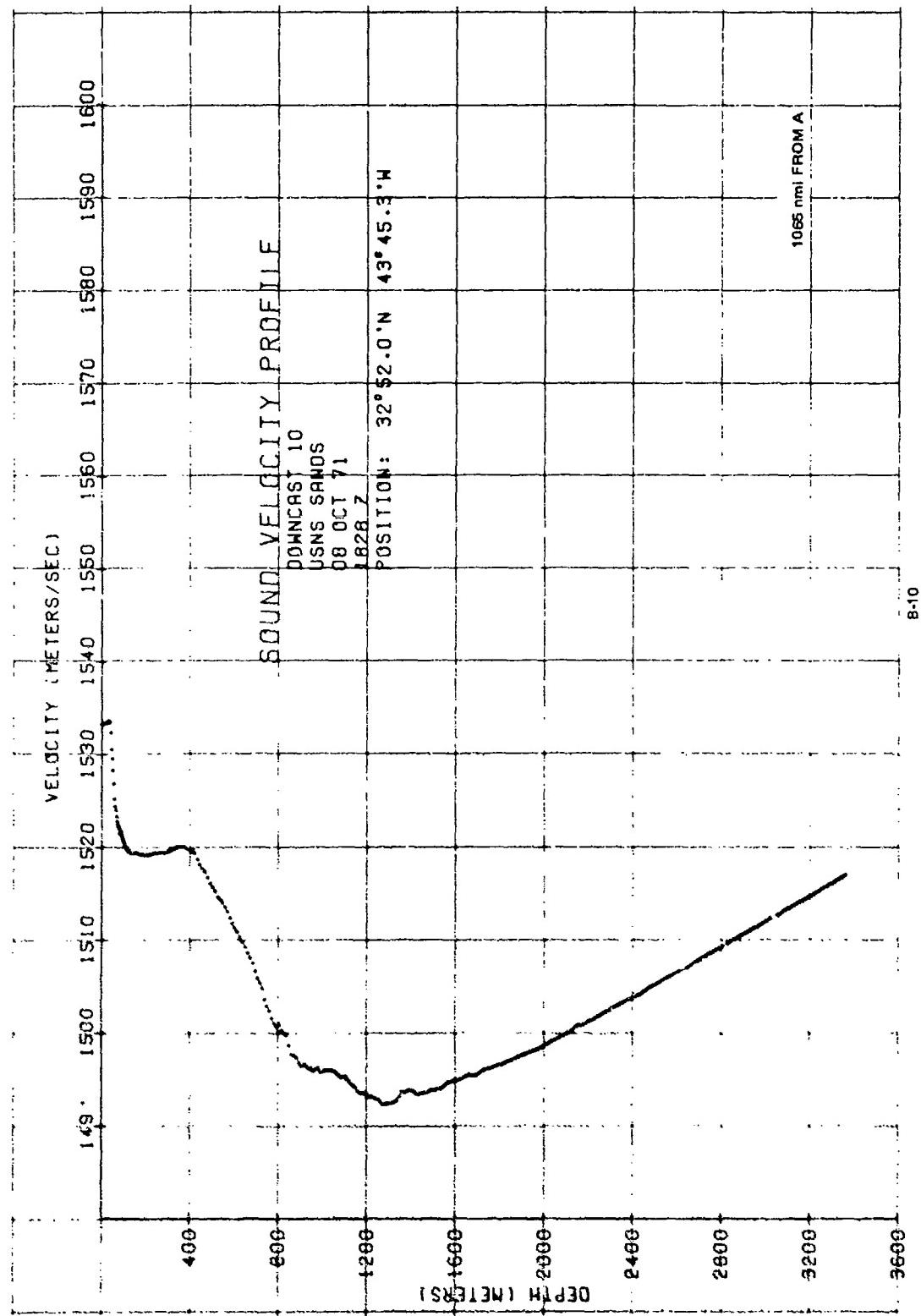
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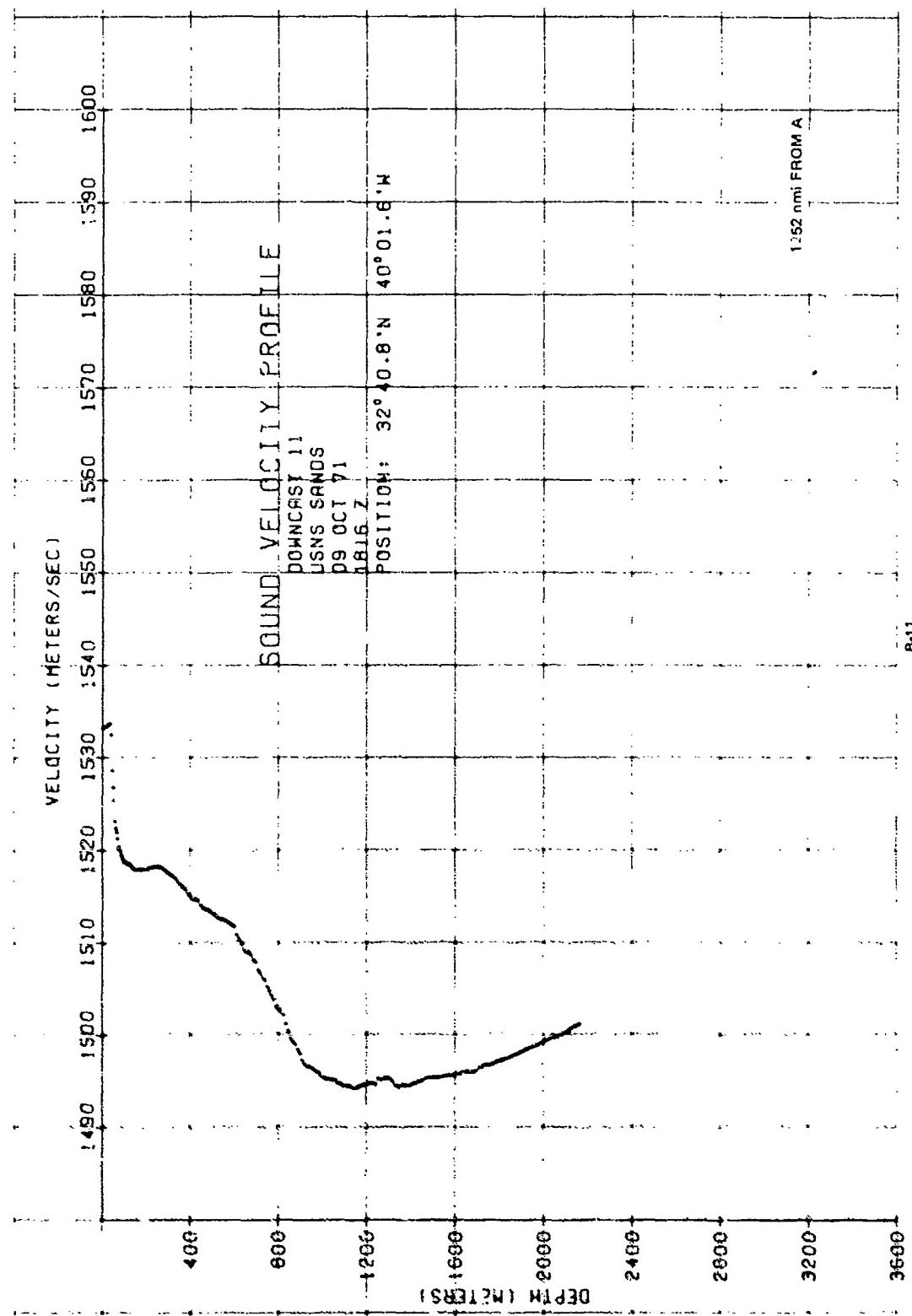


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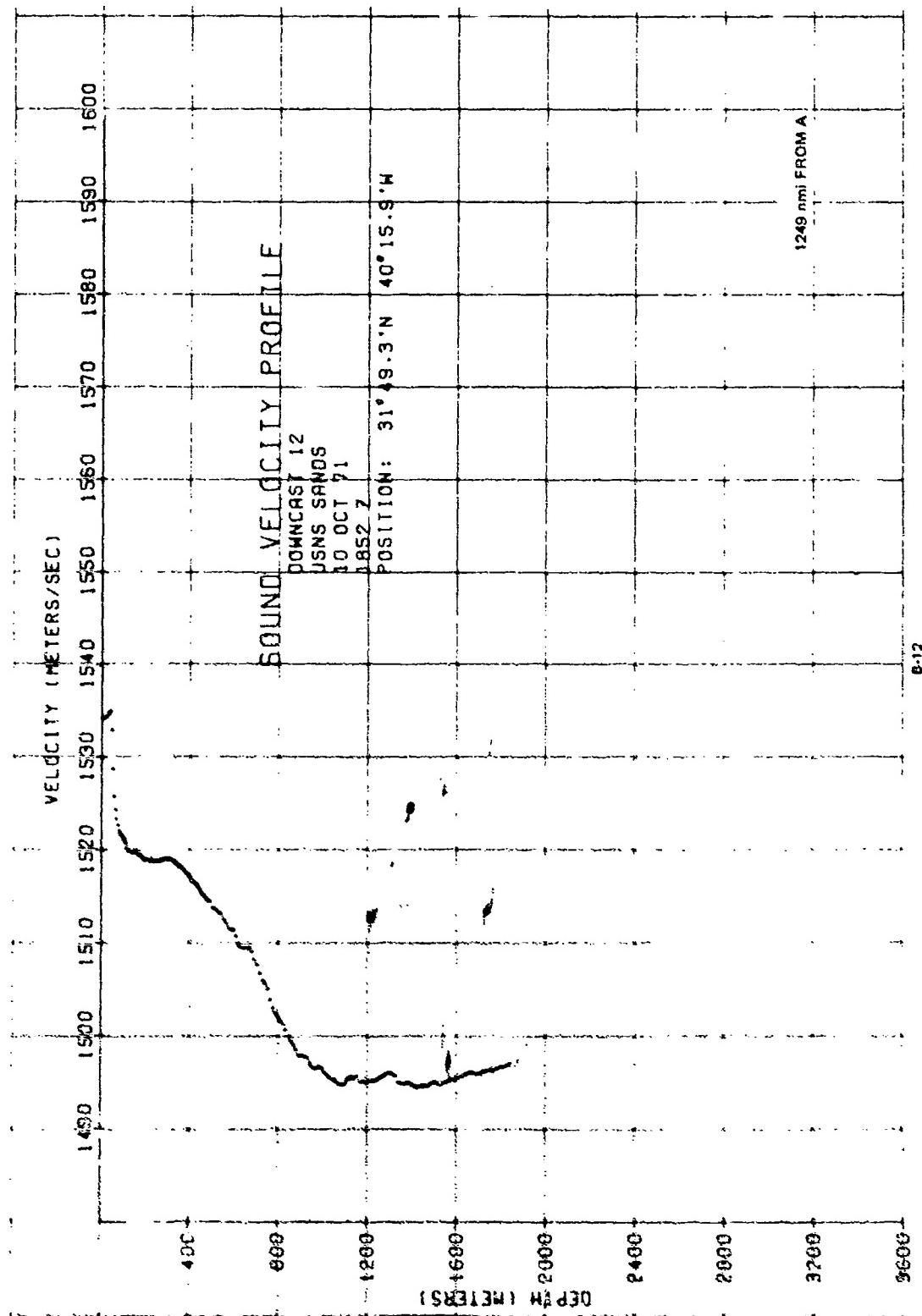


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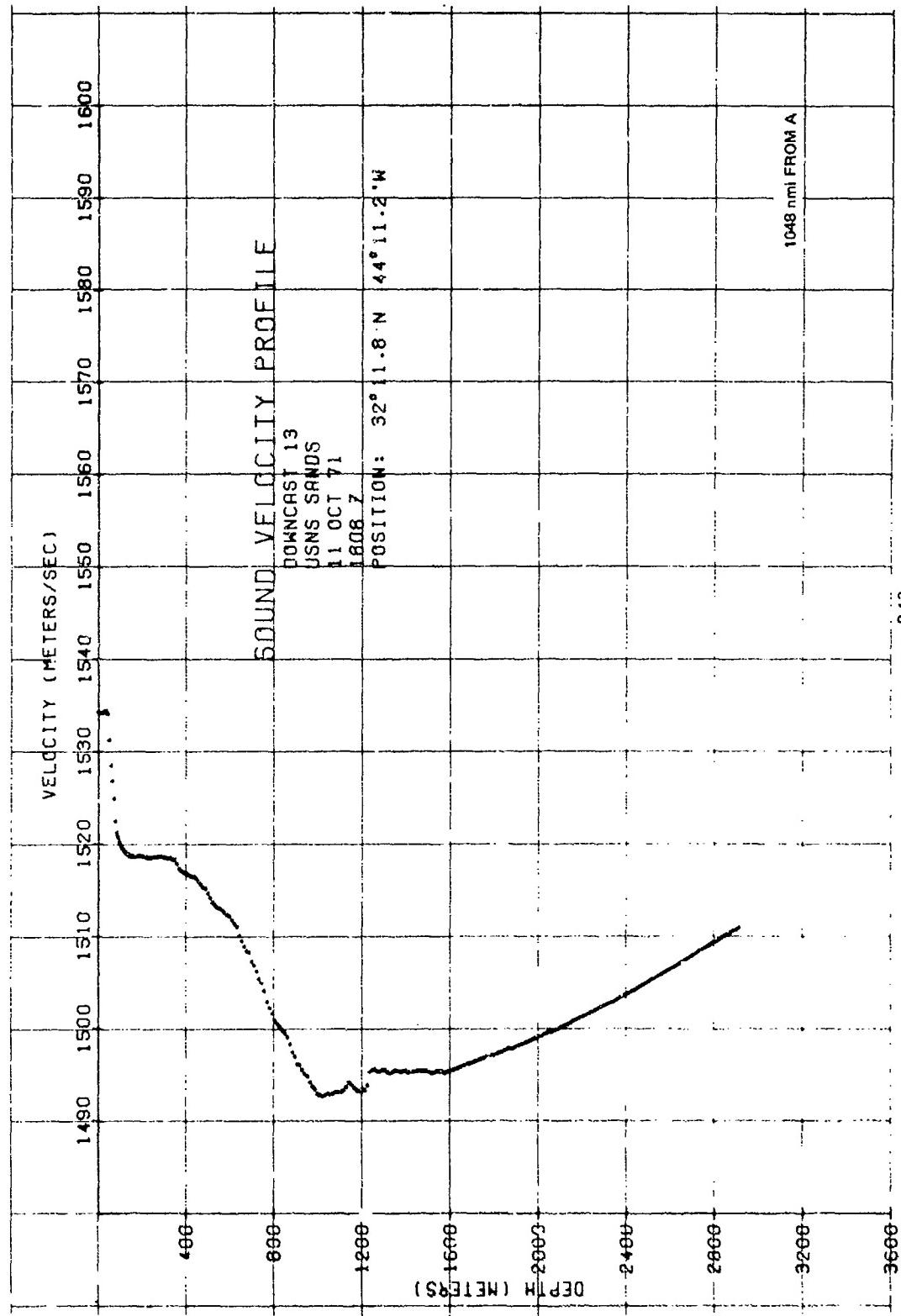
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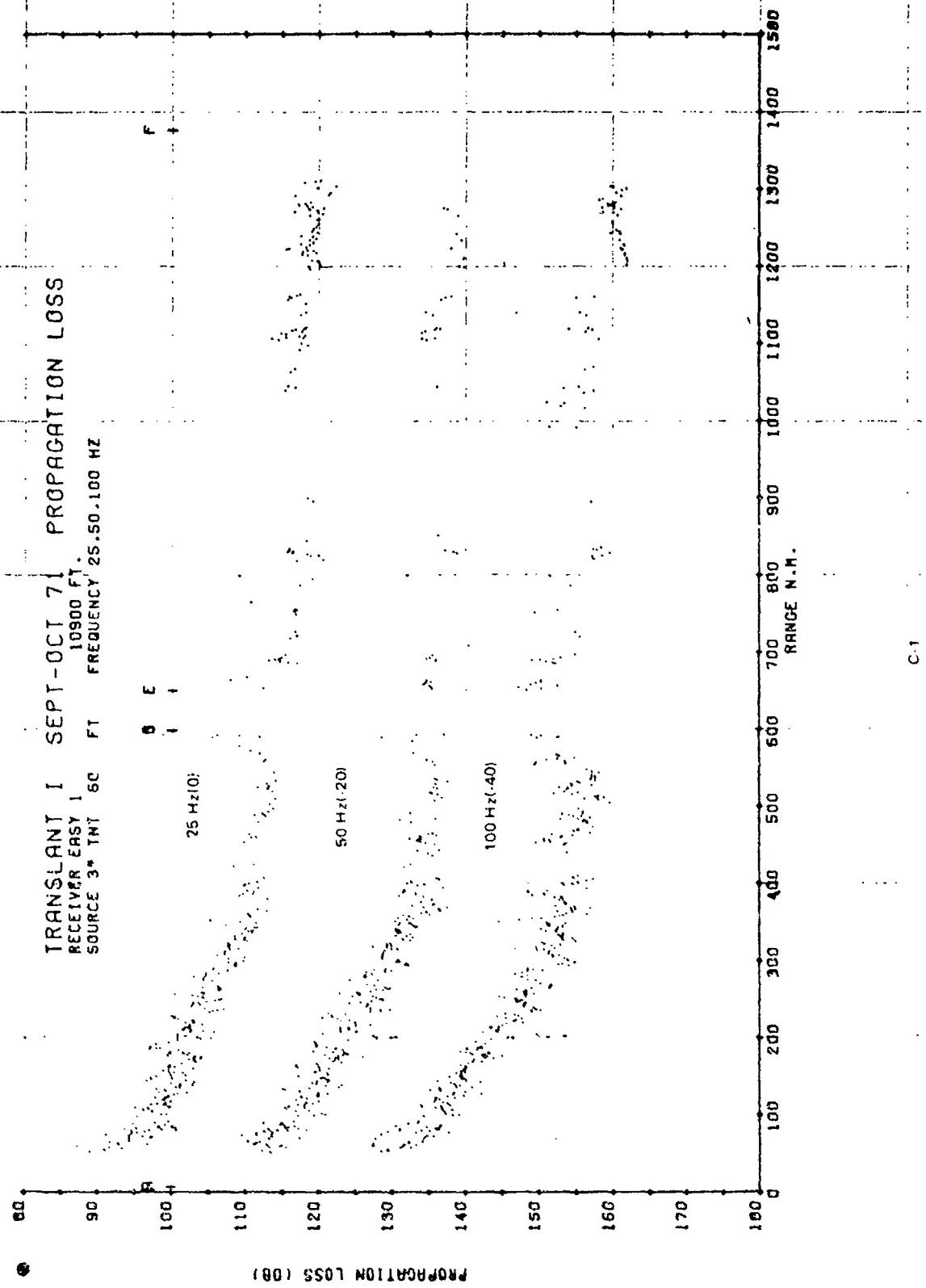
Appendix C
TRANSLANT I PROPAGATION LOSS

(U) The measured propagation loss for the TRANSLANT I experiment as a function of range and frequency are presented on the following pages.

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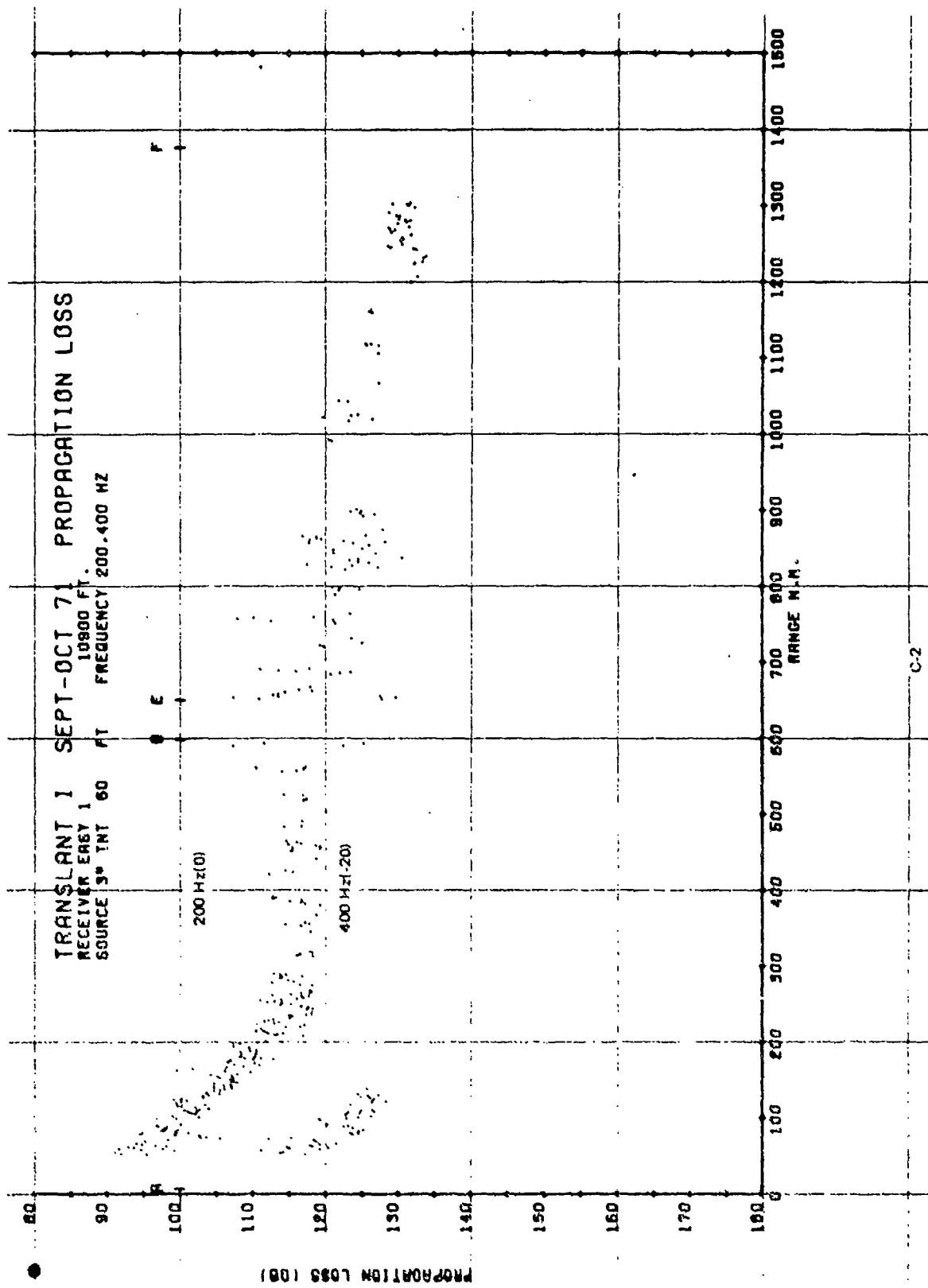


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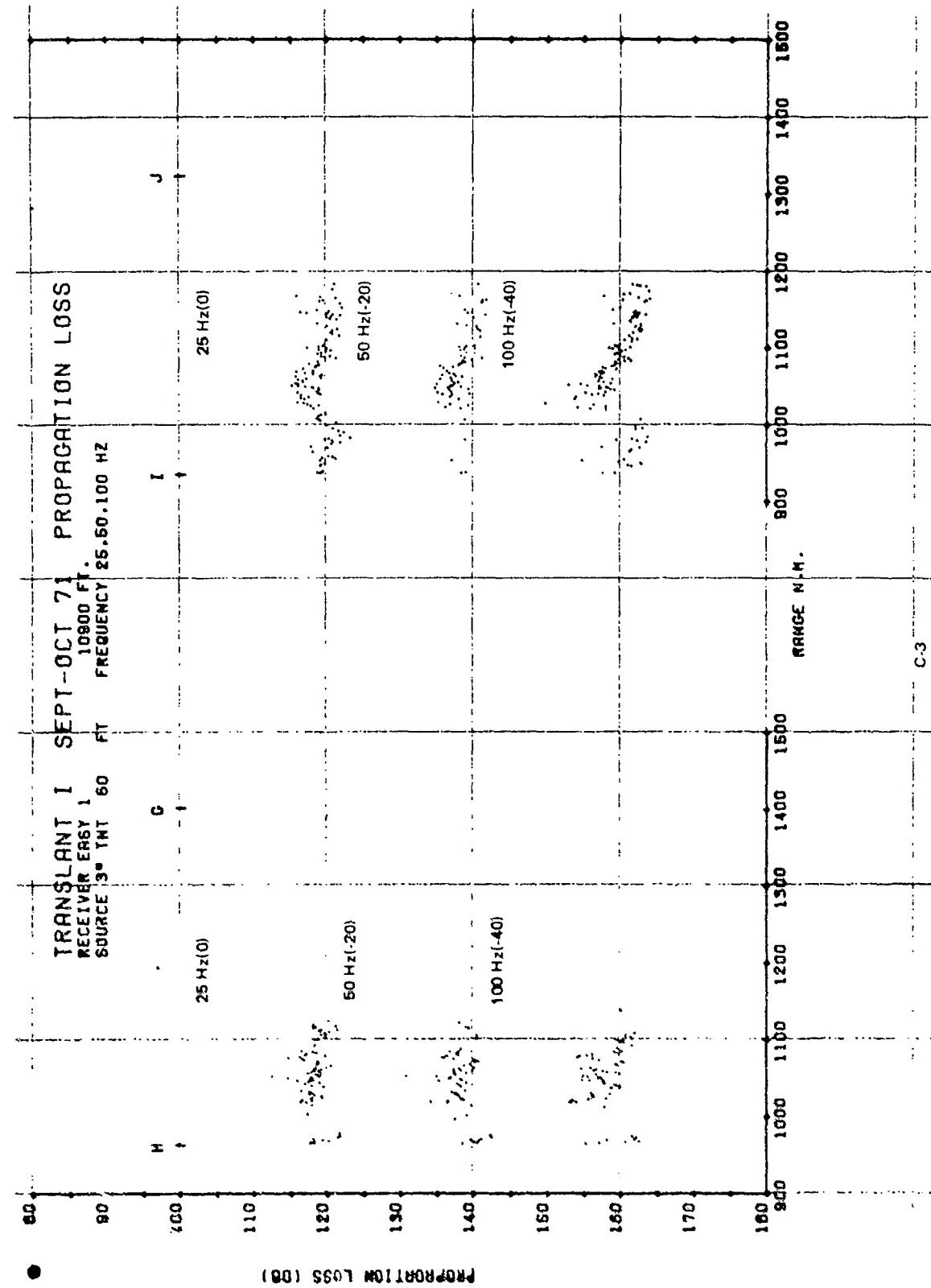
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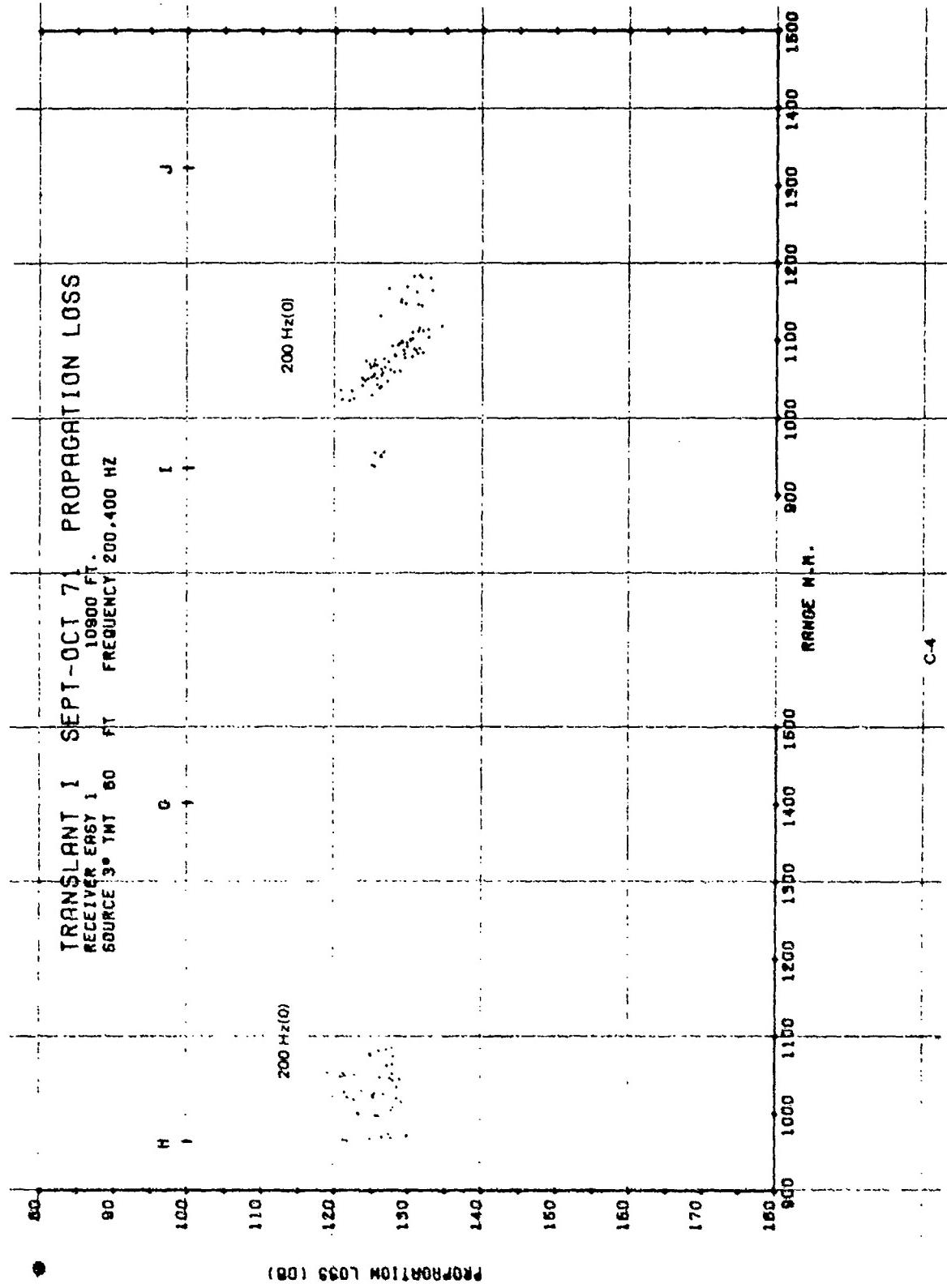
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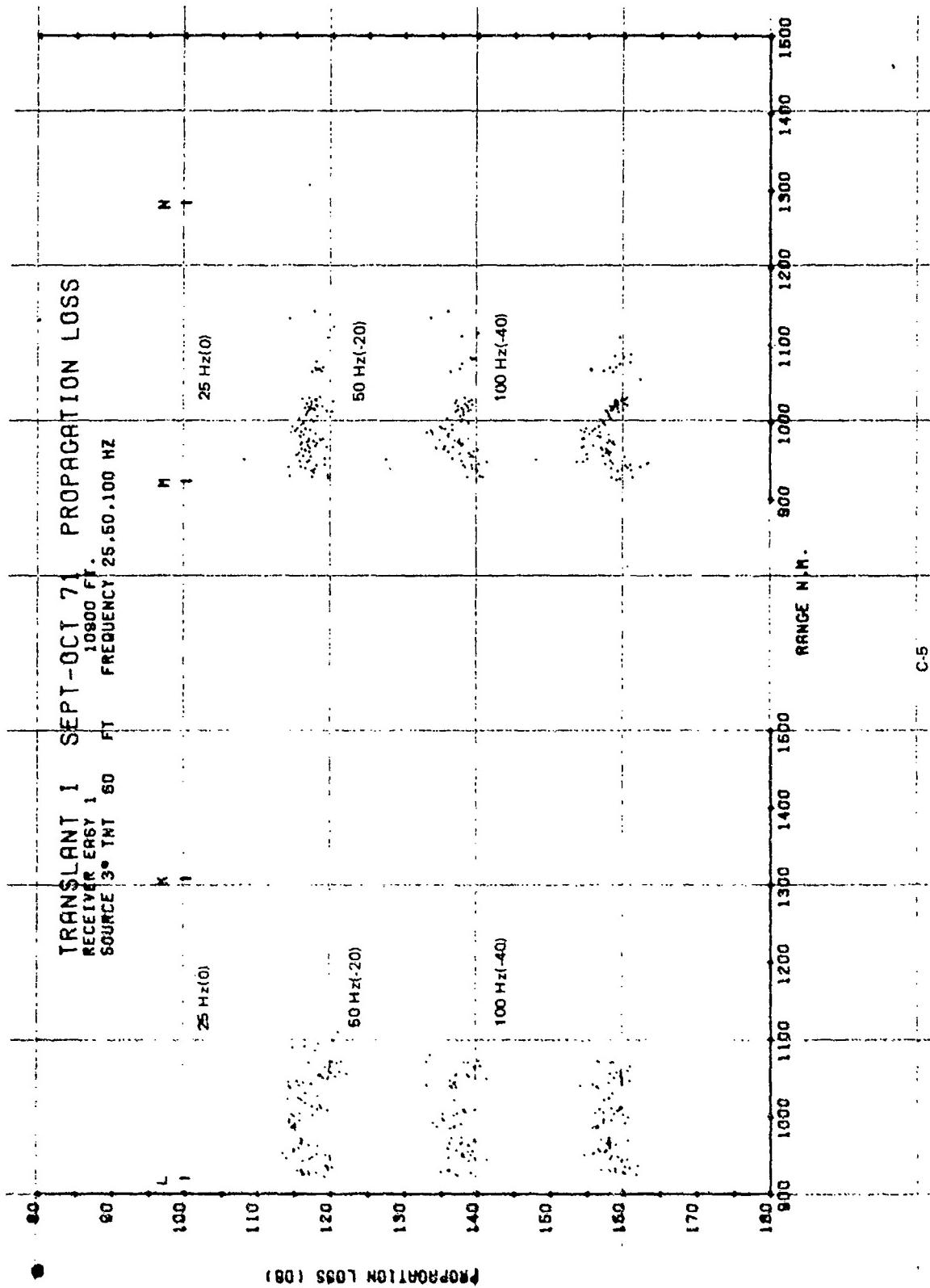
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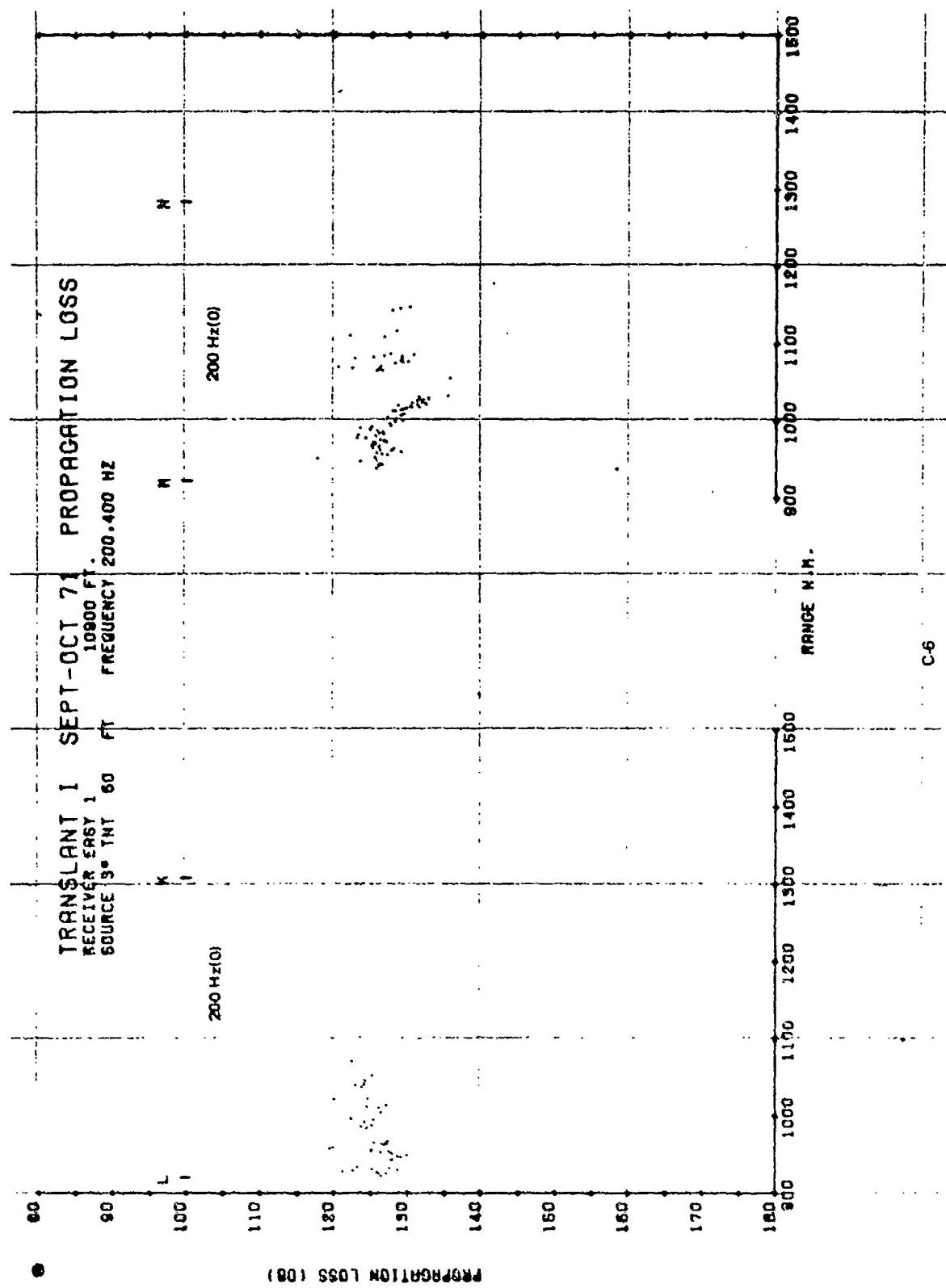
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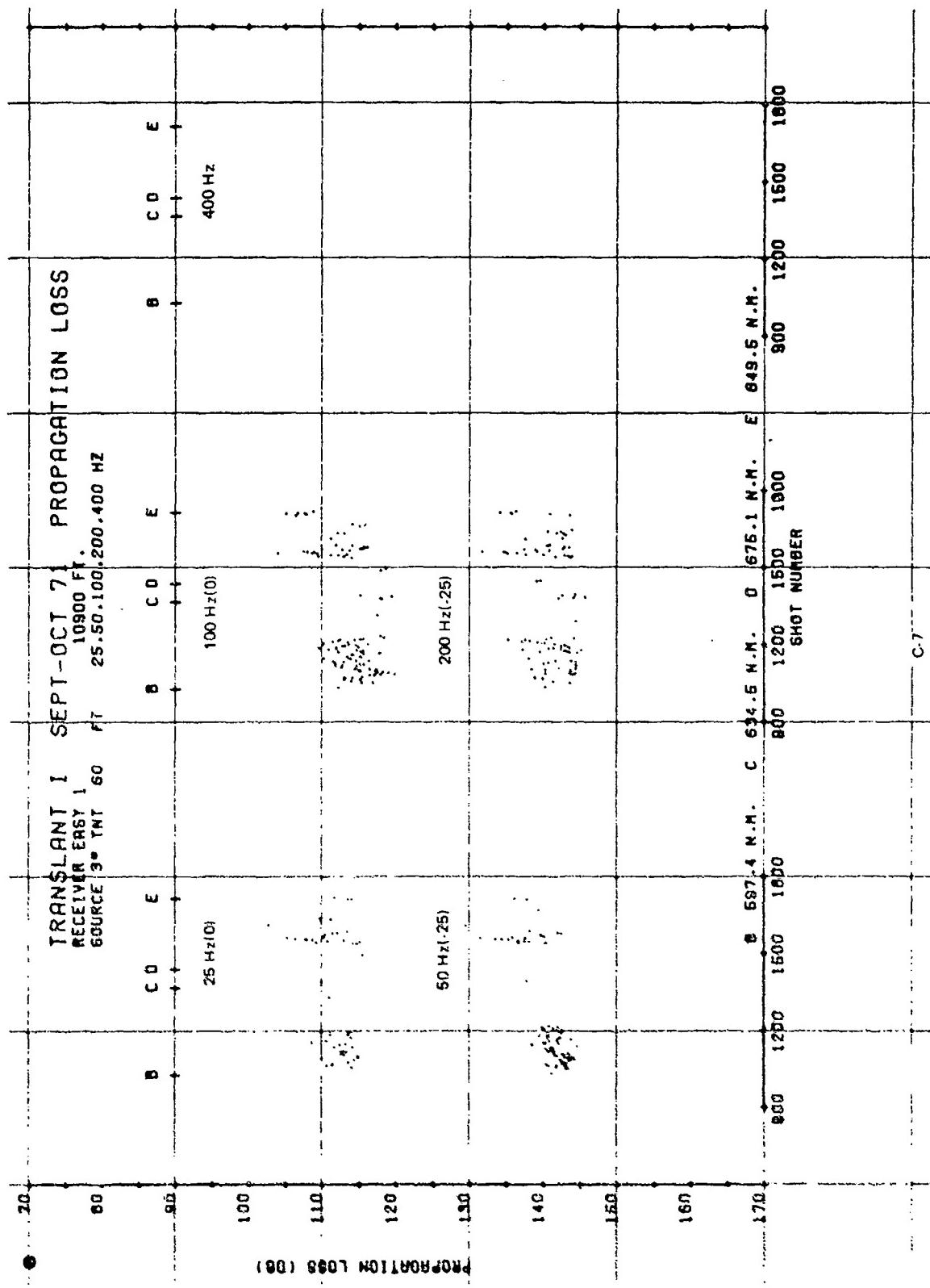
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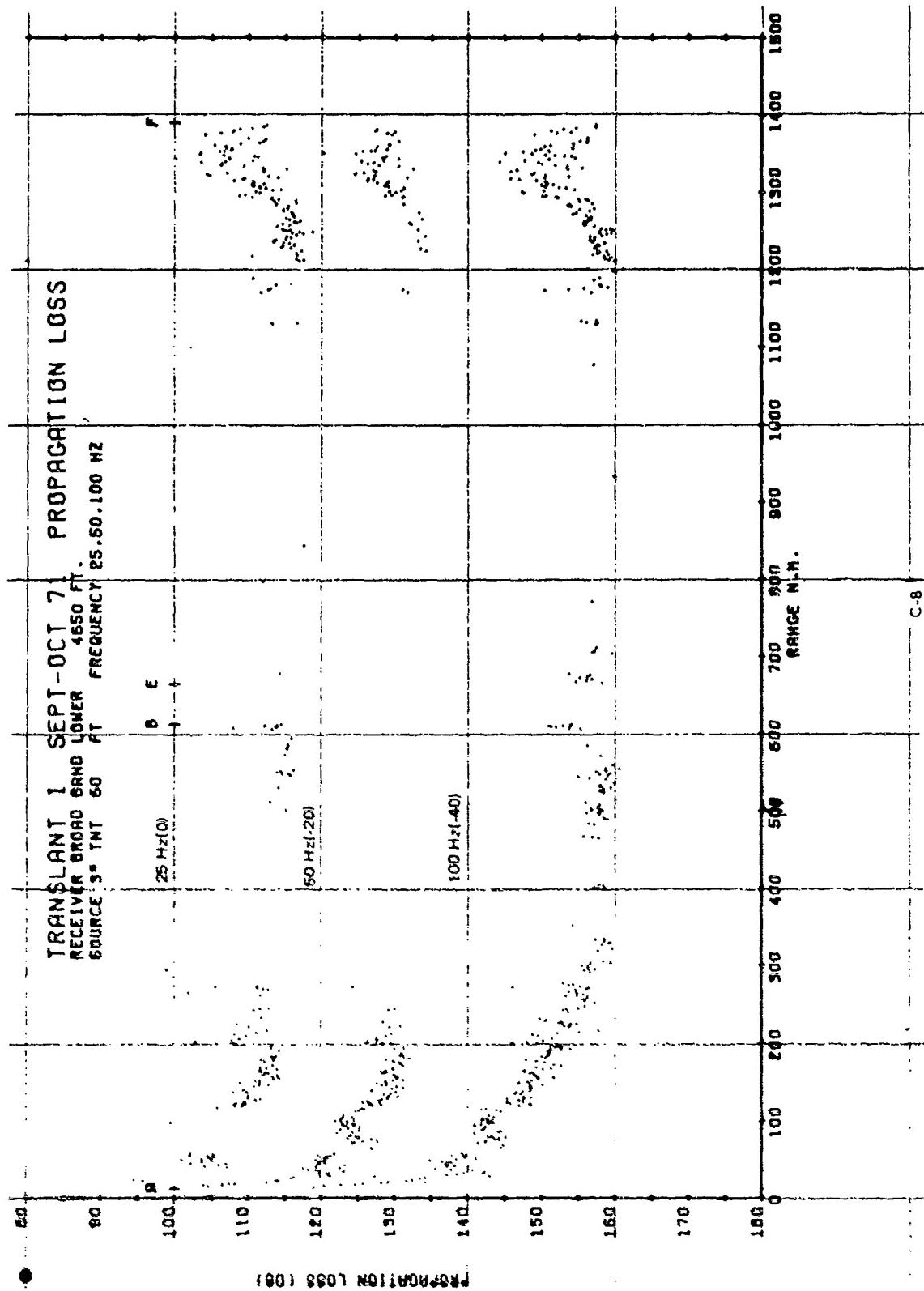
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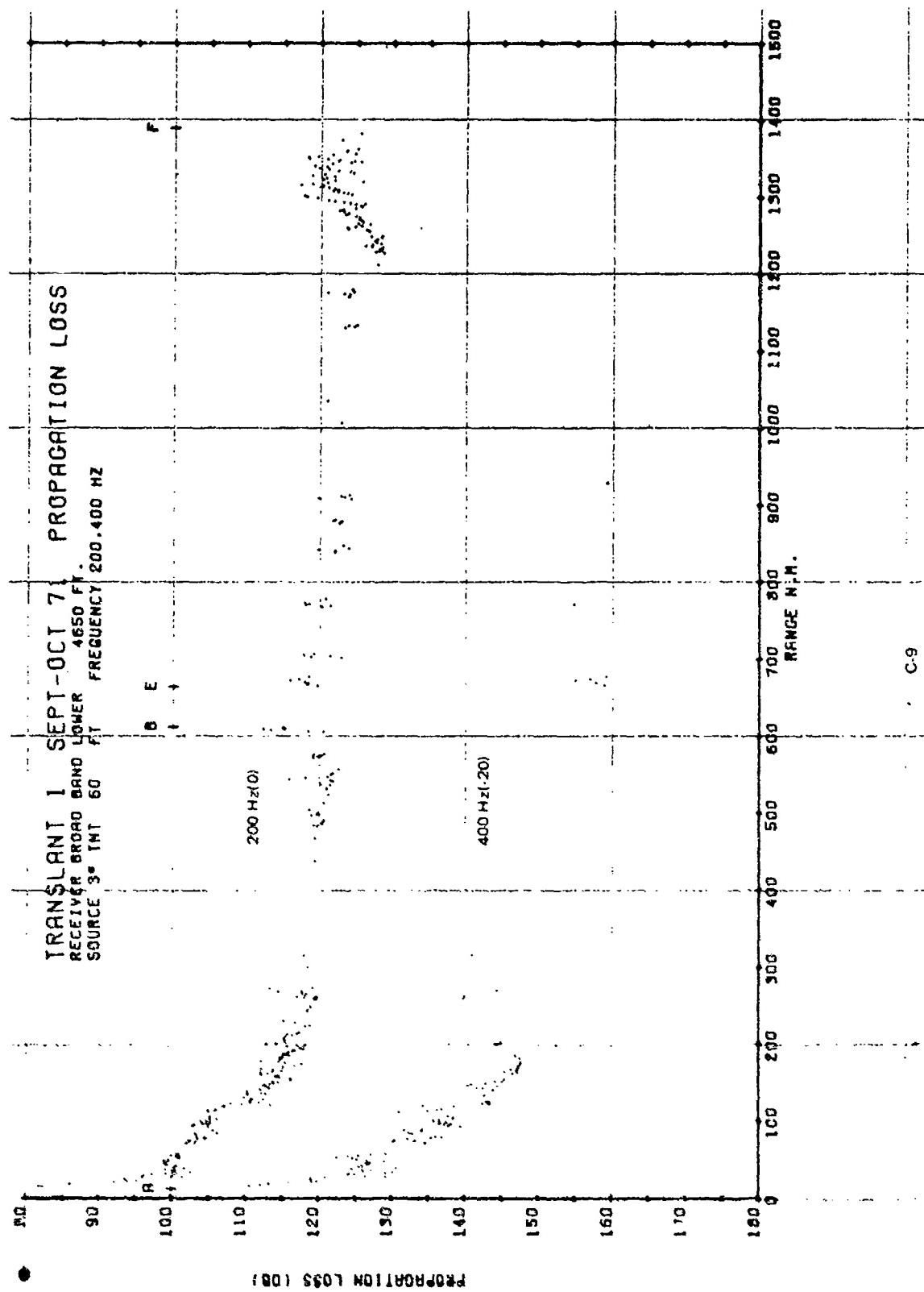
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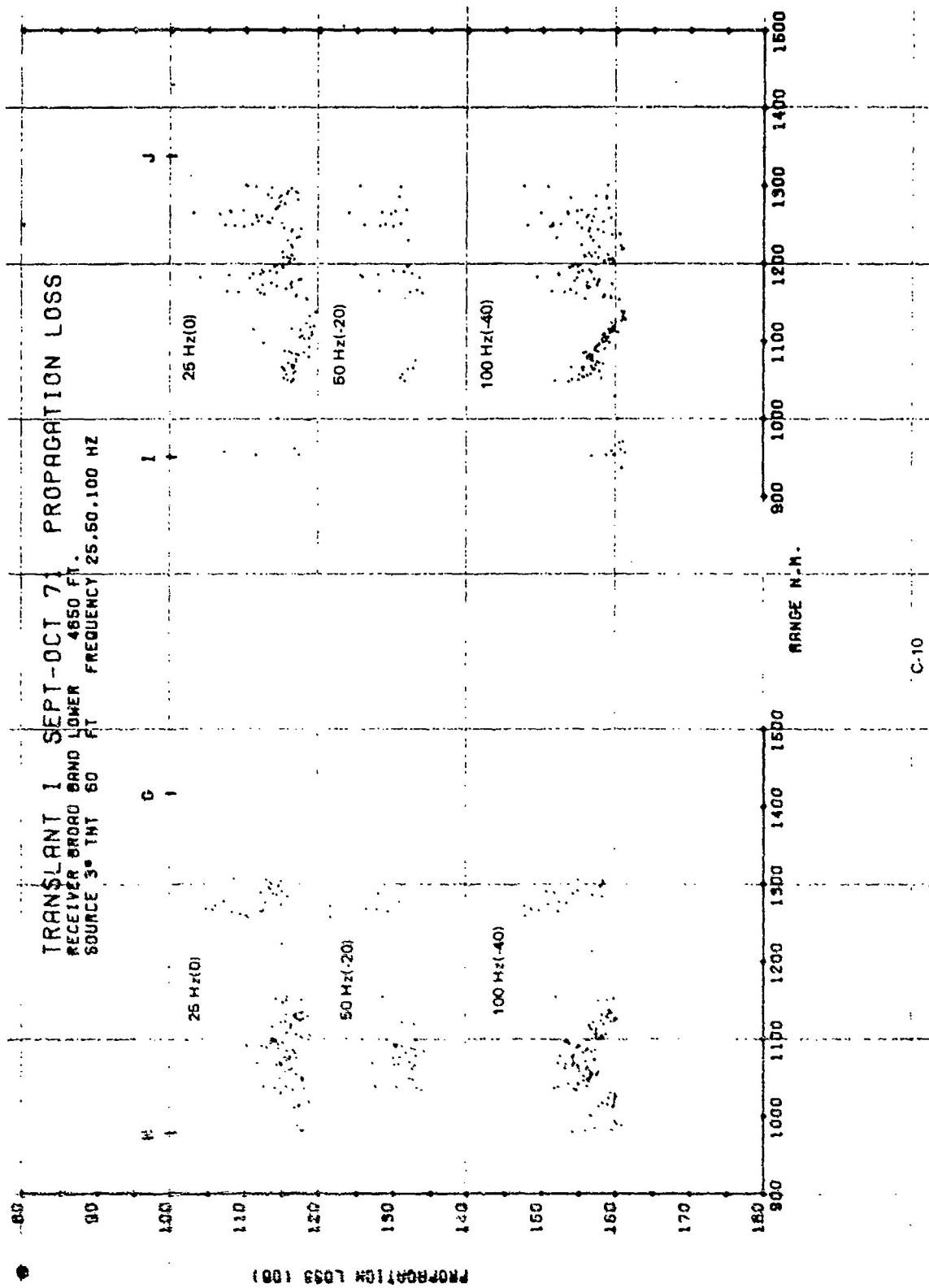
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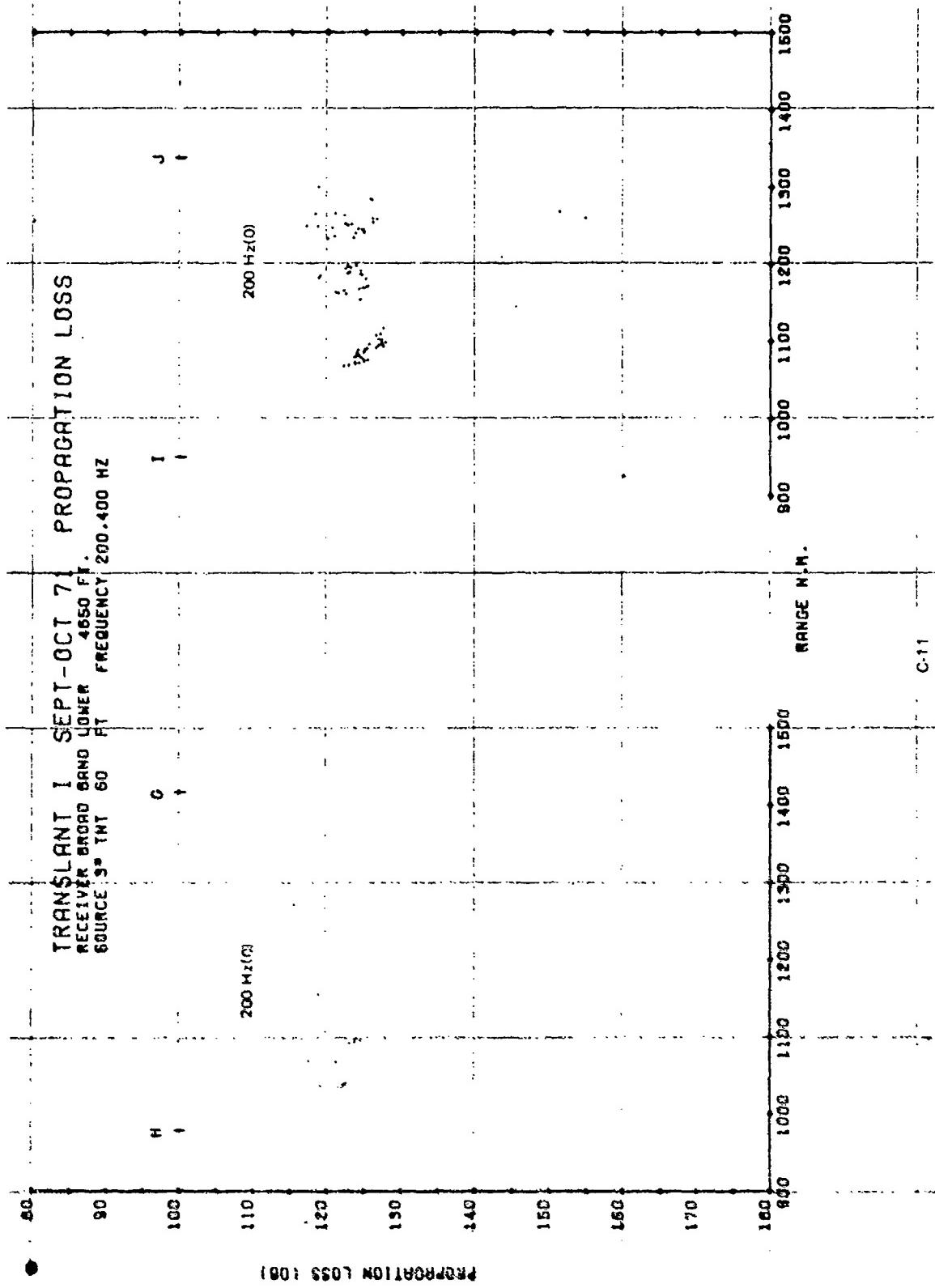
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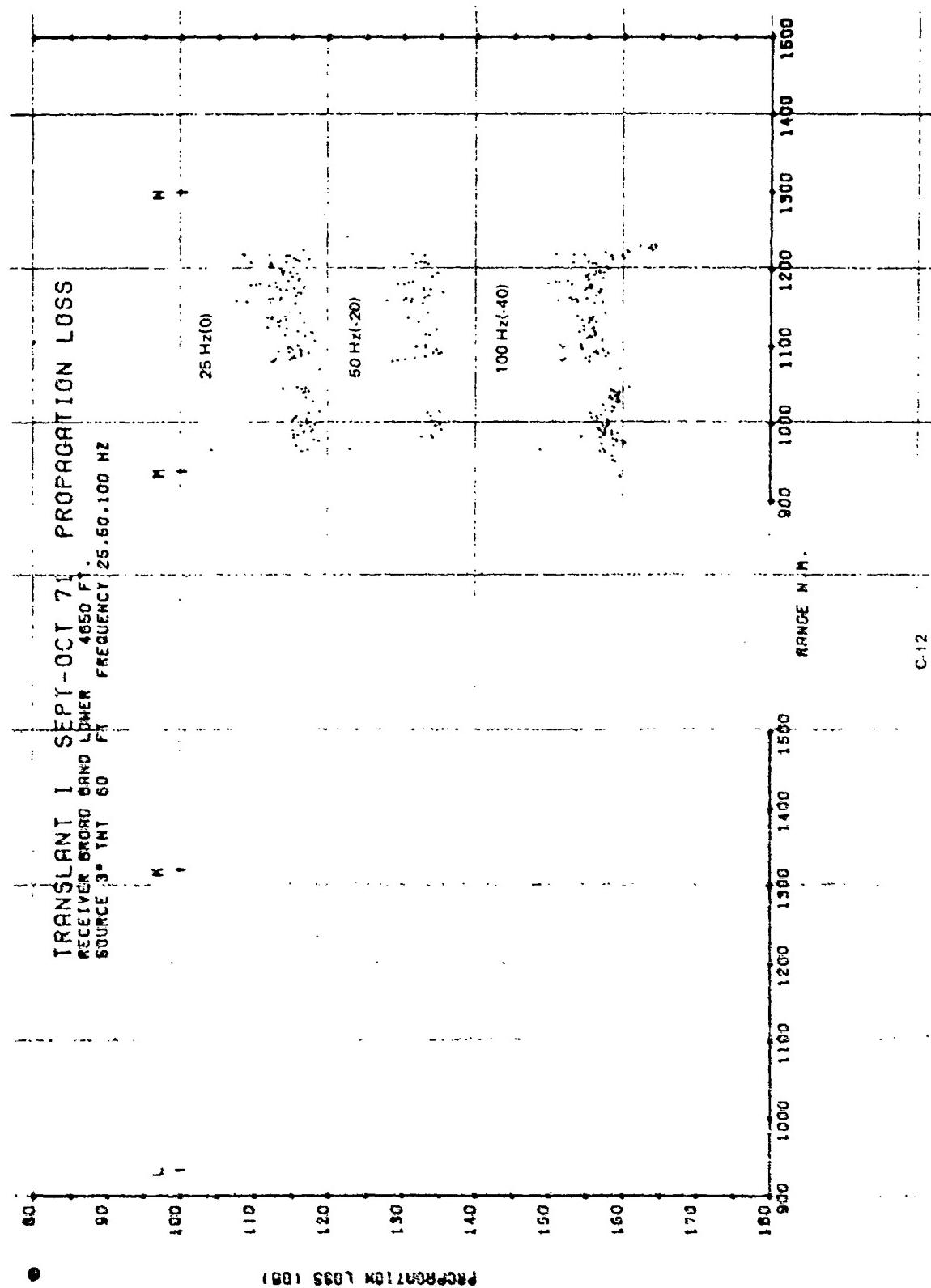
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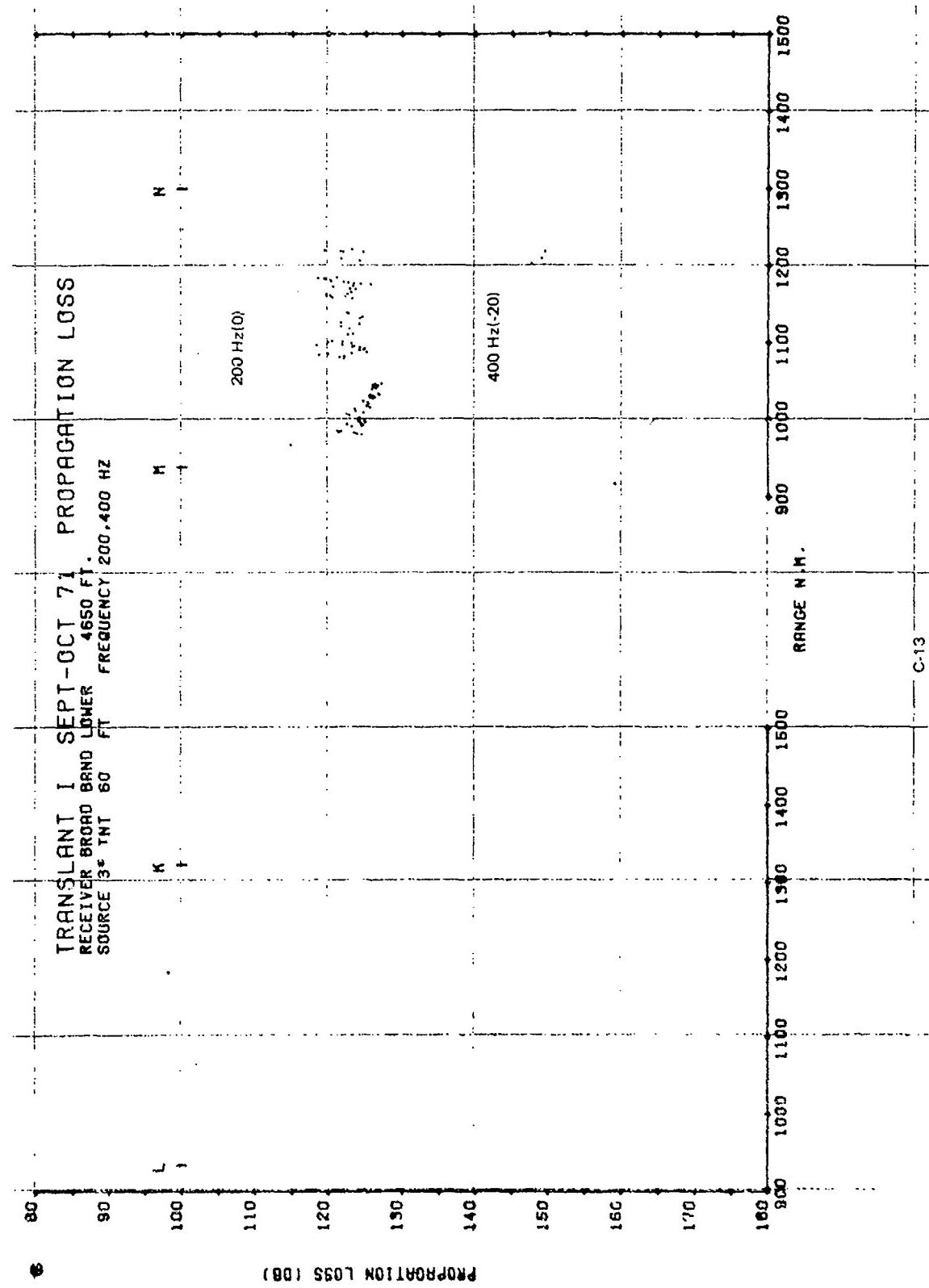
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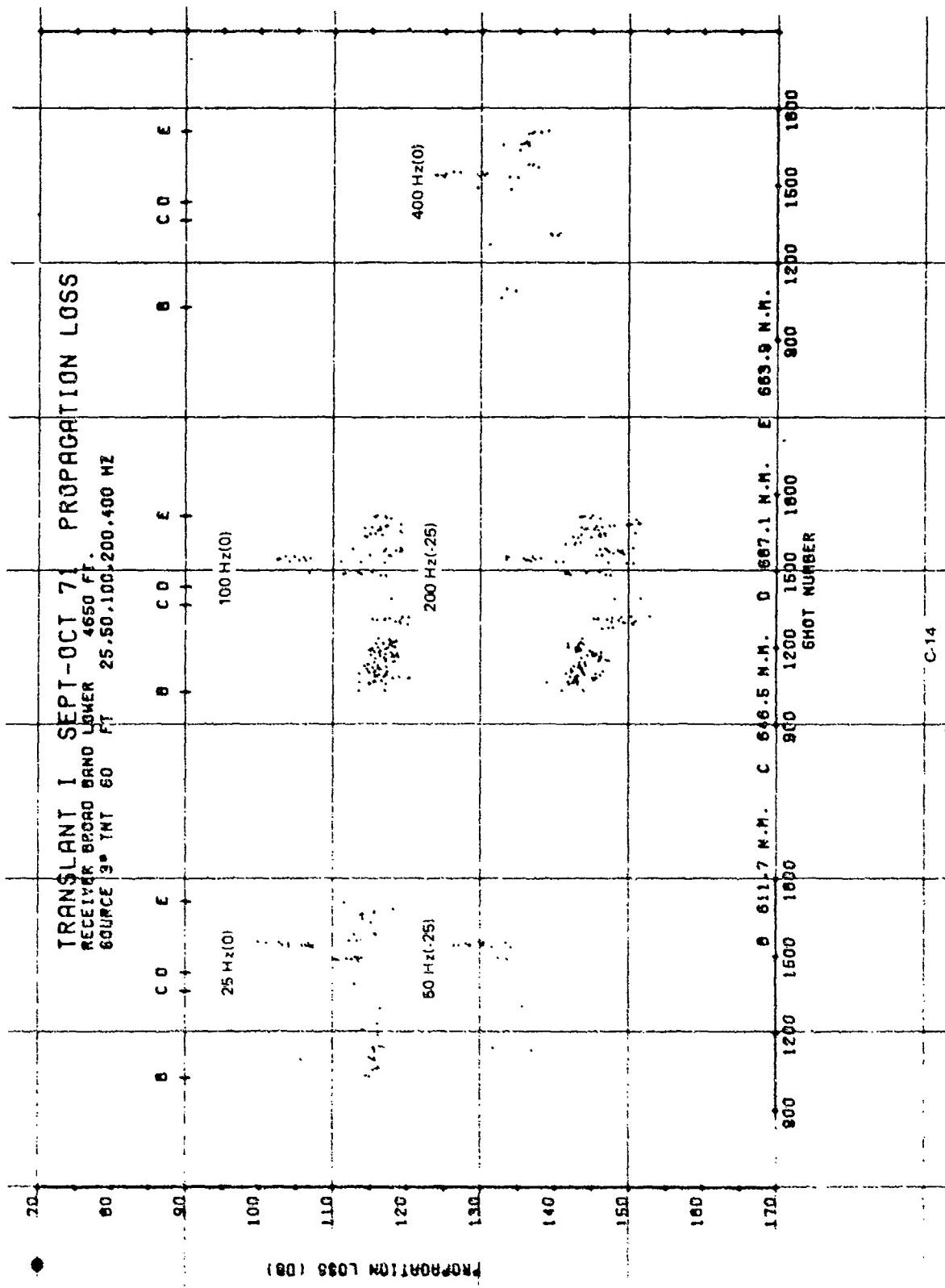
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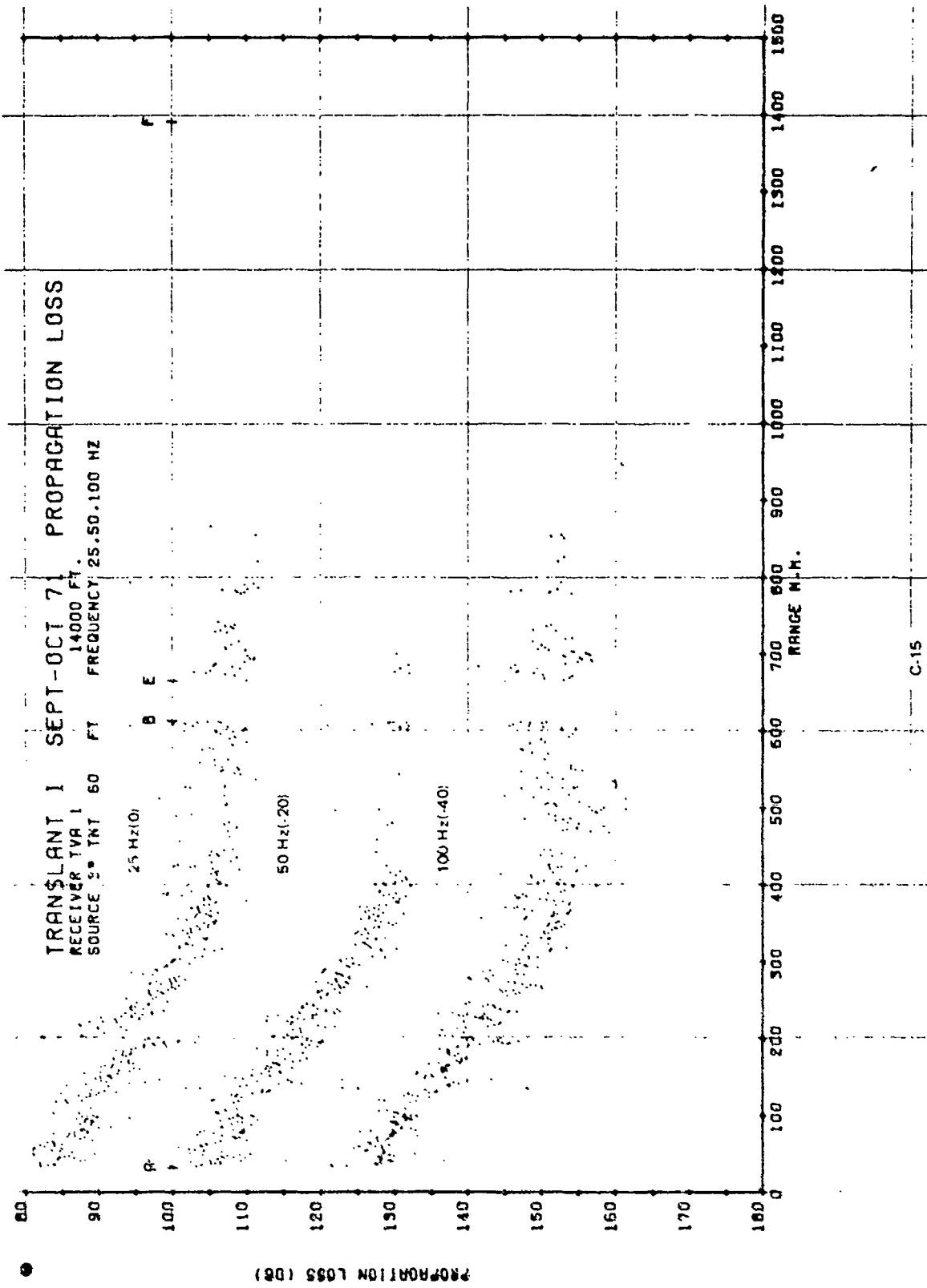
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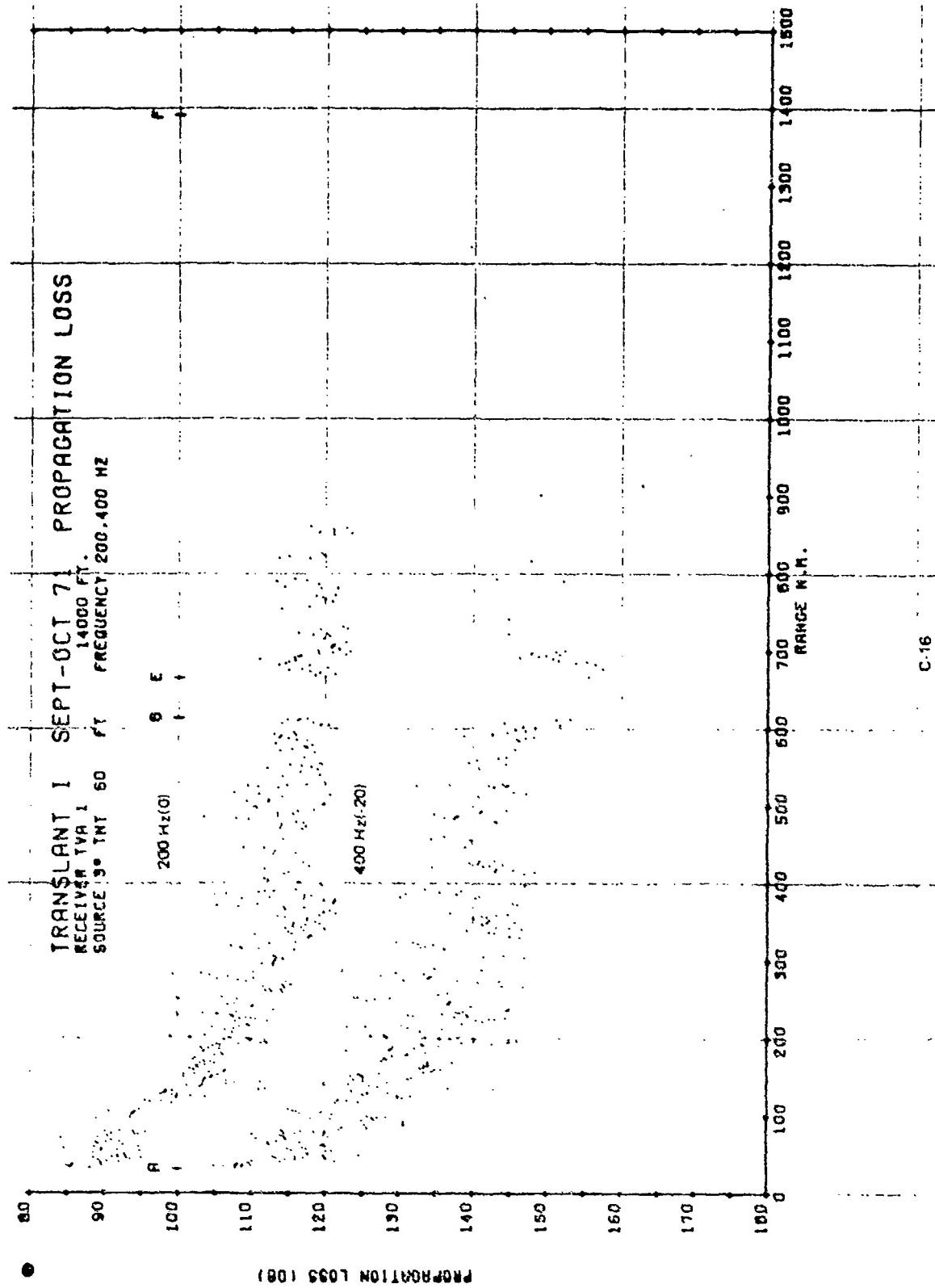
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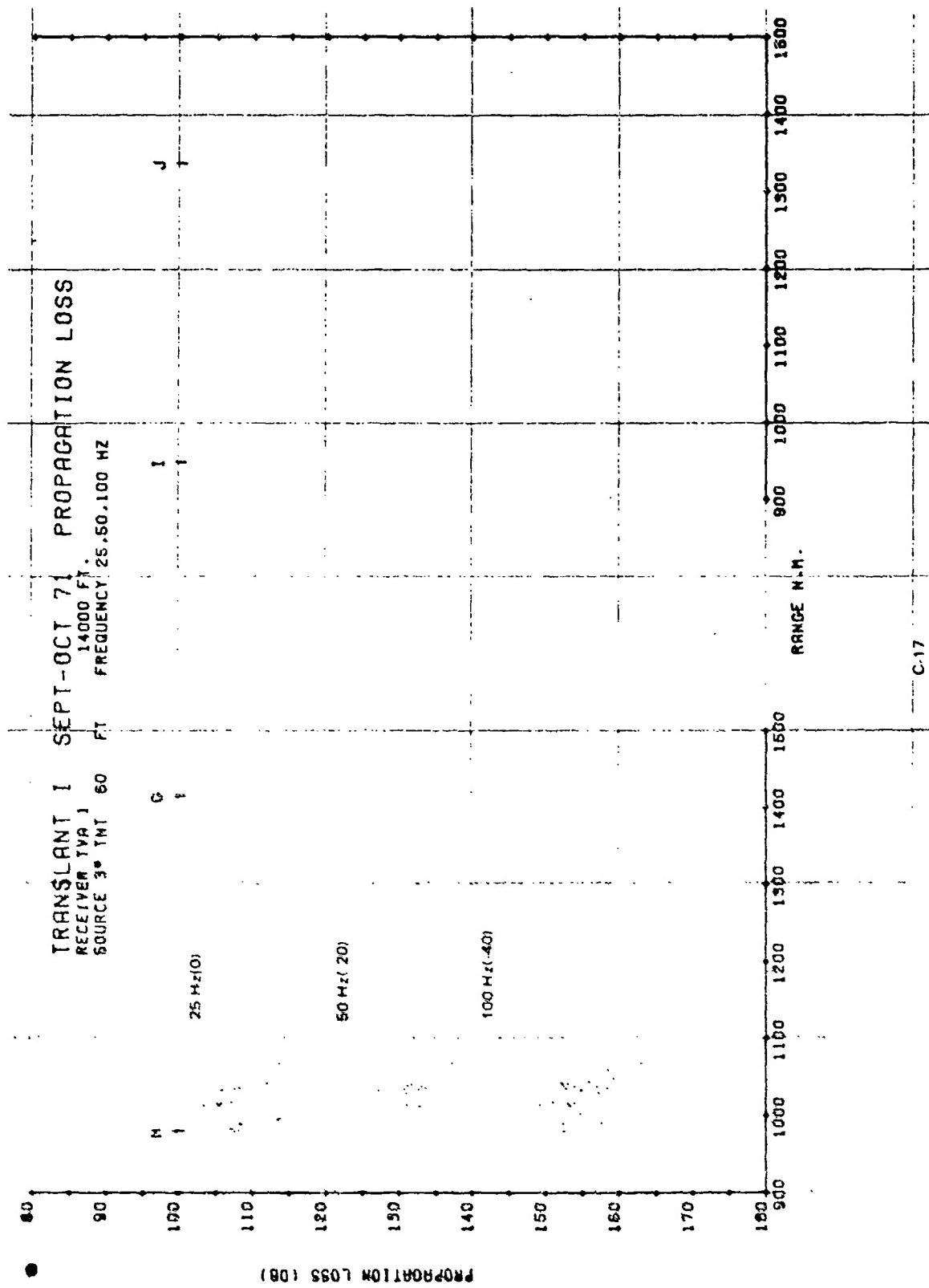
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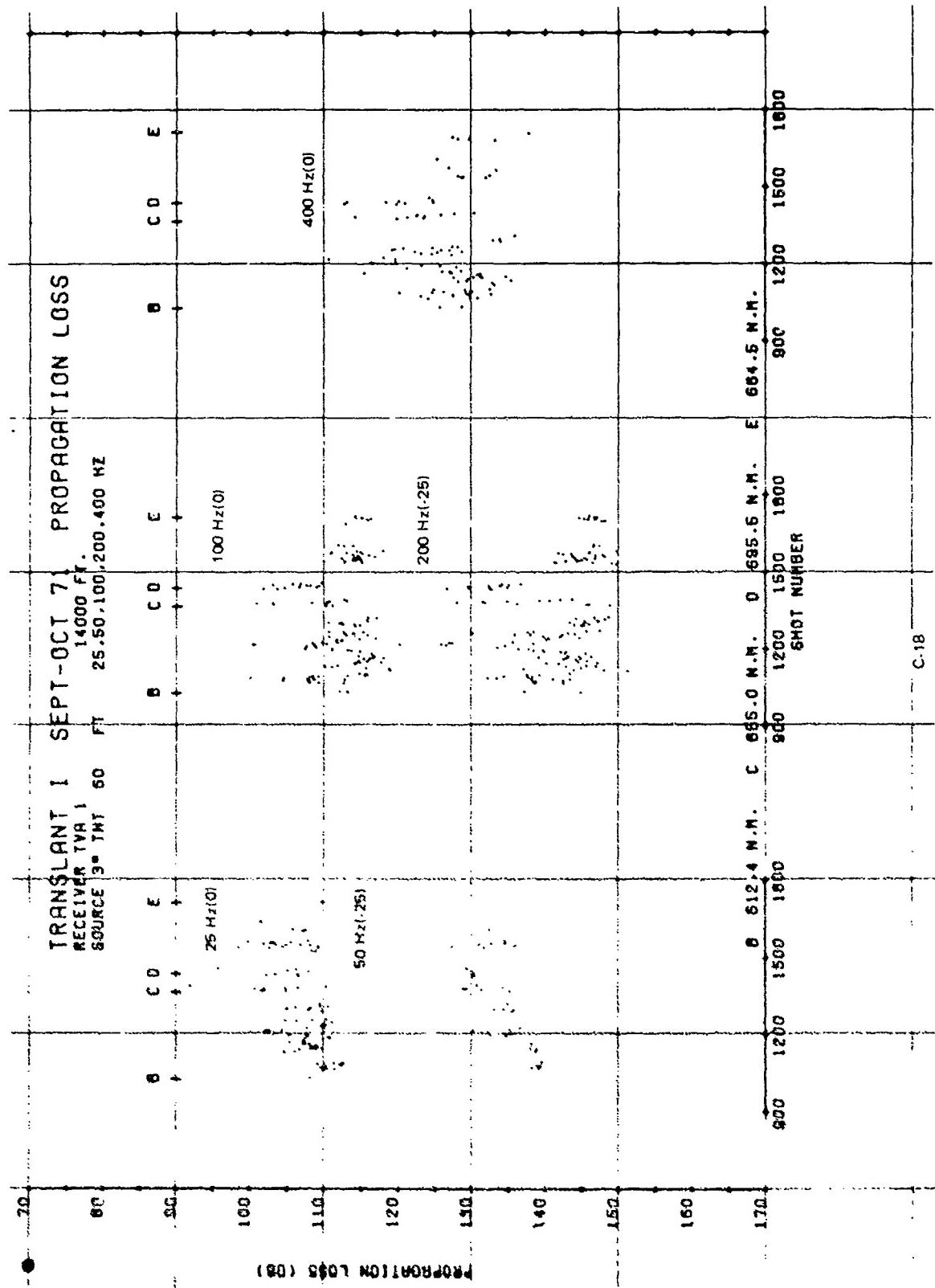
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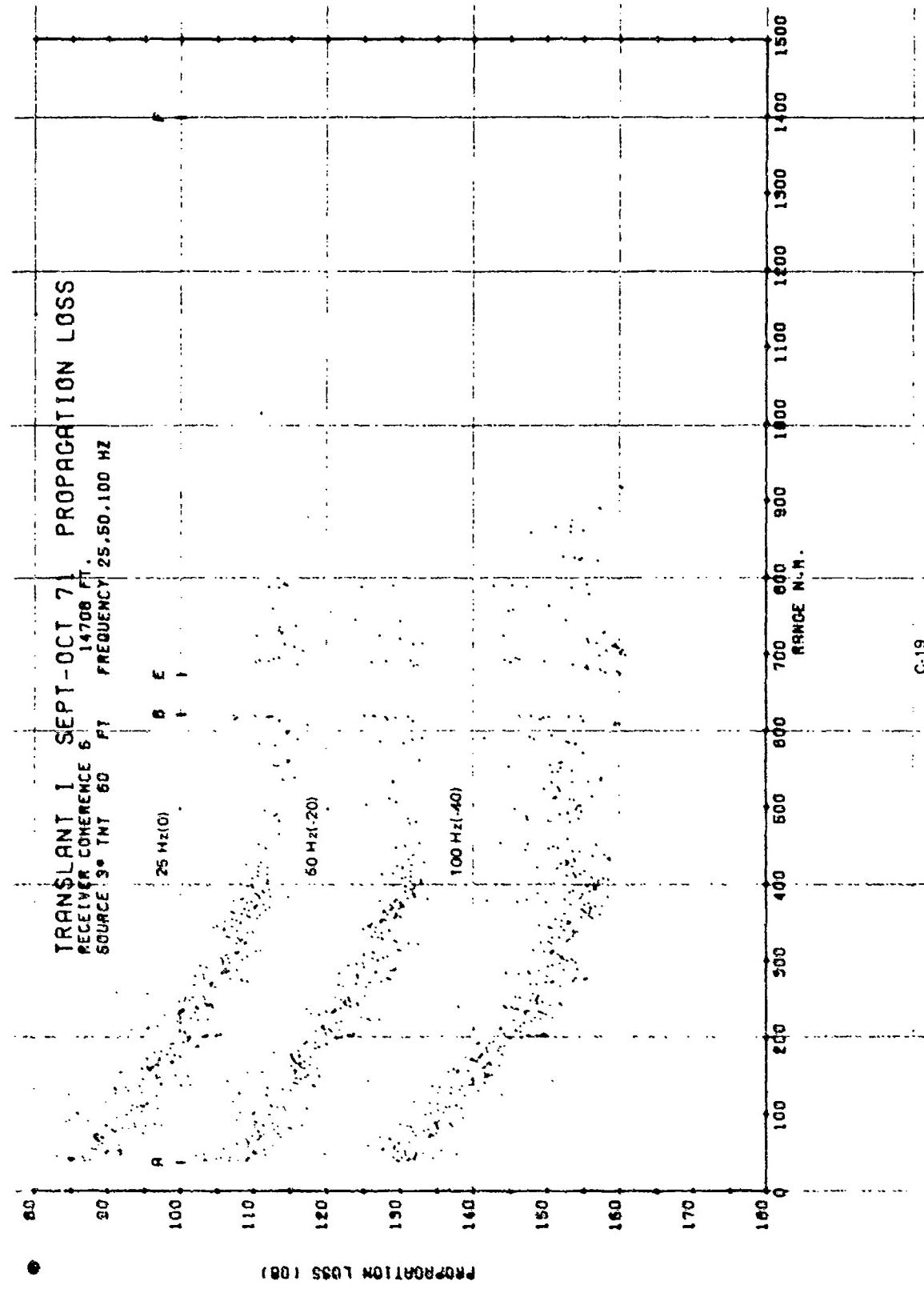
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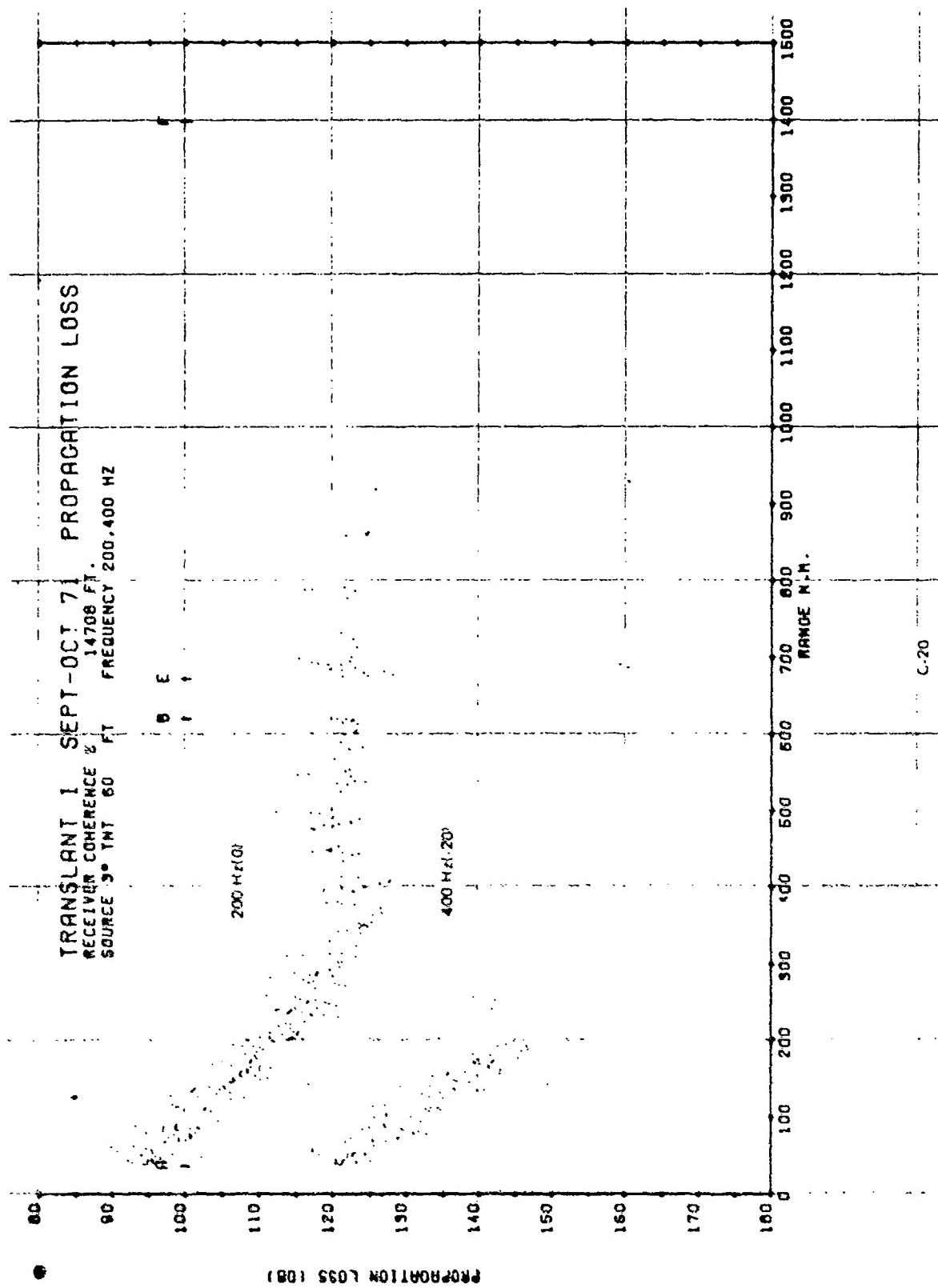
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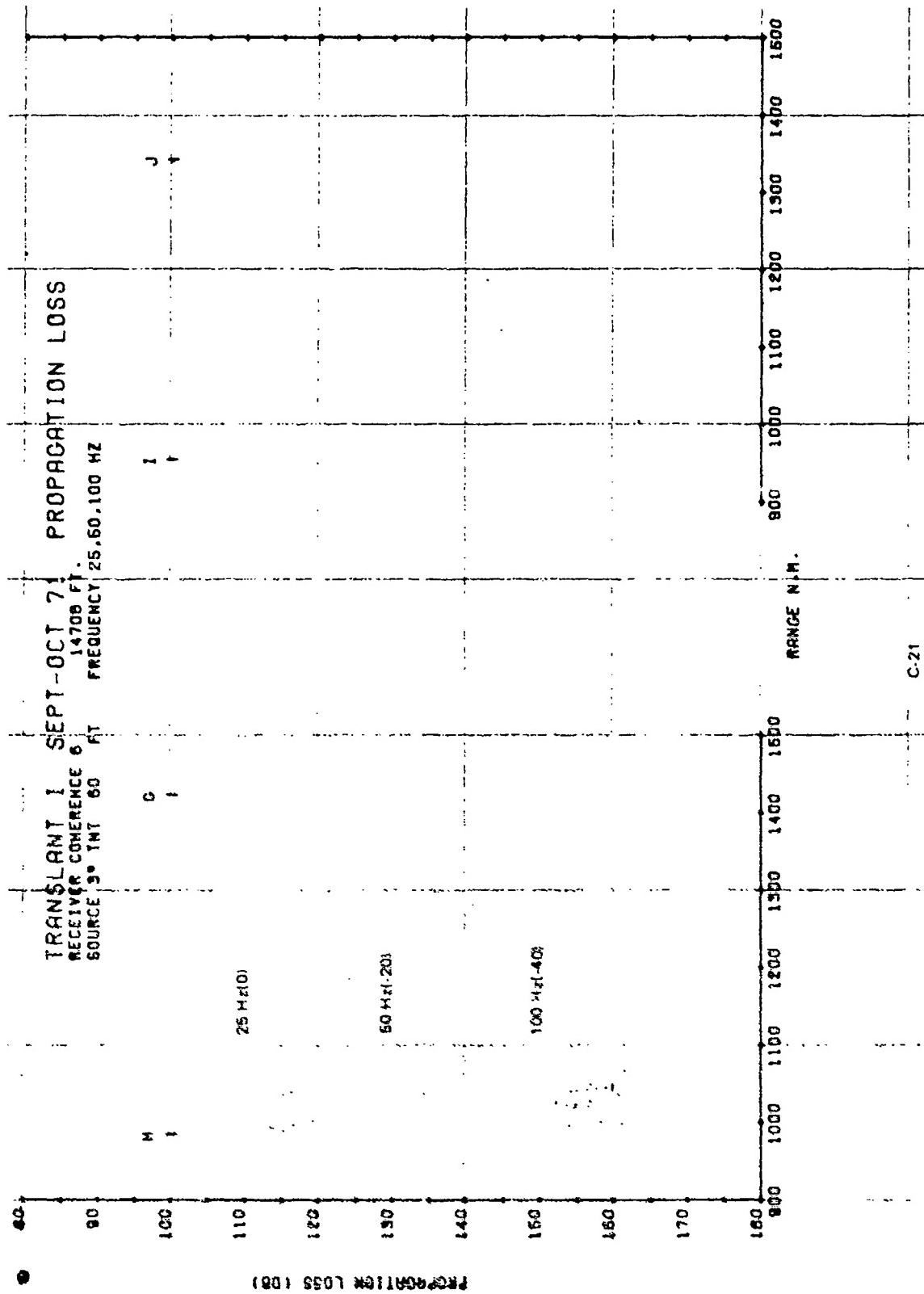
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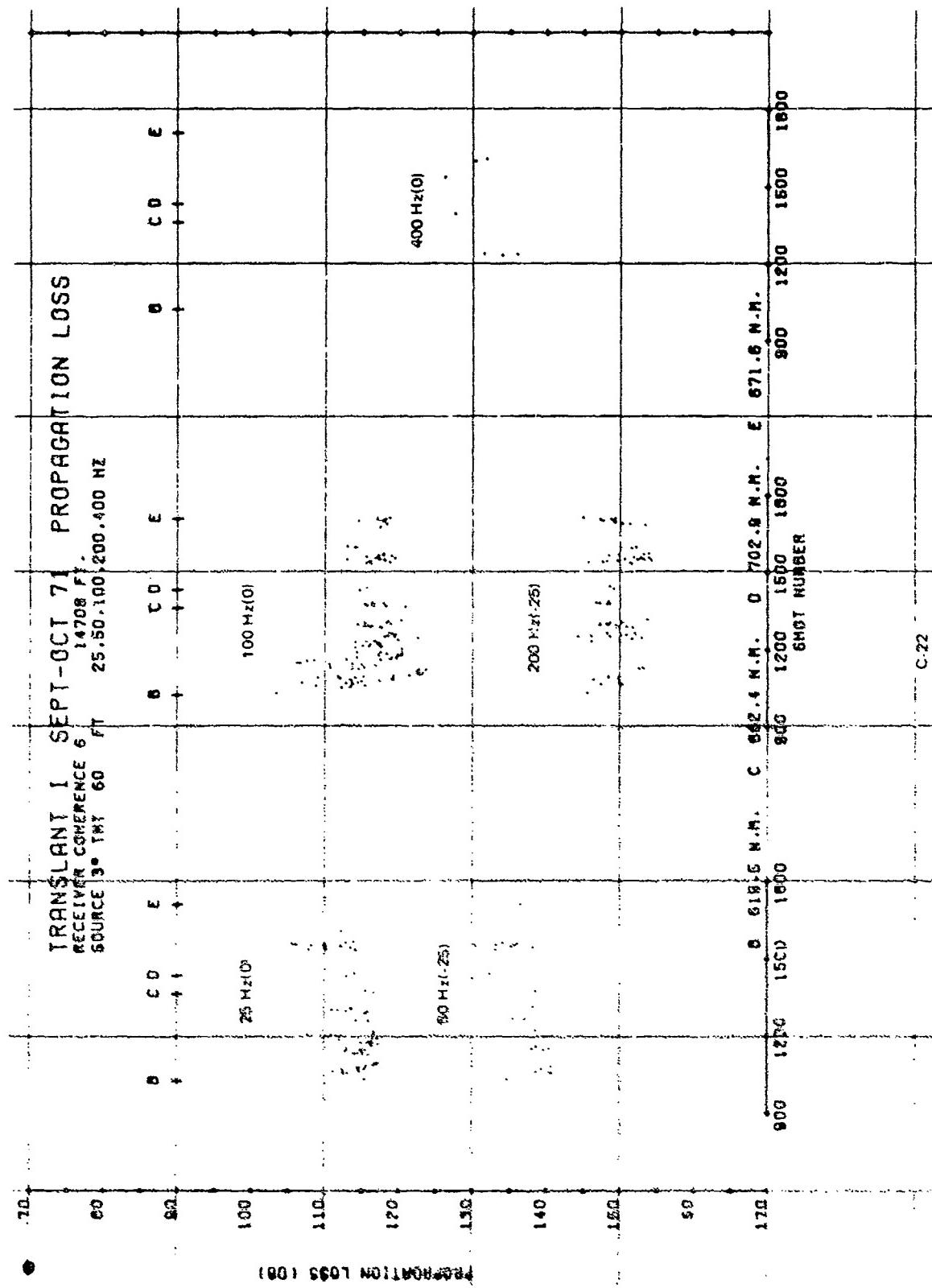
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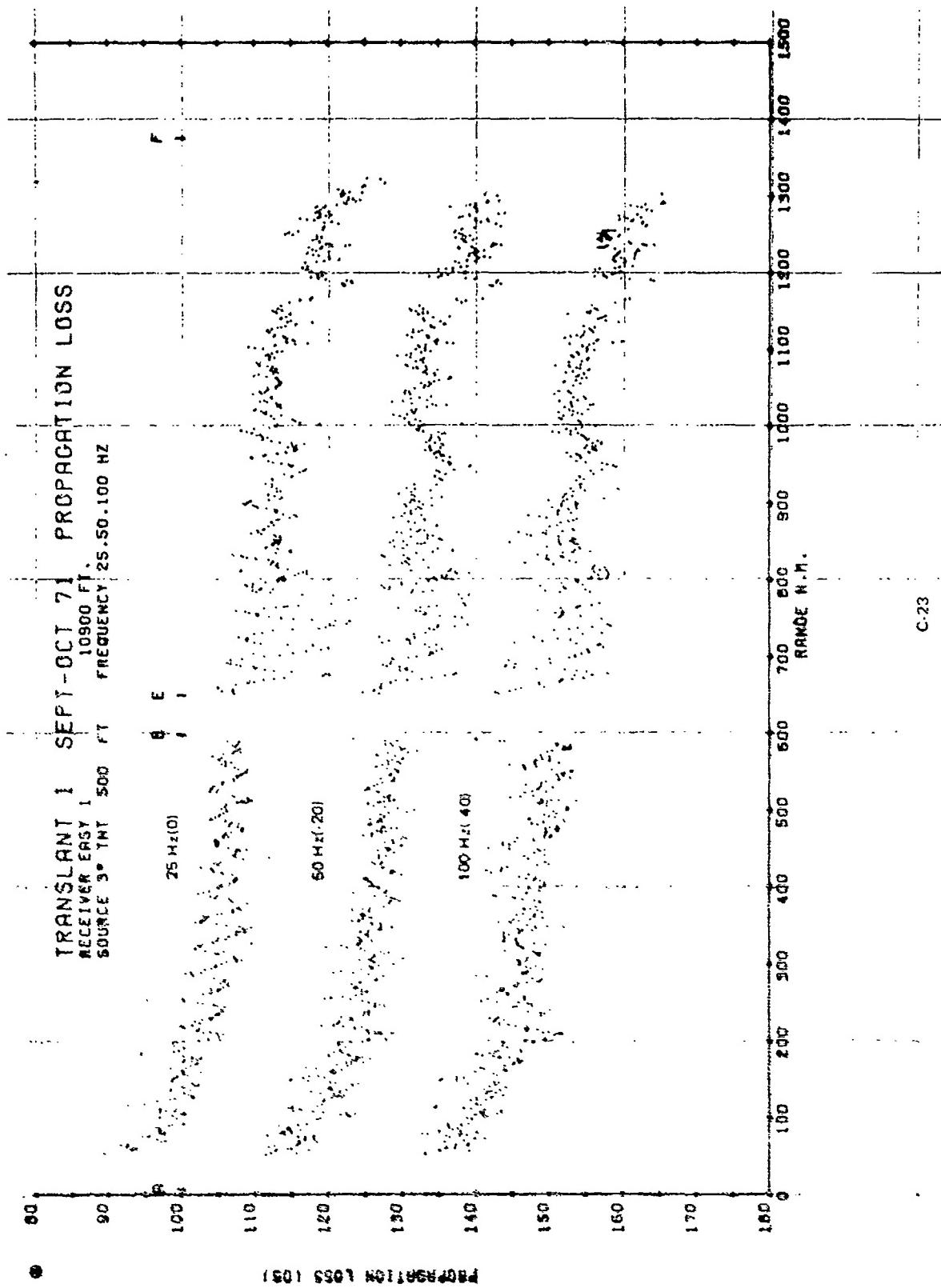


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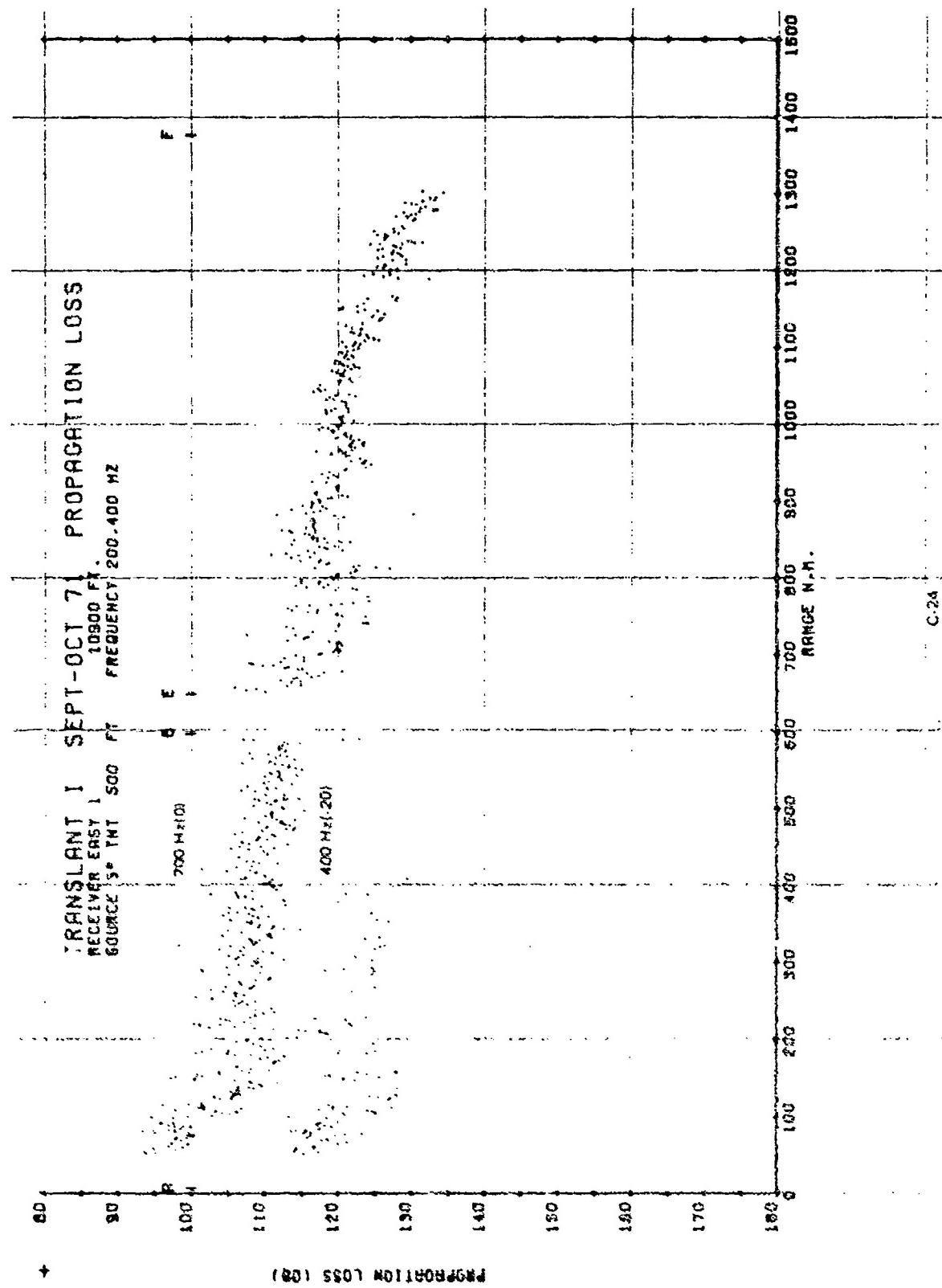
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C-24

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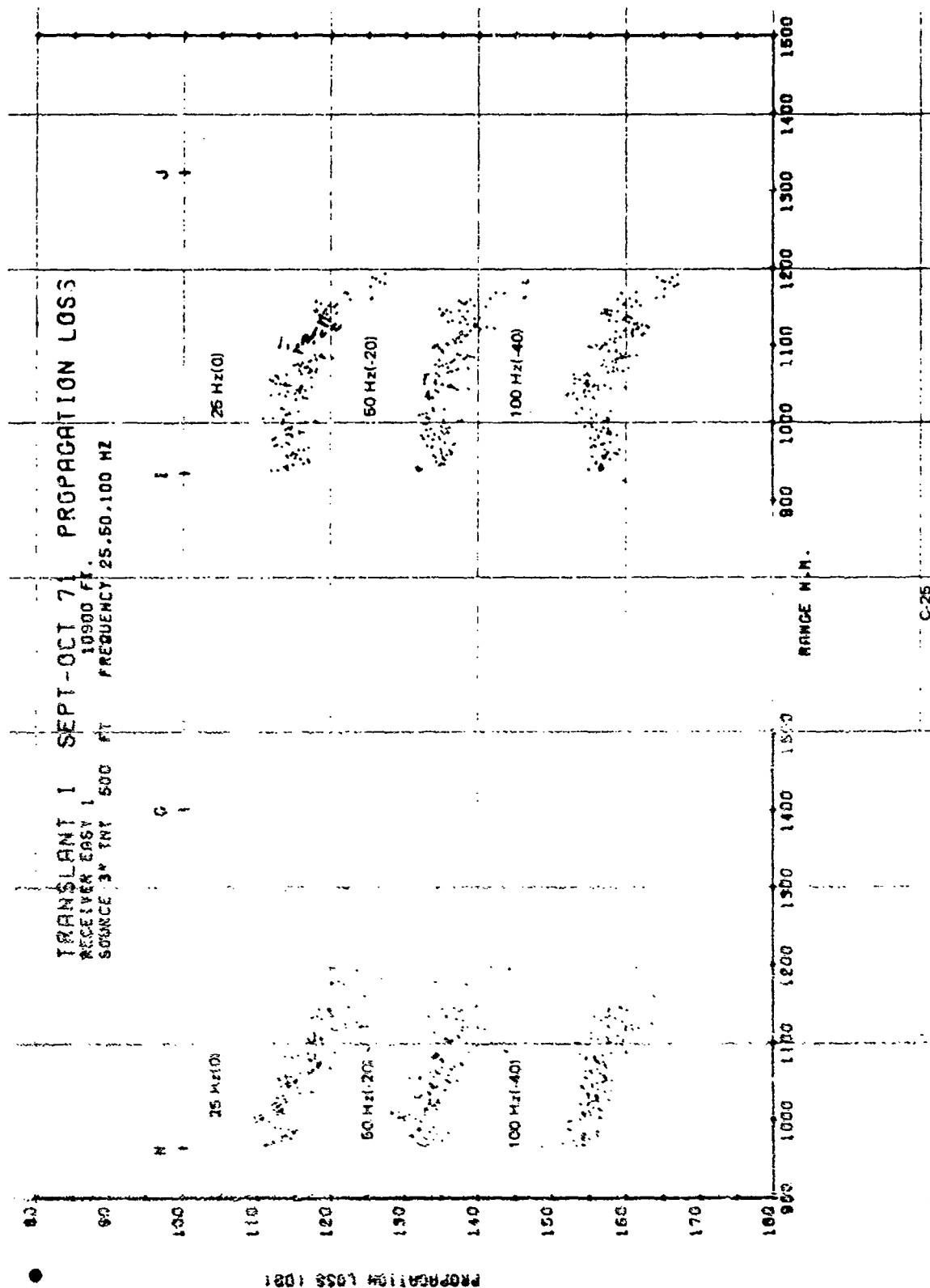
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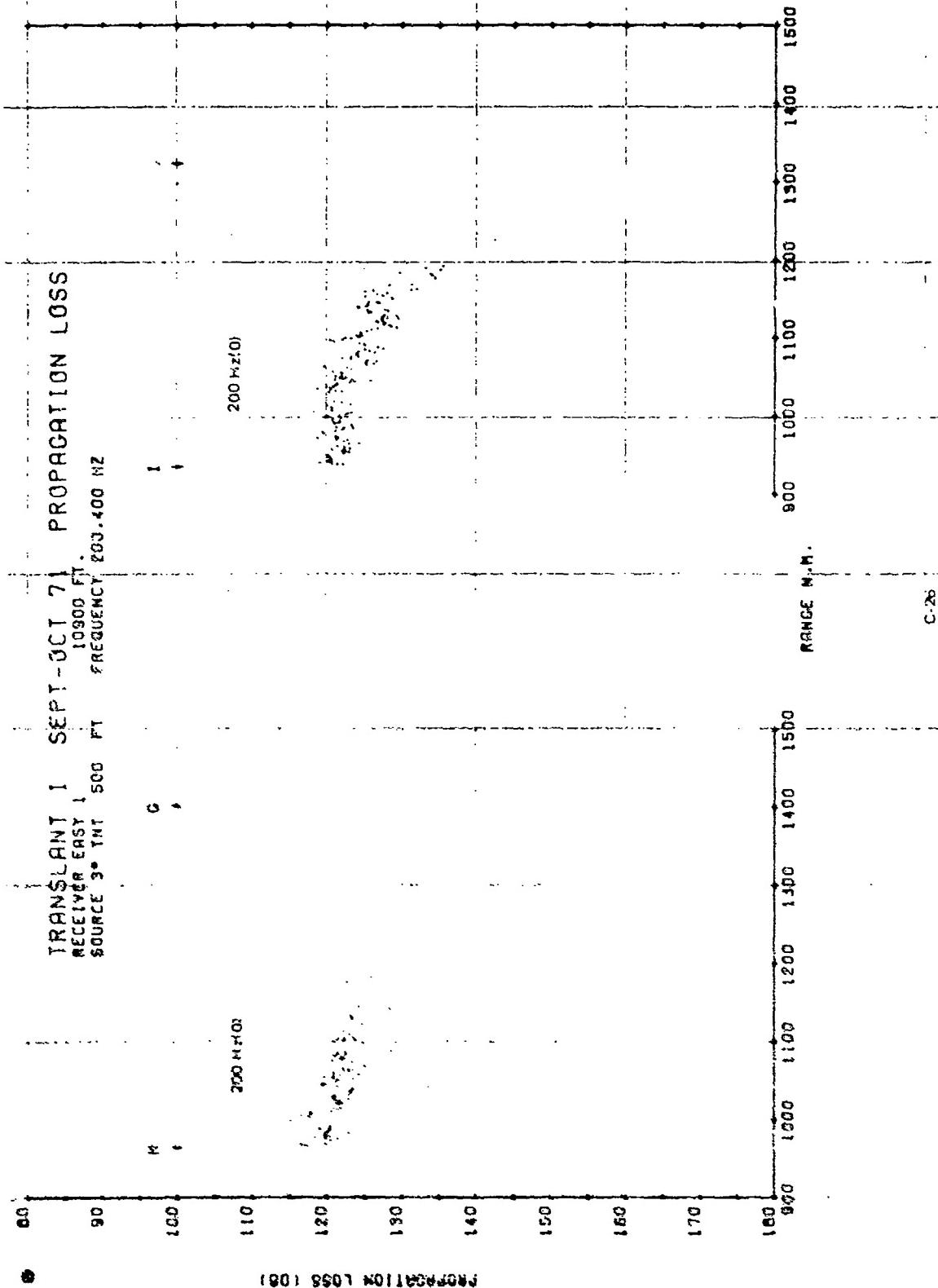
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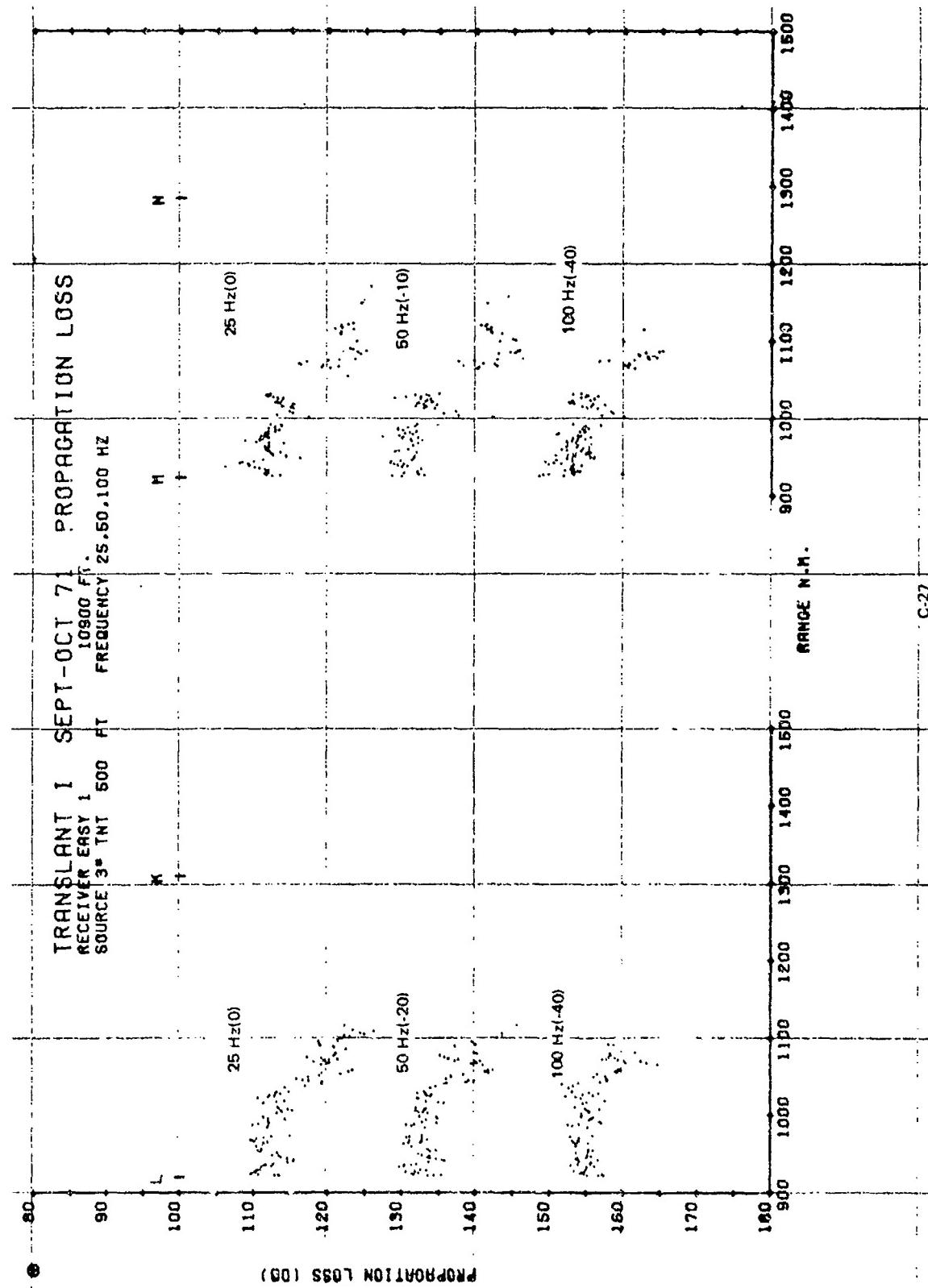
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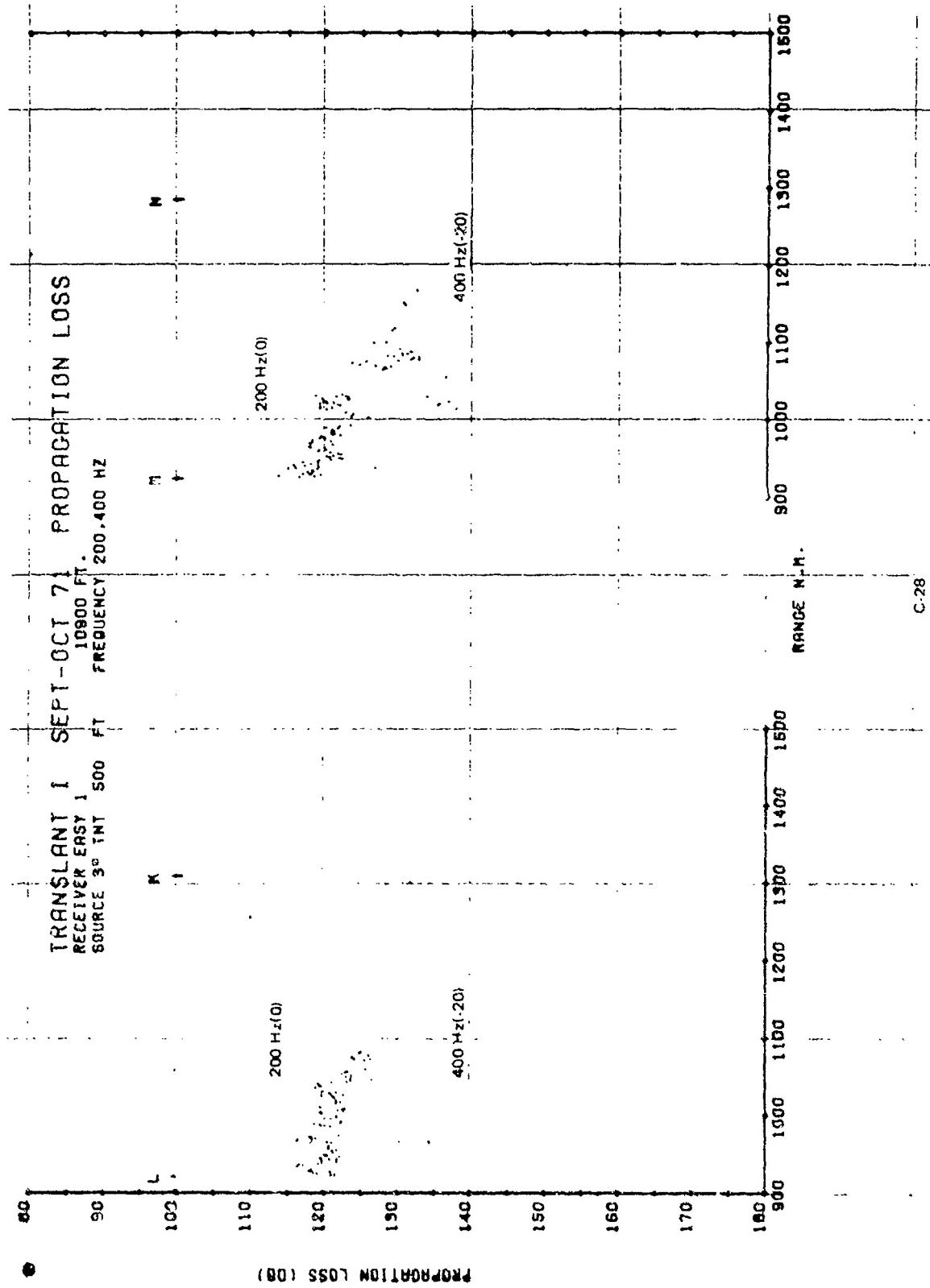


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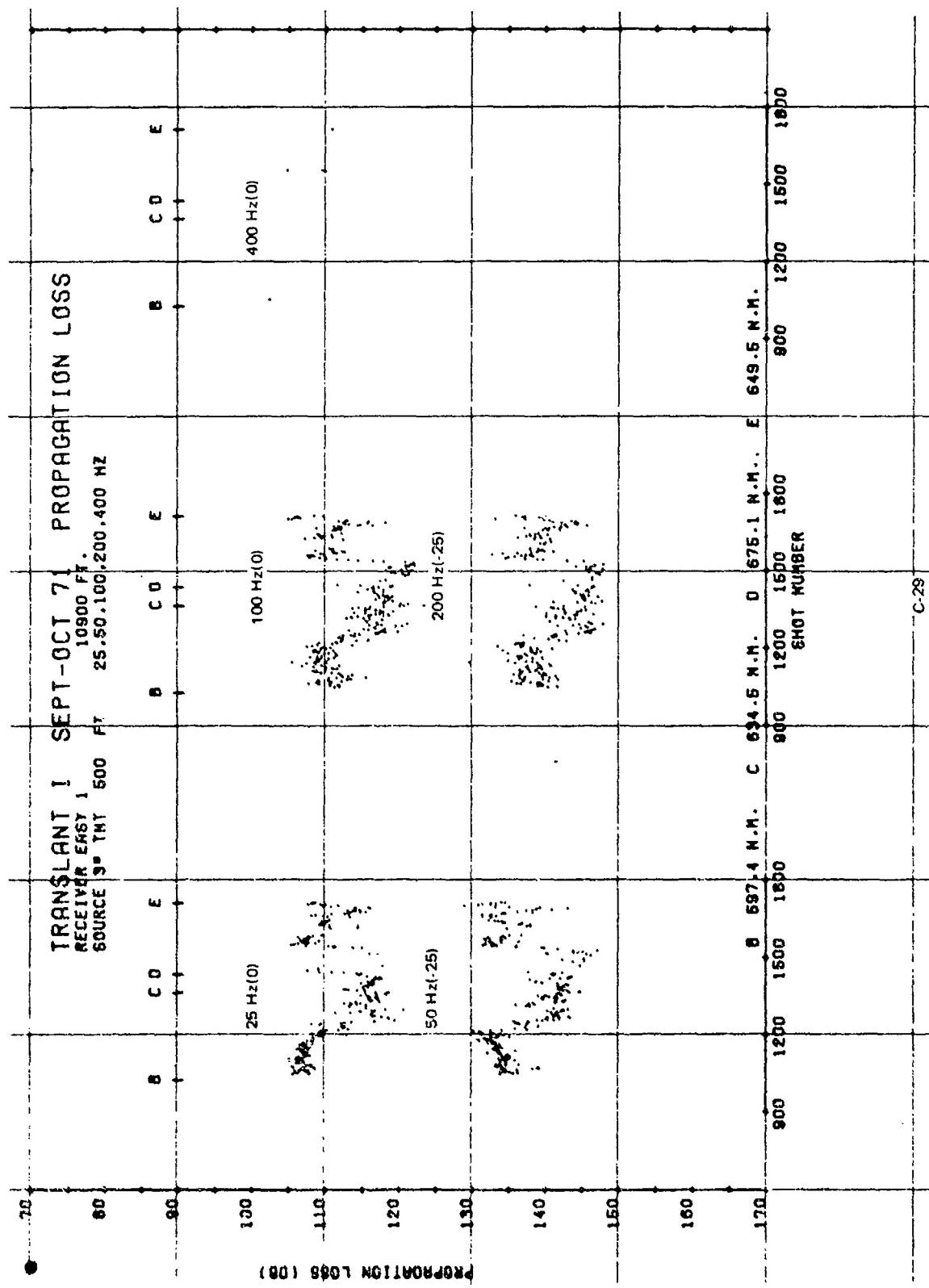
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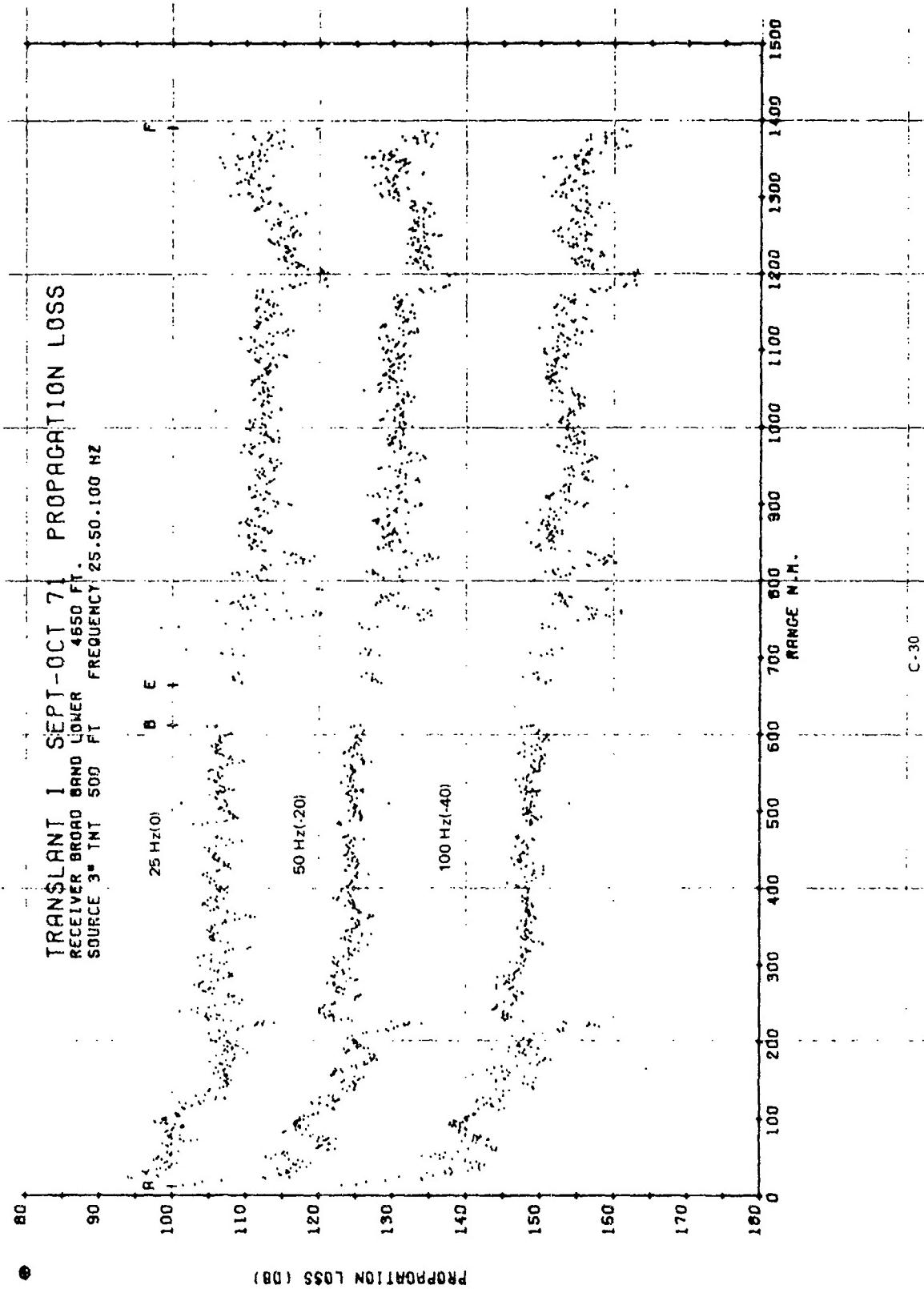
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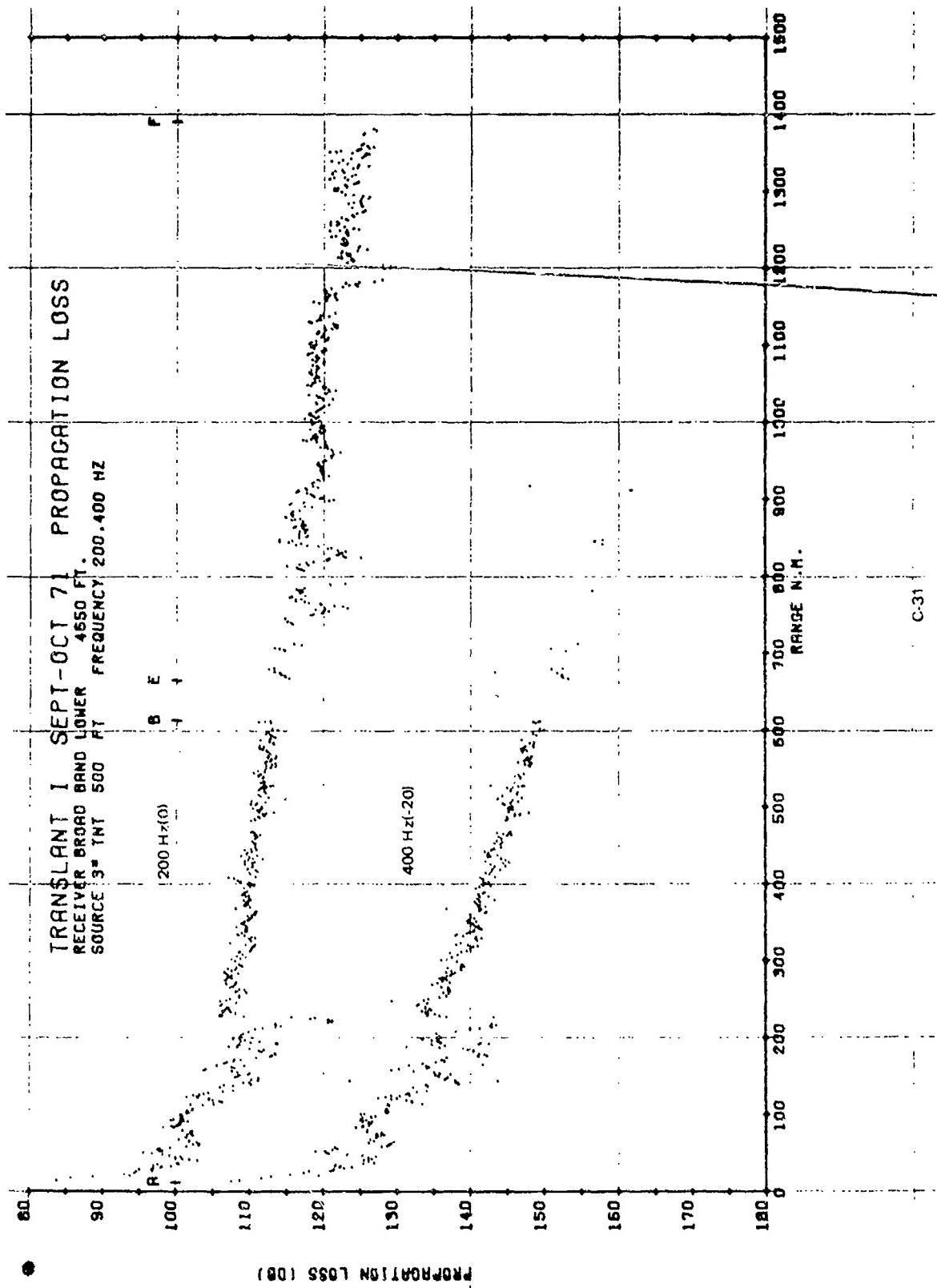
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C-31

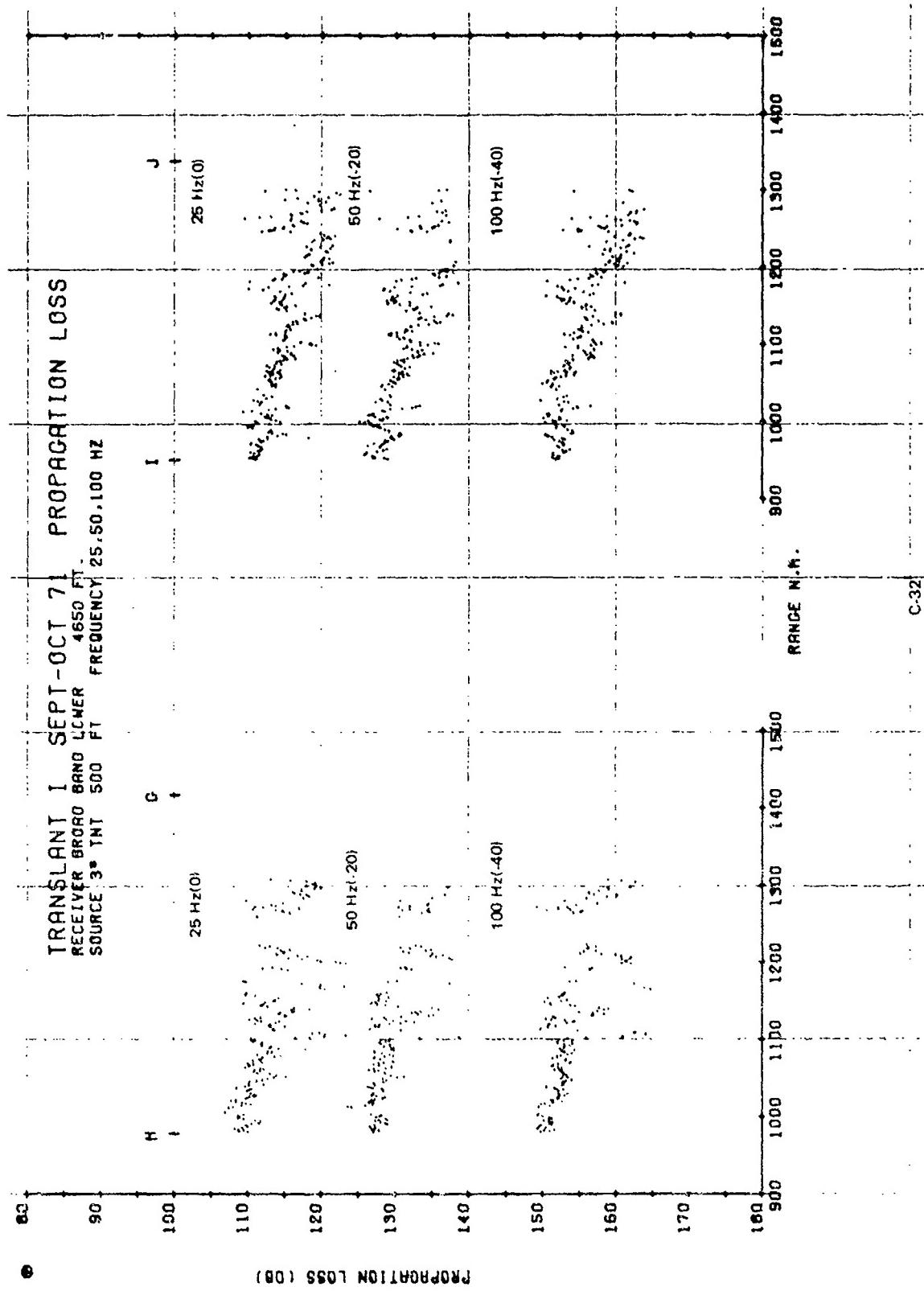
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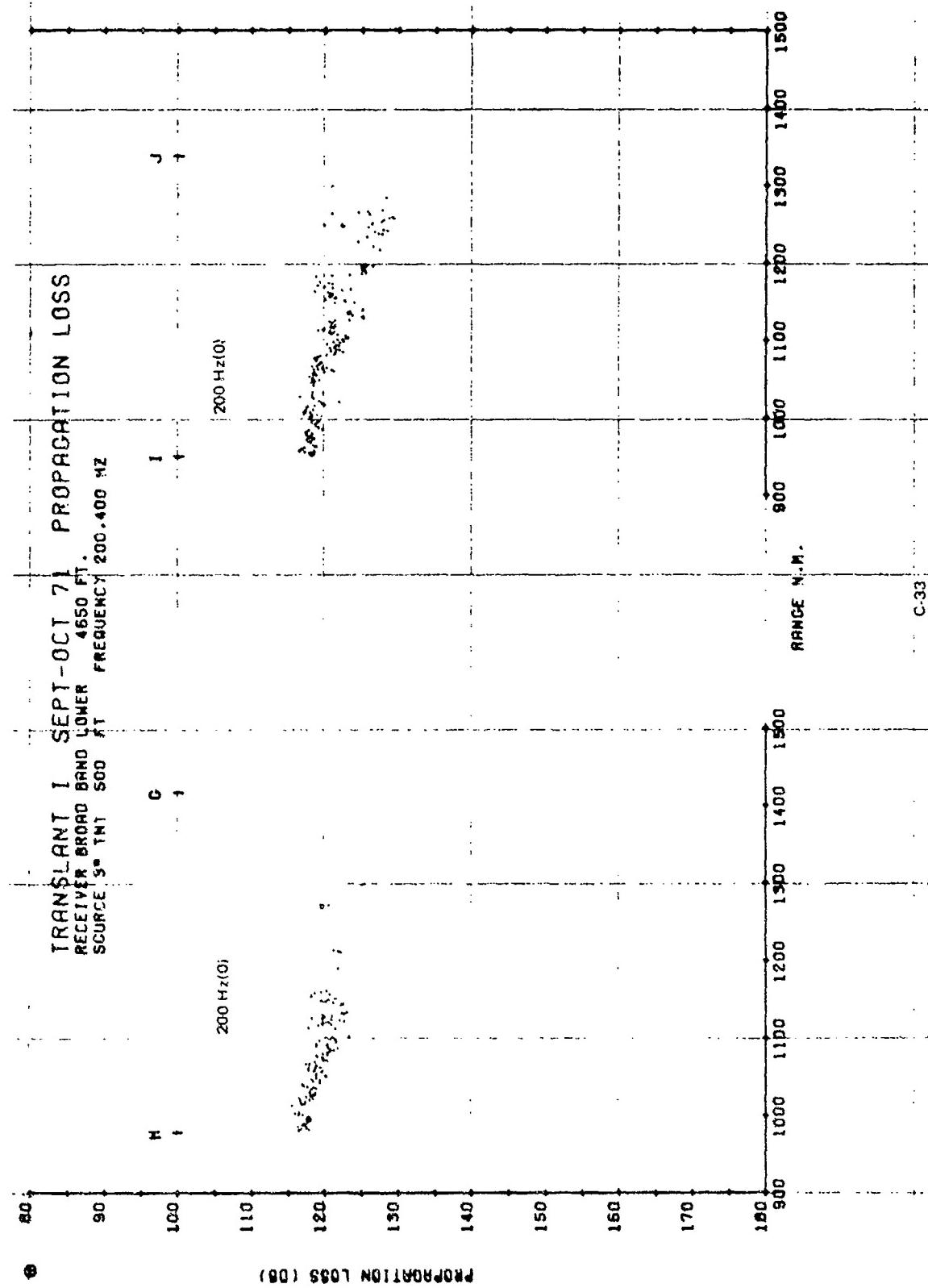
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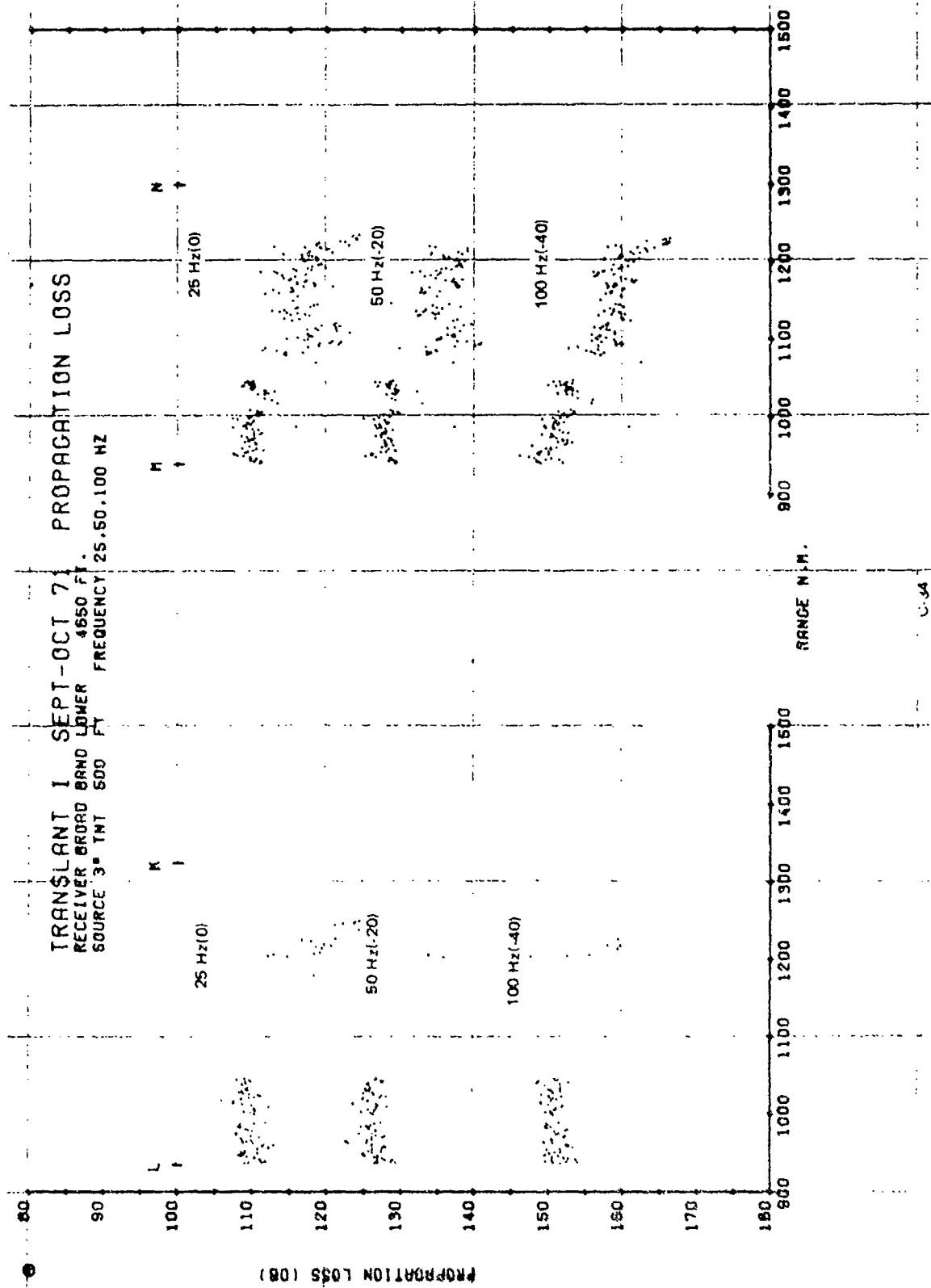
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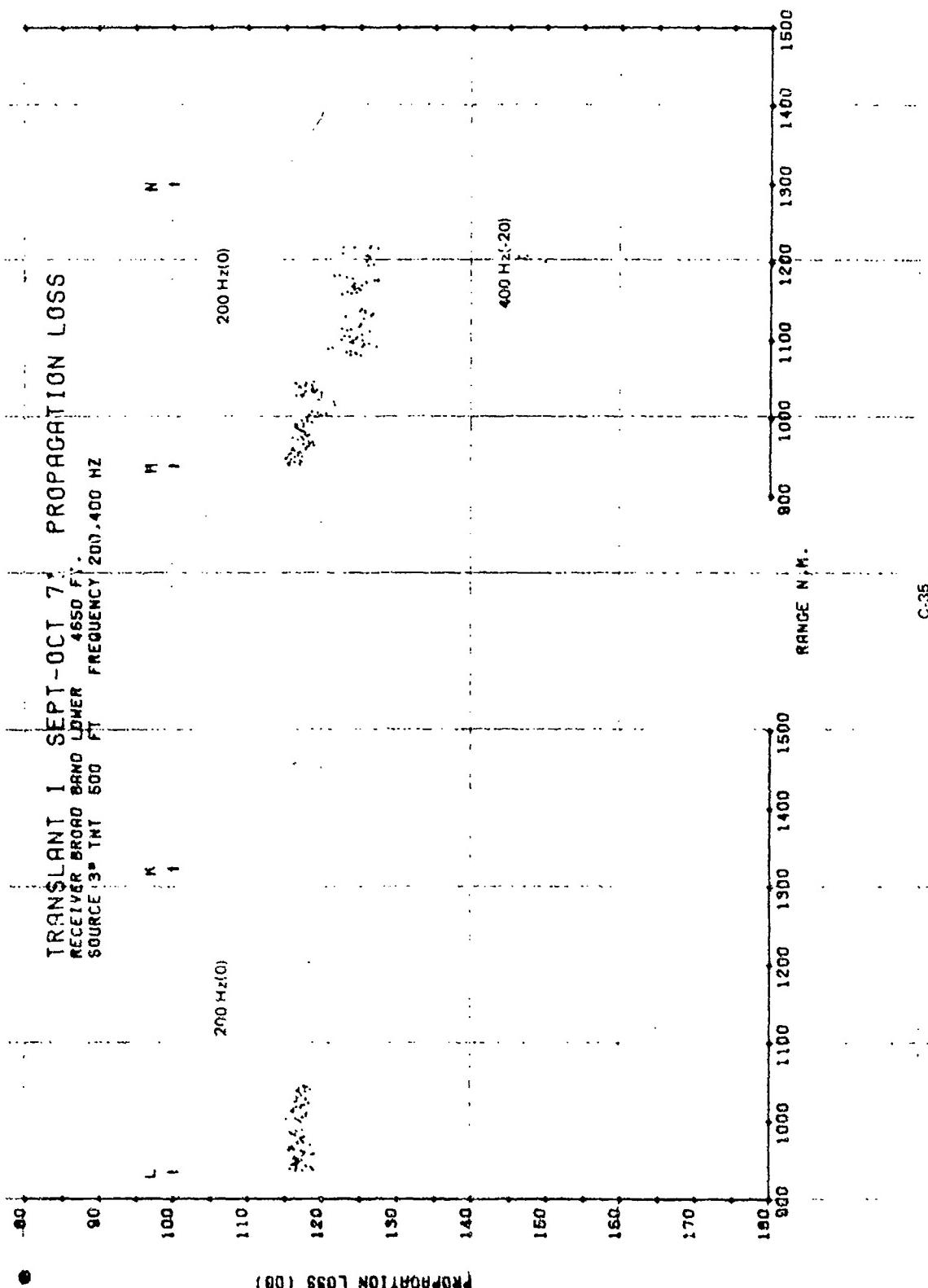


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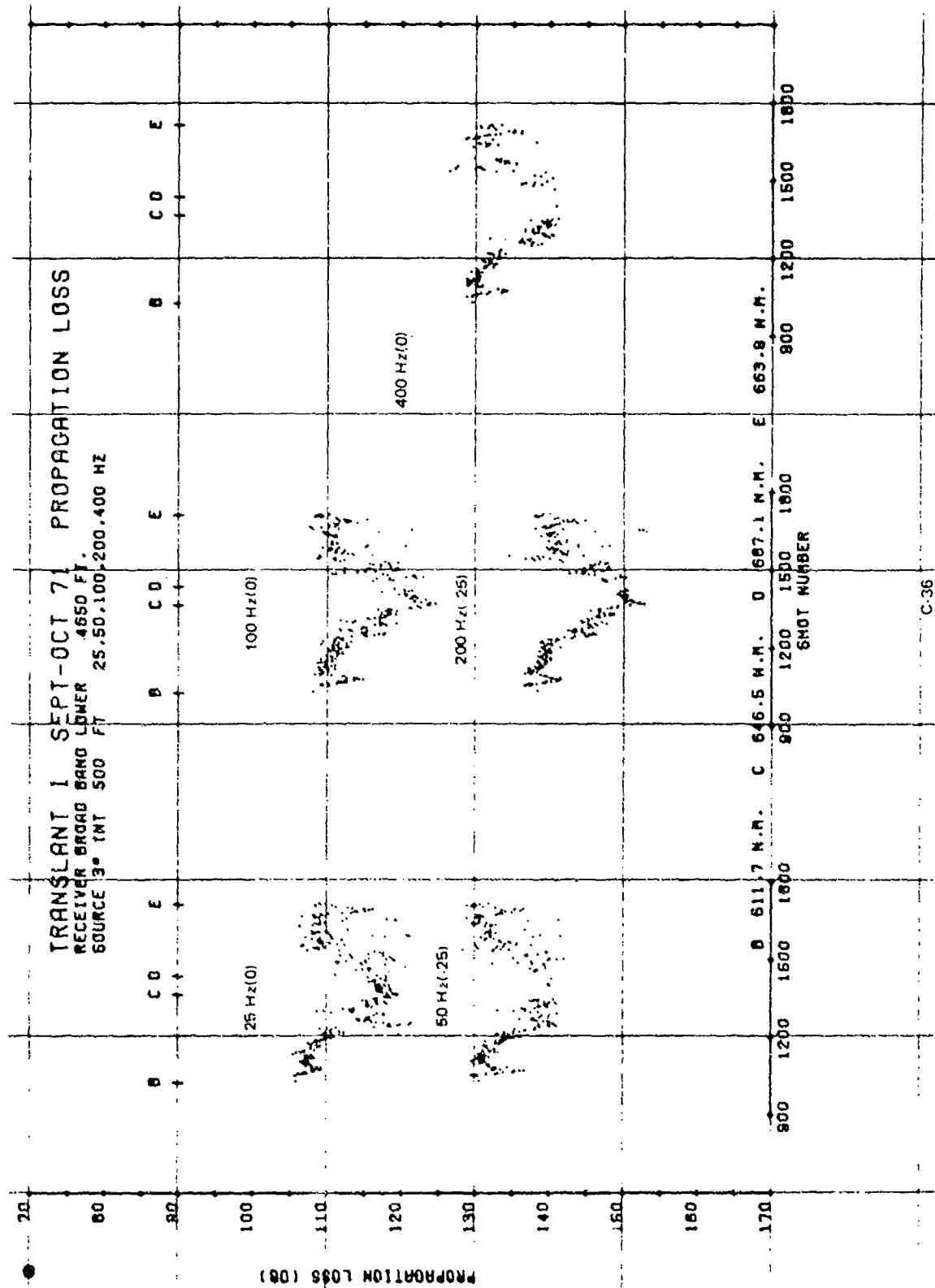
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C-36

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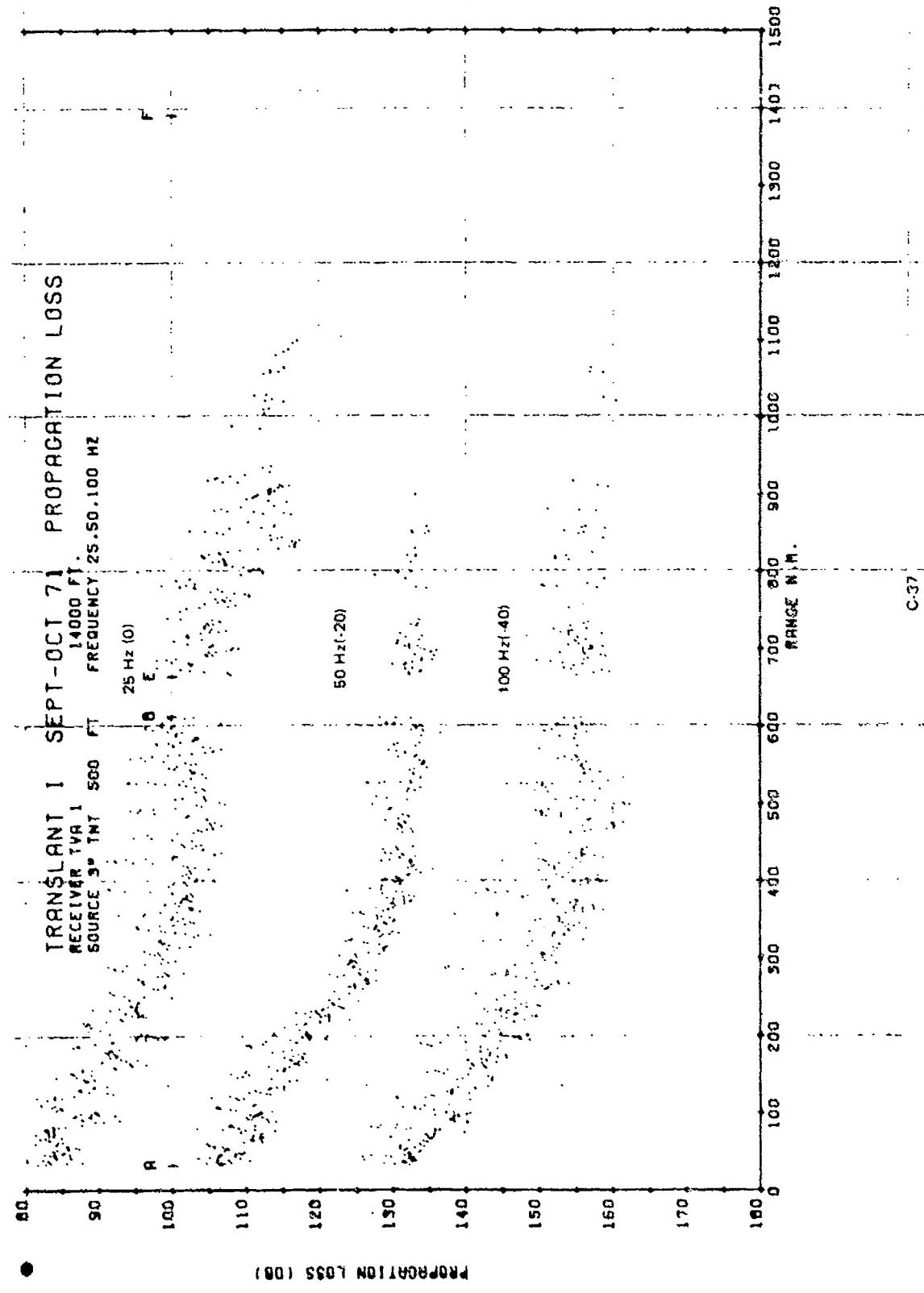
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C-37

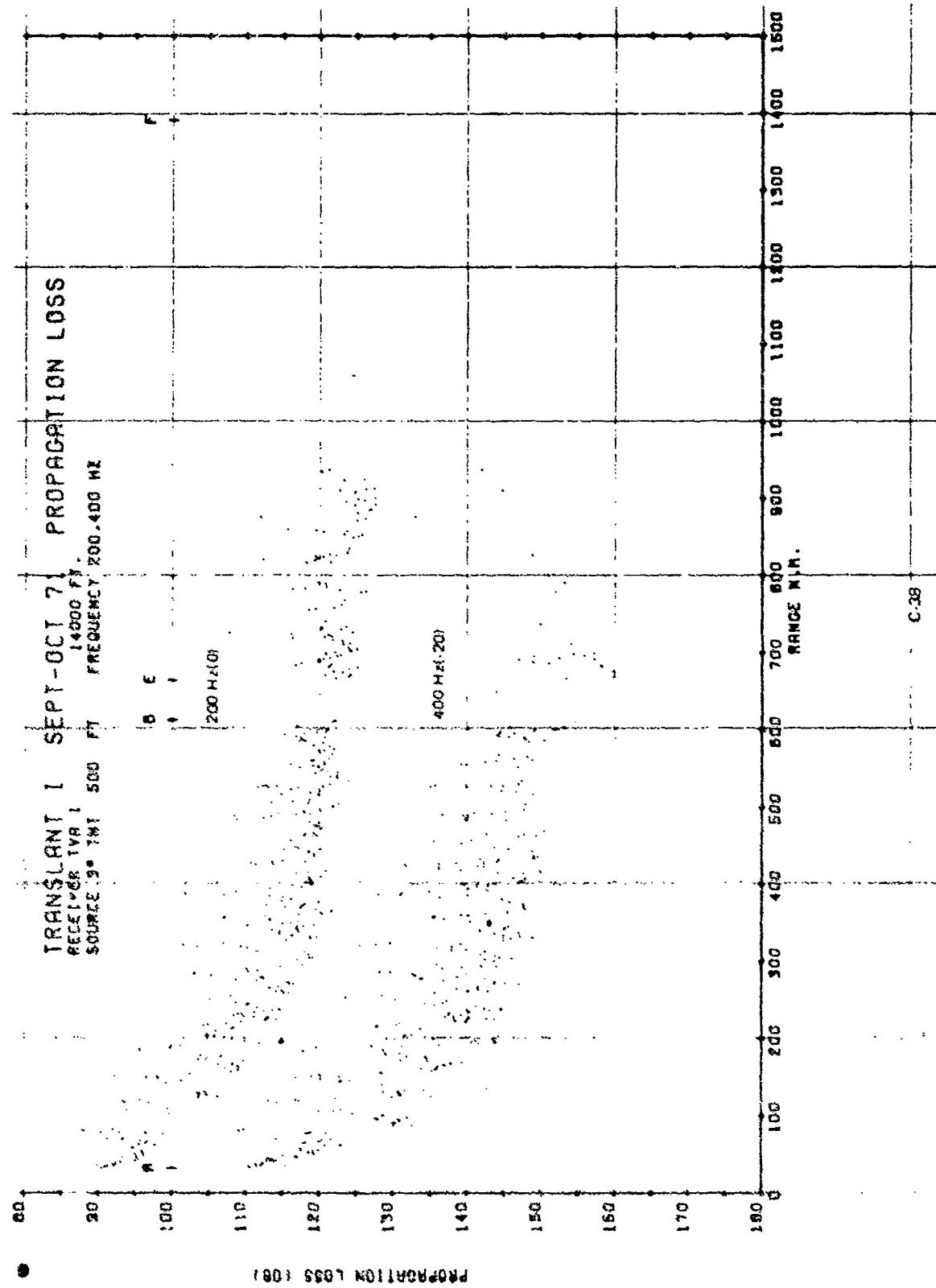
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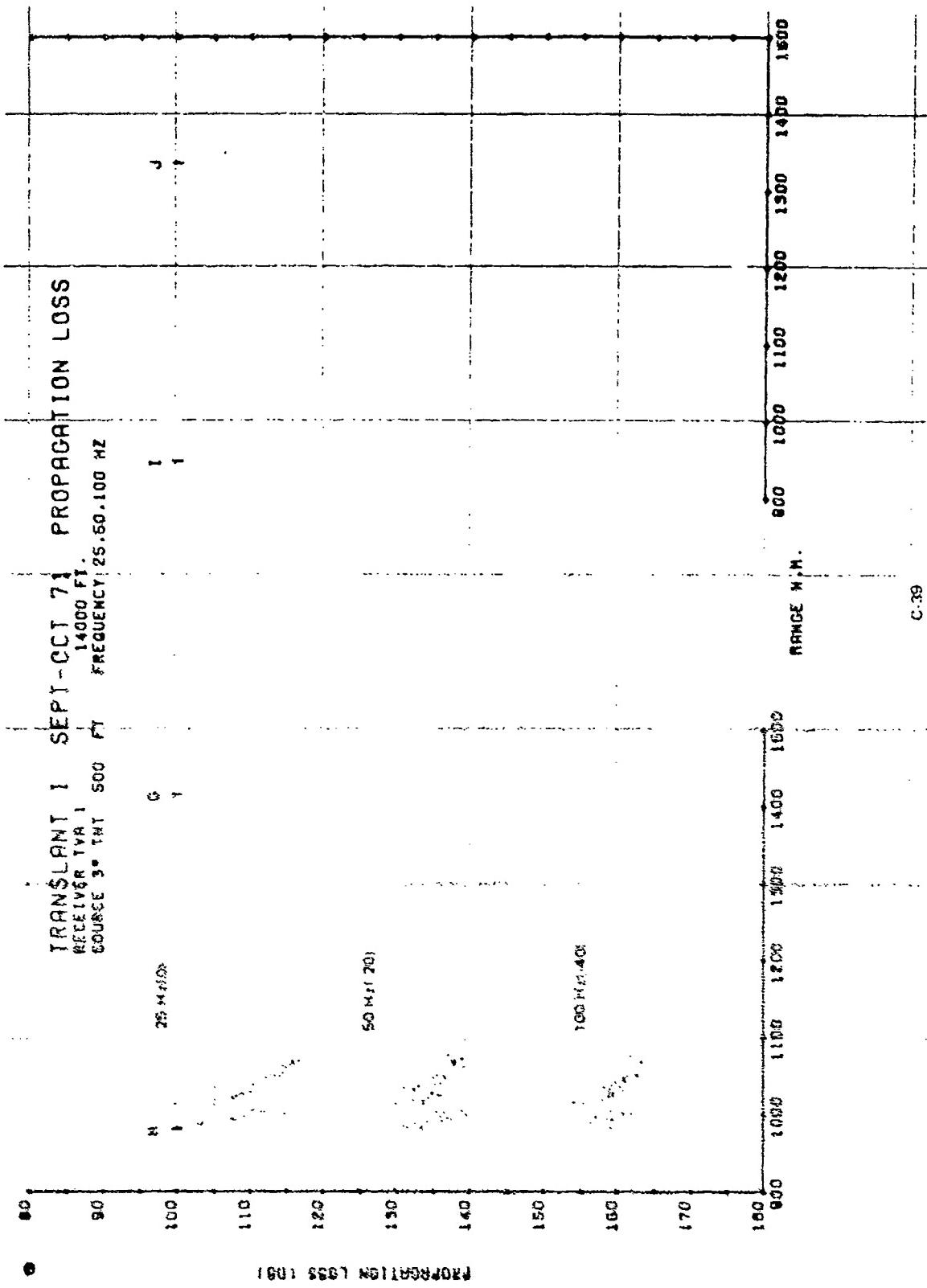
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C-39

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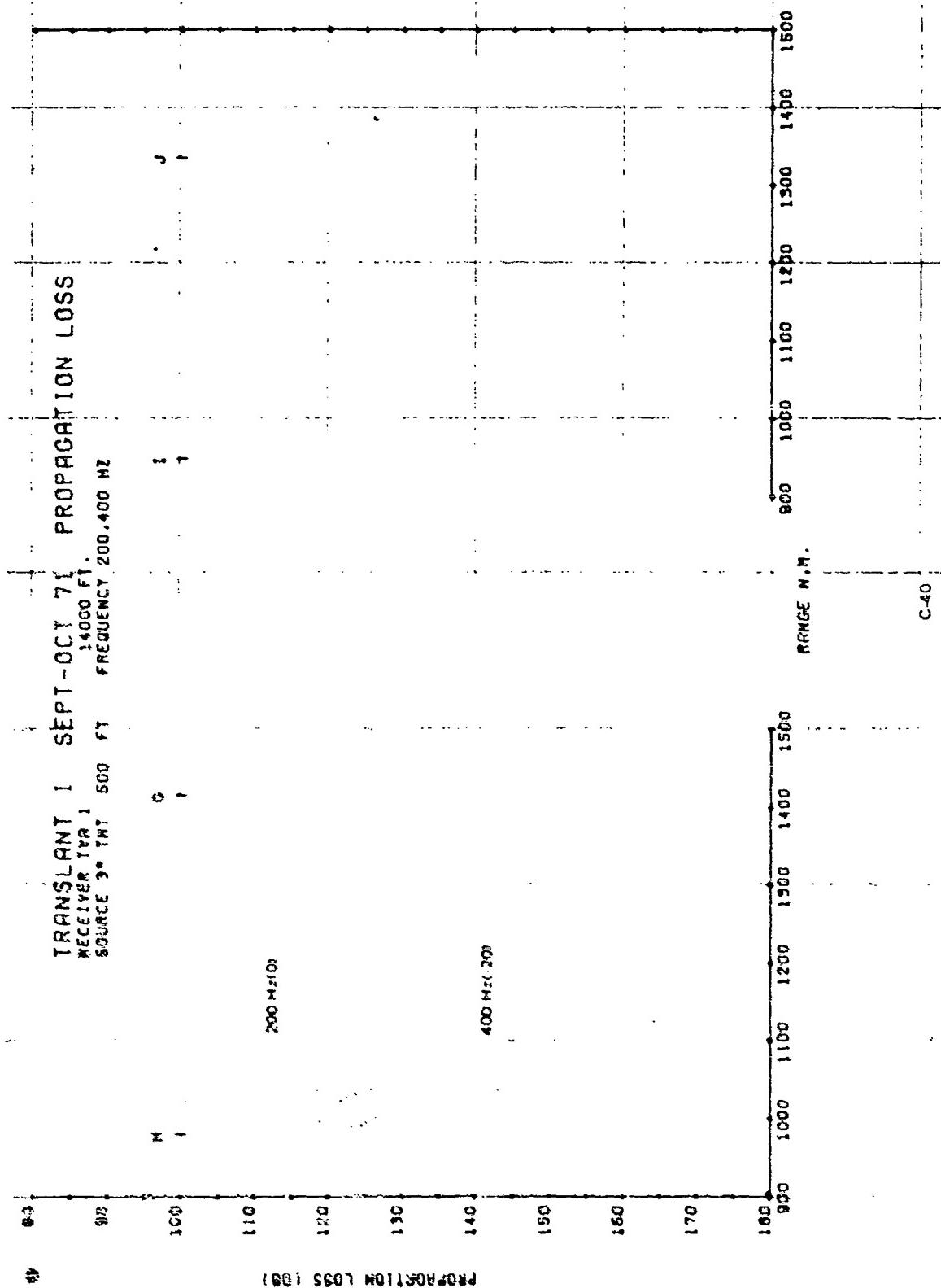
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PROTECTION LOSS

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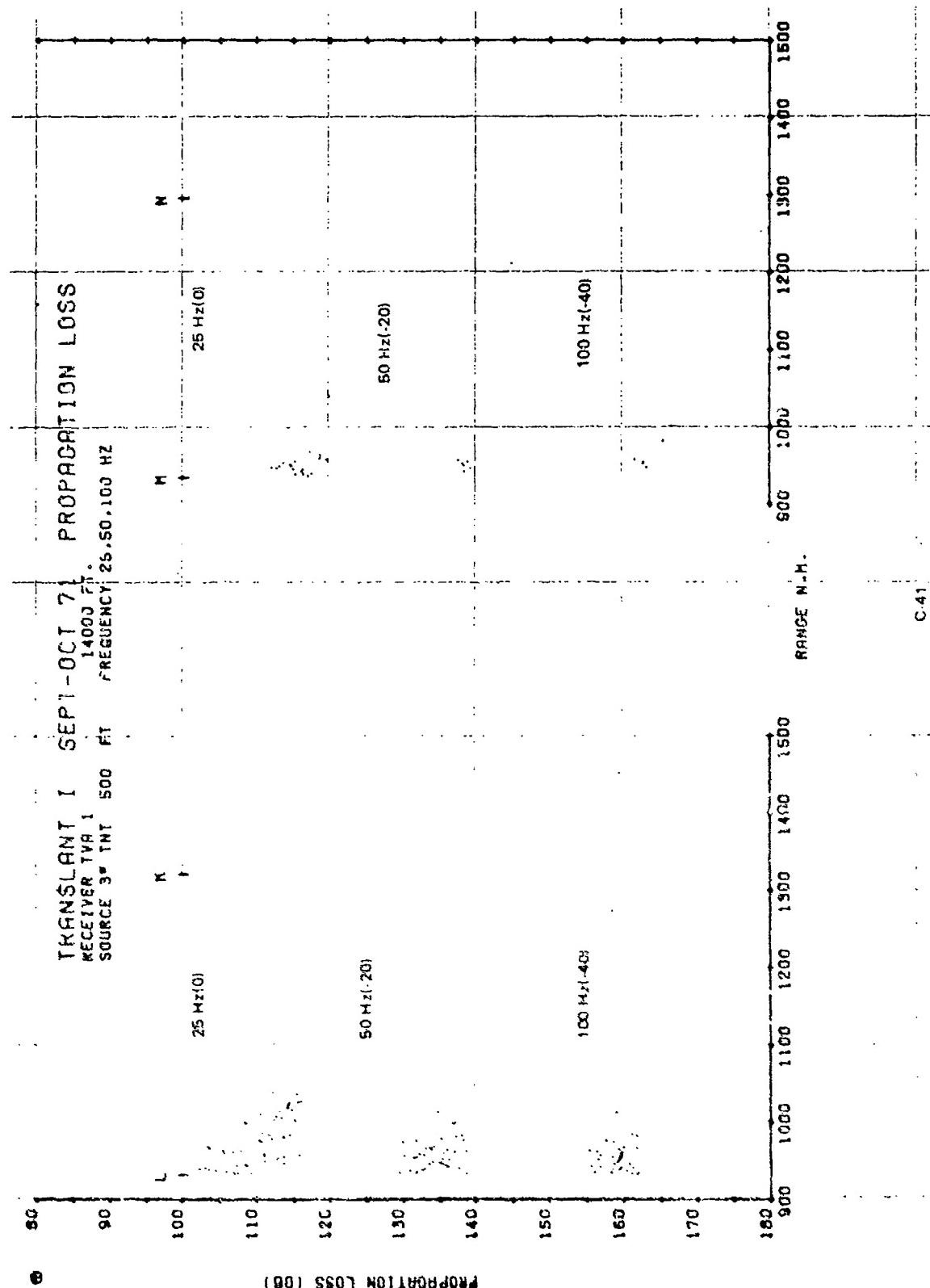


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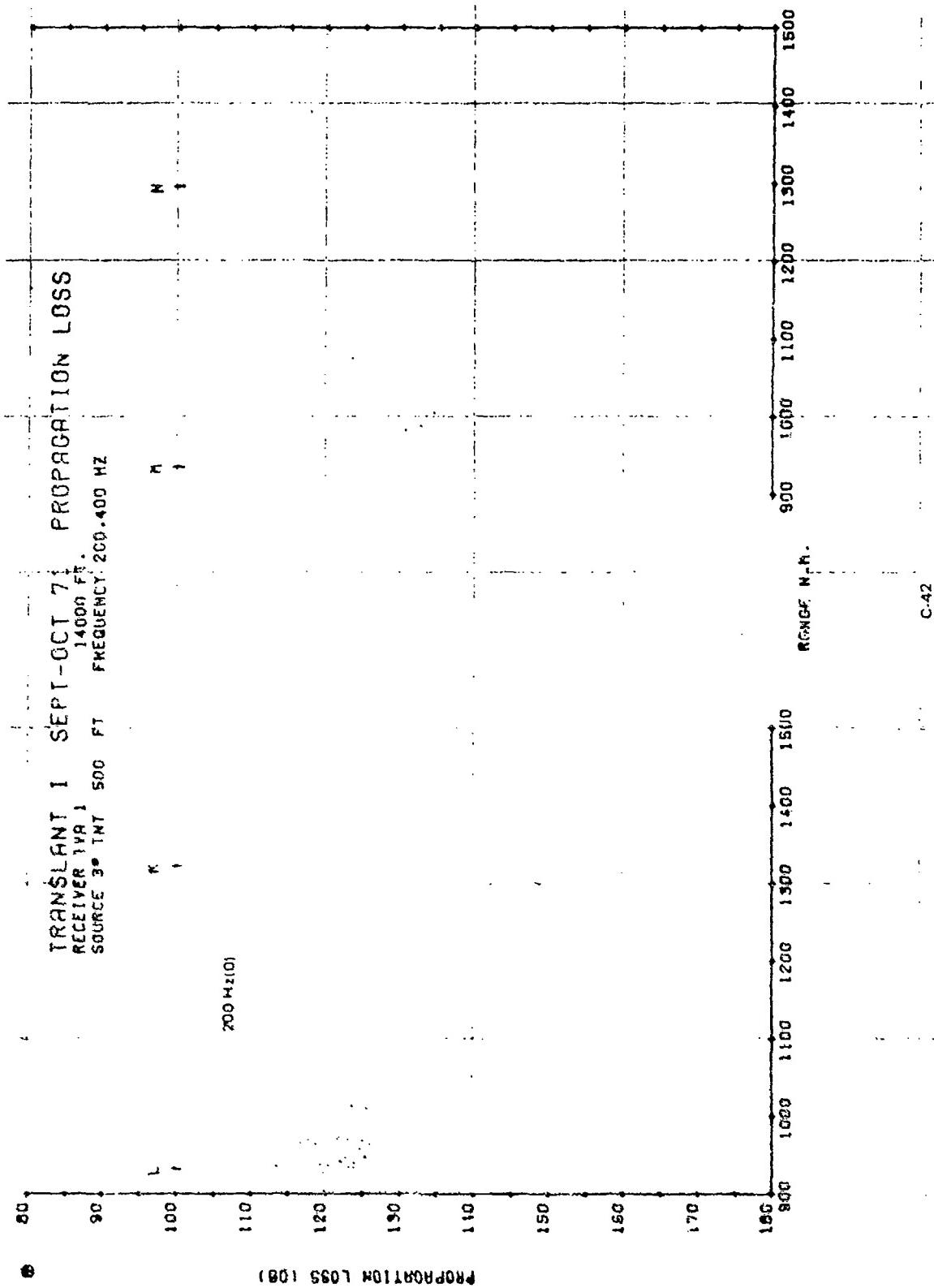


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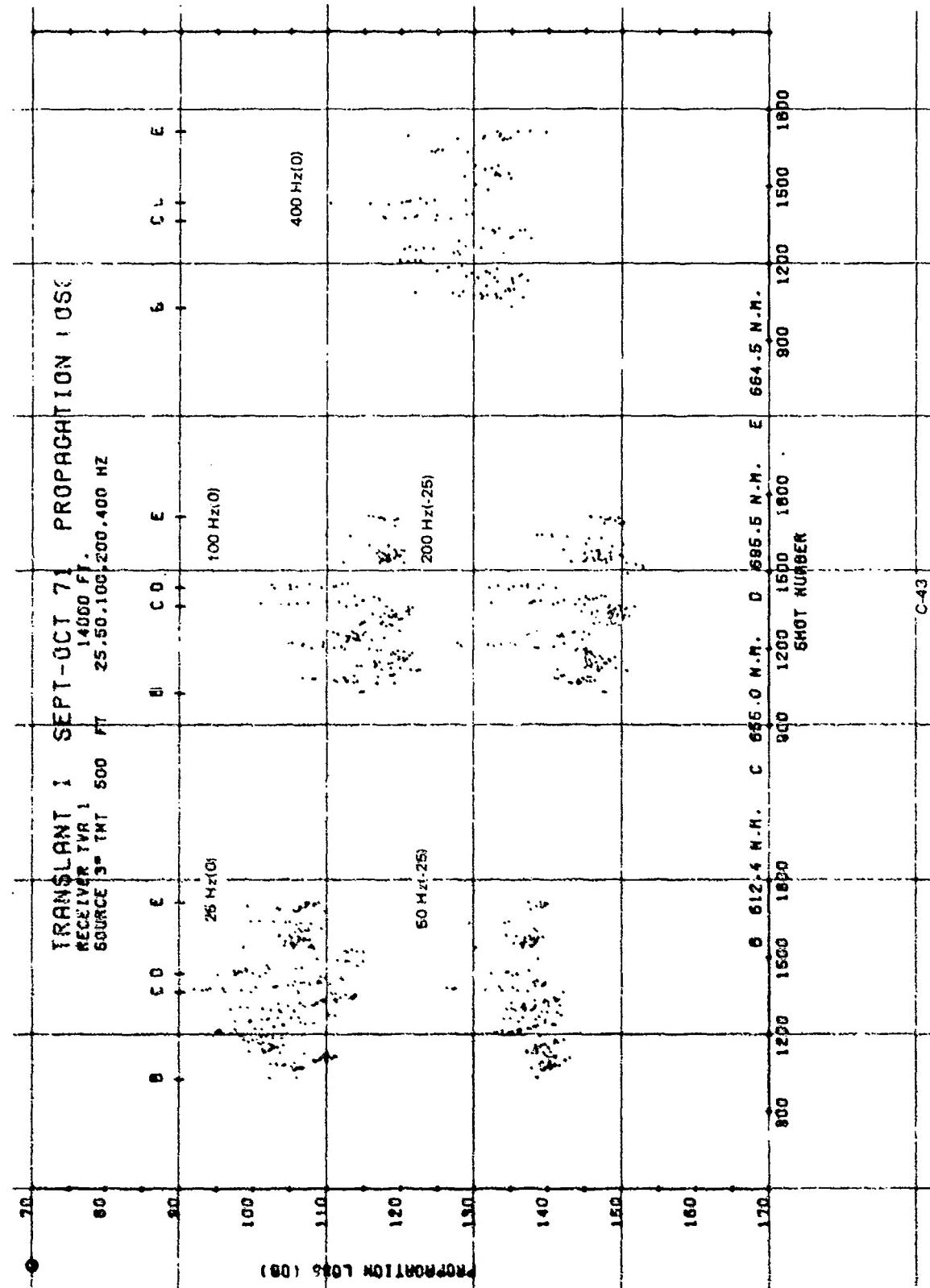


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C-43

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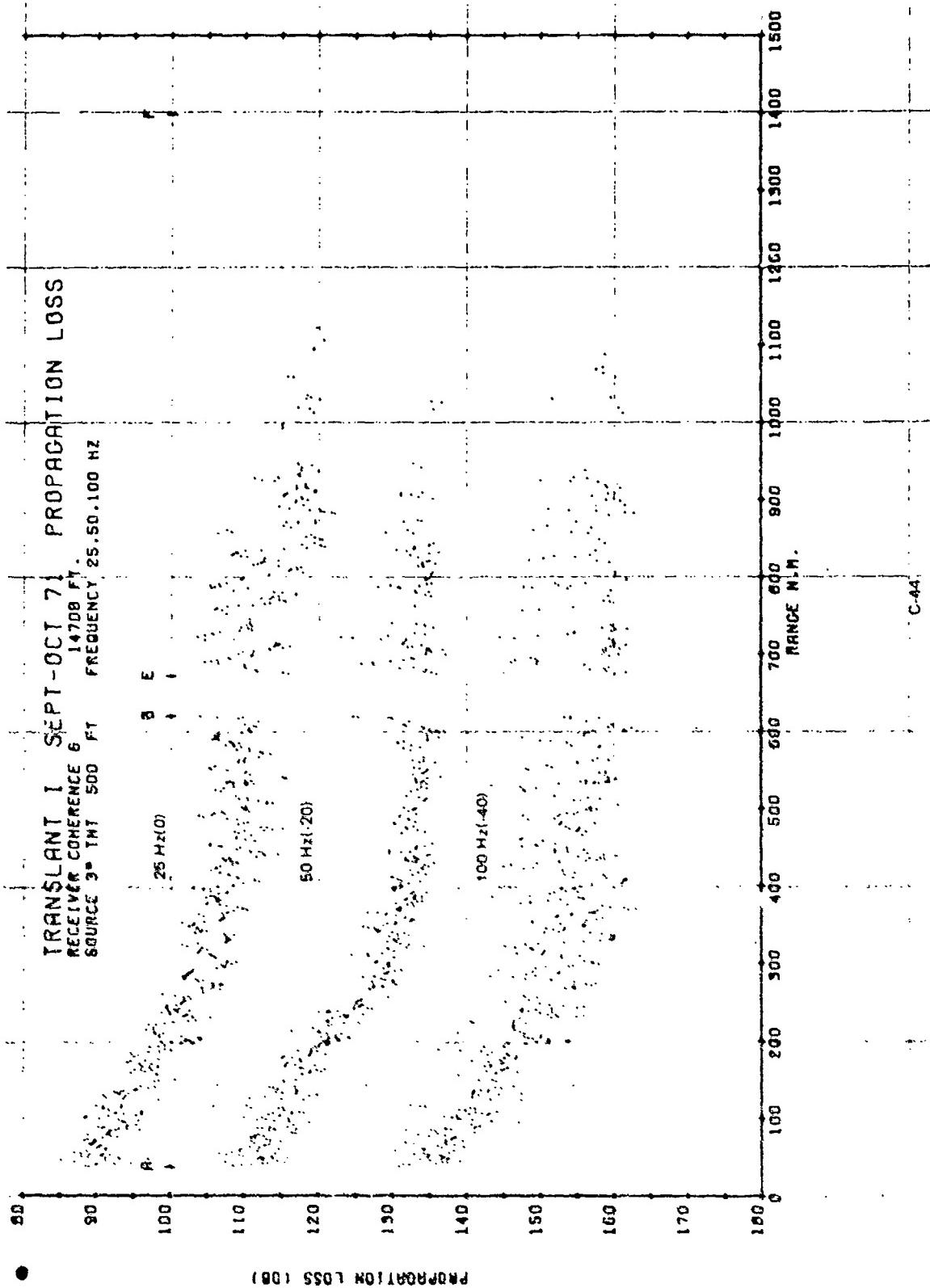


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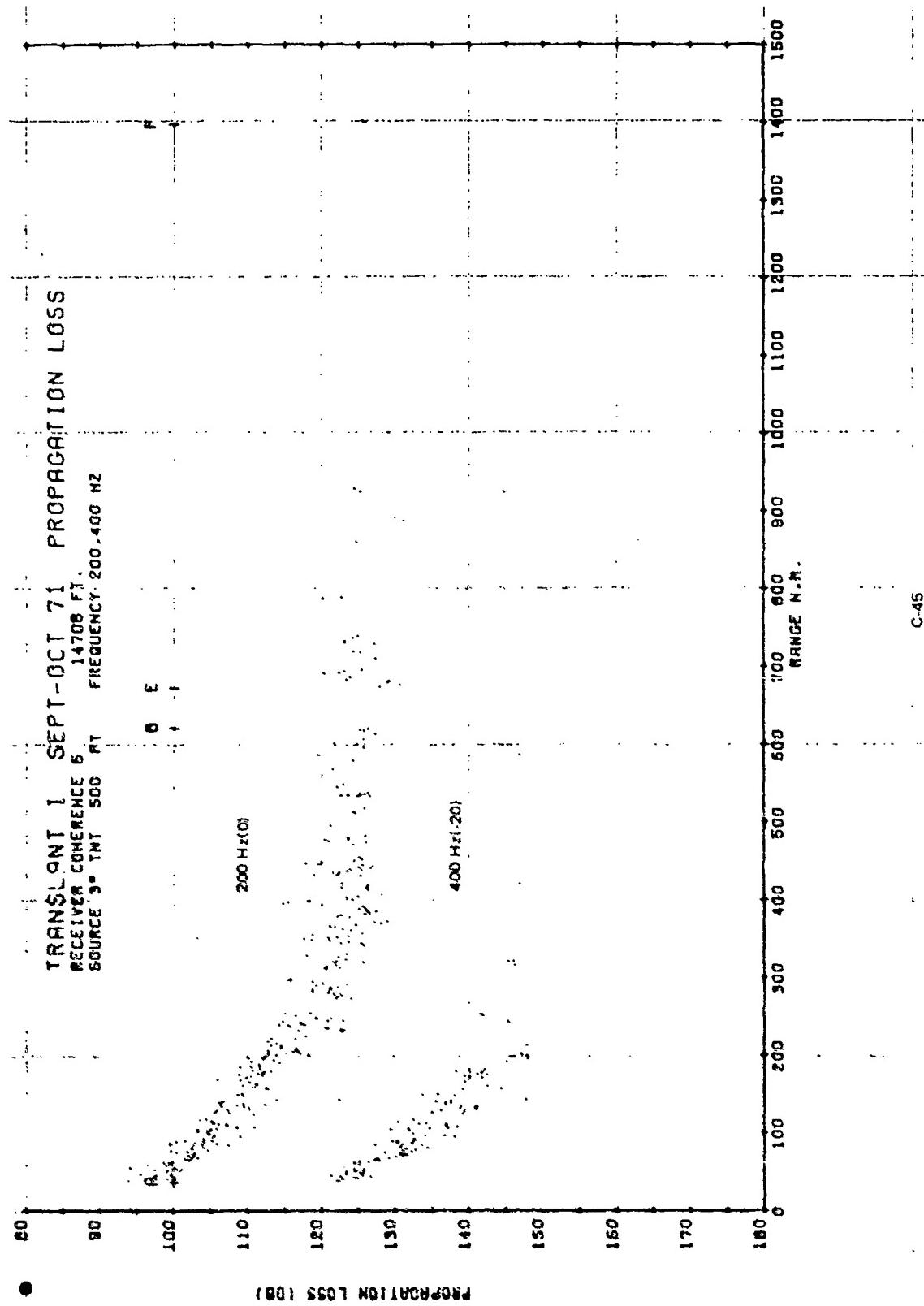


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C-45

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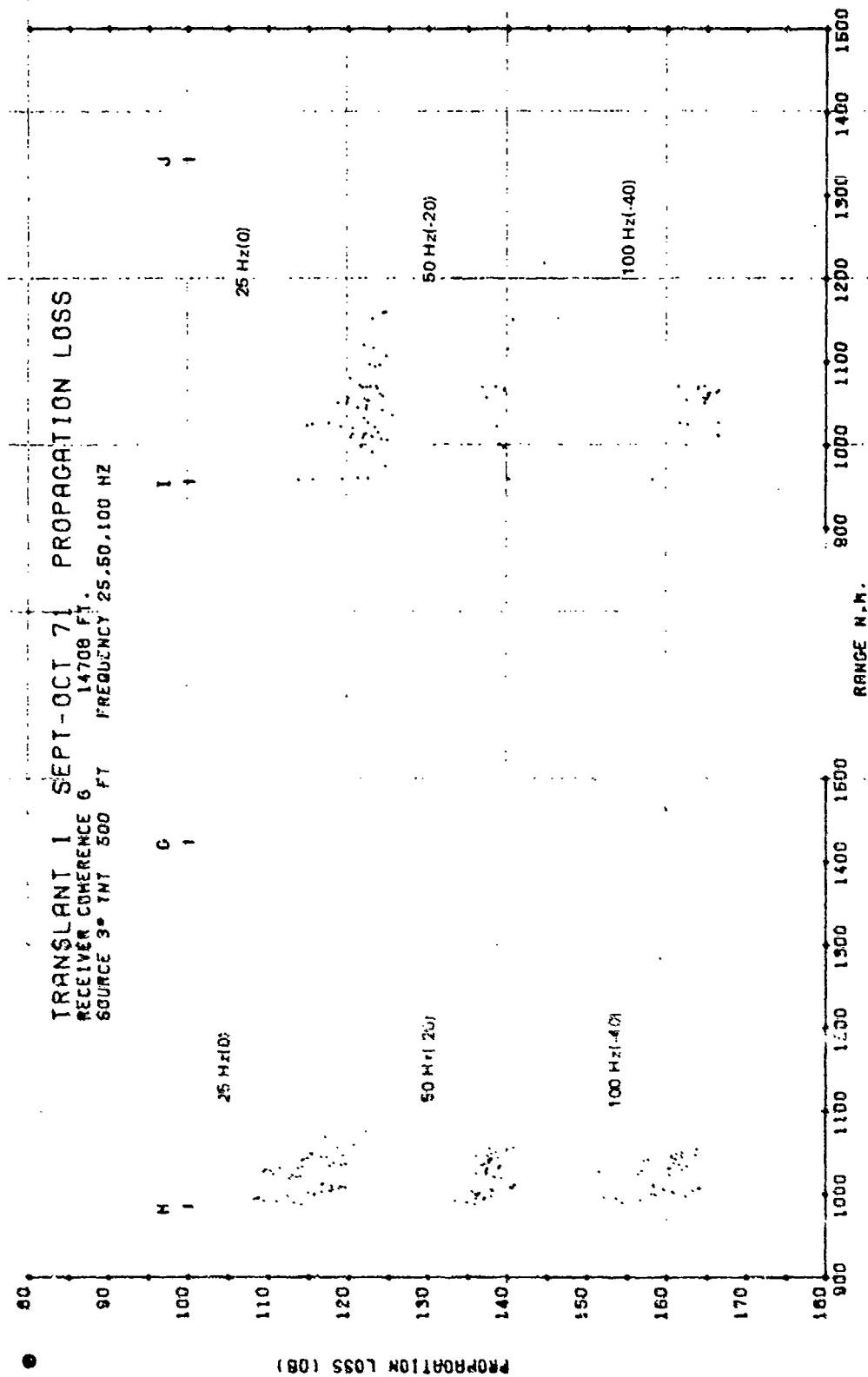


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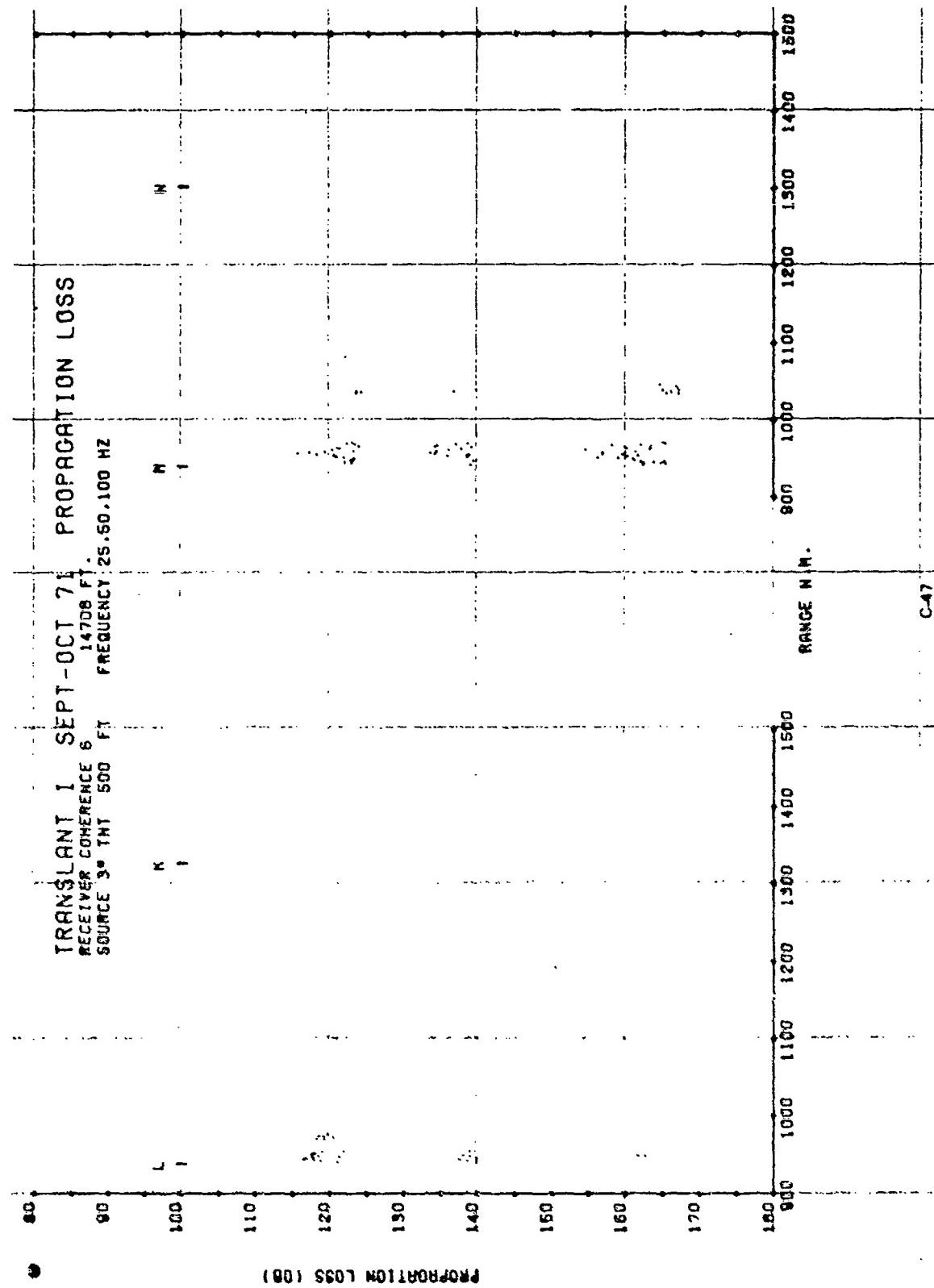
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C-47

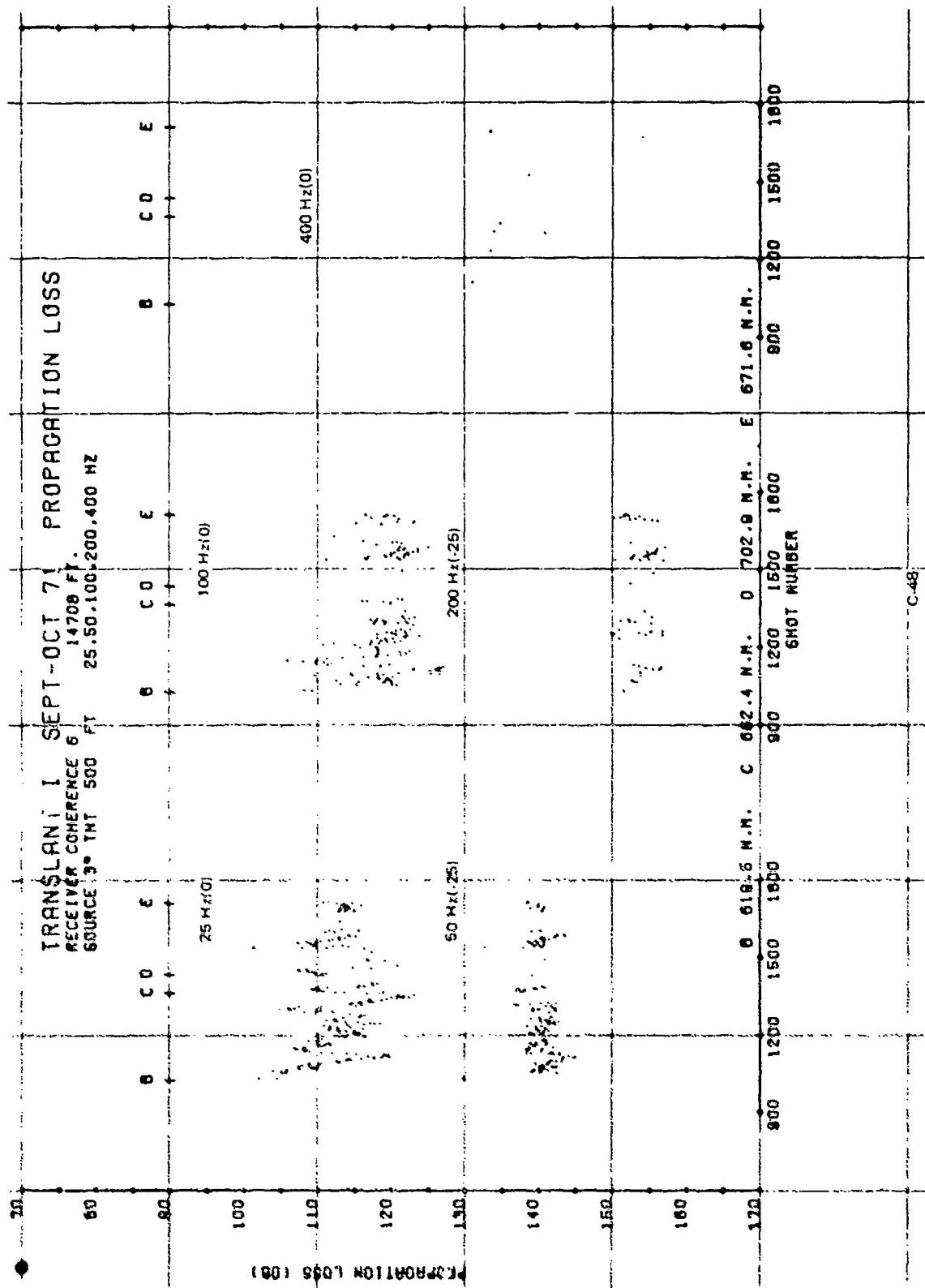
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TR 4635



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C-49/C-50

UNCLASSIFIED

TR 4635

Appendix D

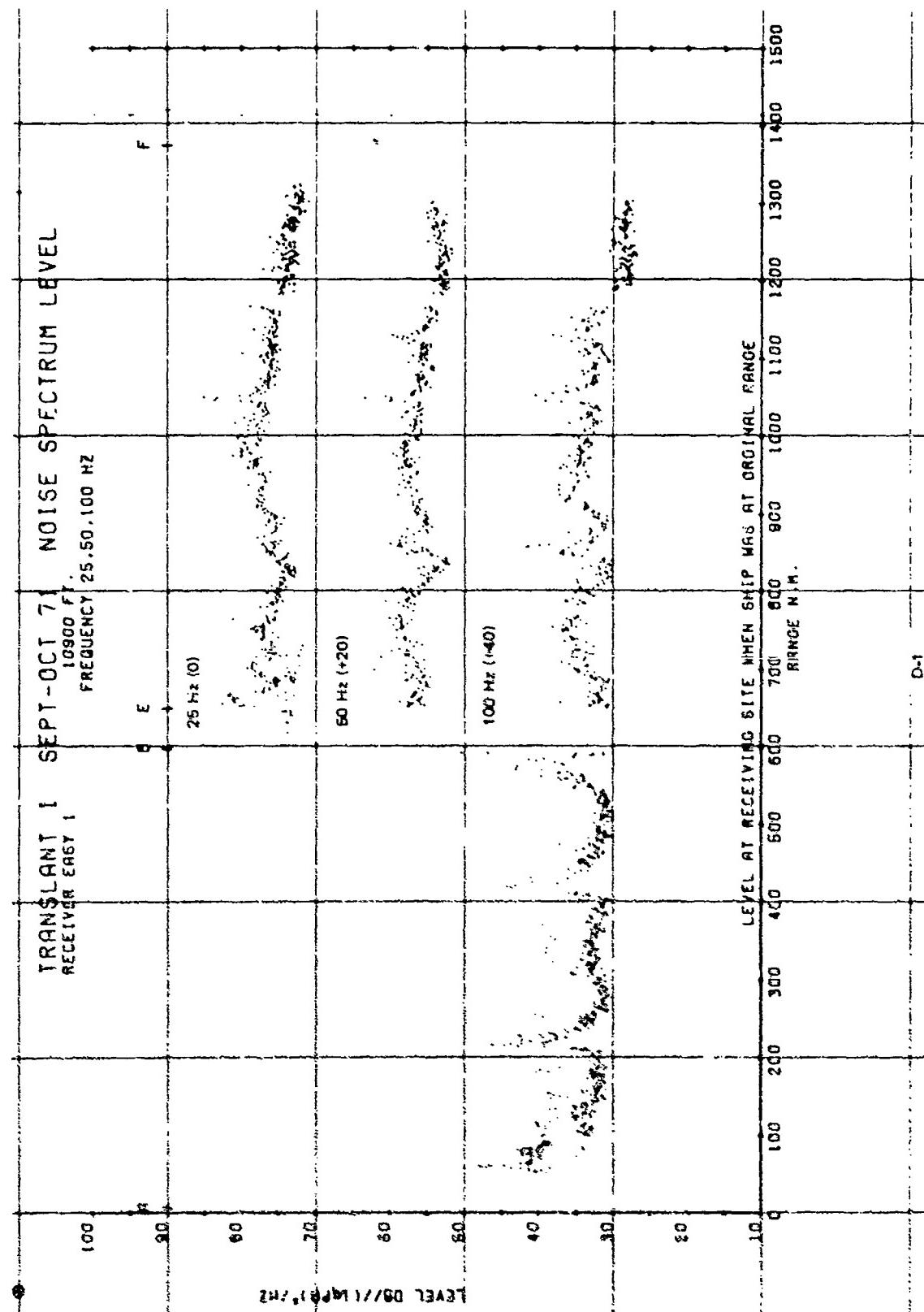
TRANSLANT I BACKGROUND NOISE SPECTRUM LEVELS

The background noise spectrum levels as a function of time, frequency, and hydrophone are presented on the following pages.

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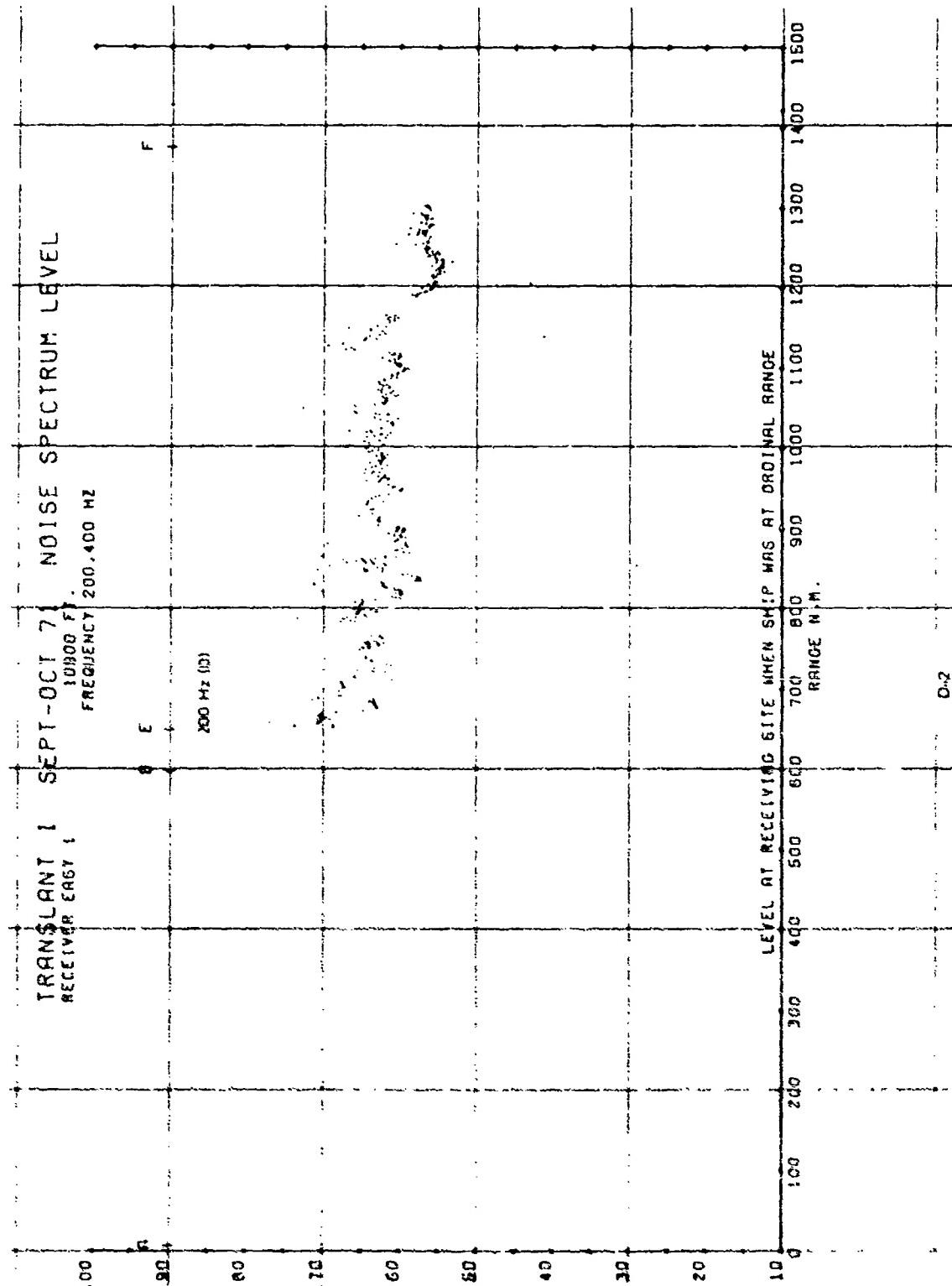
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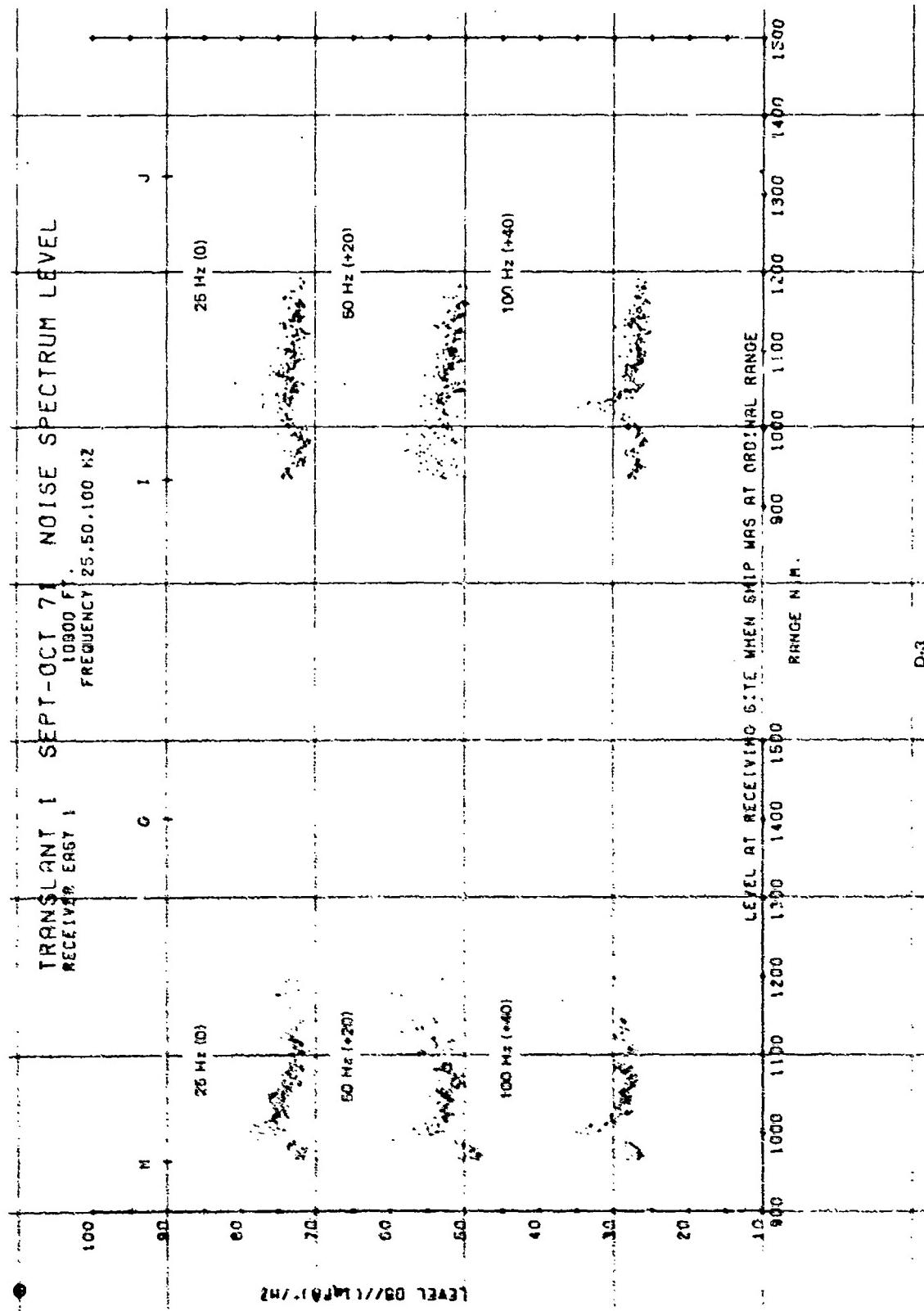


24/148-11/60 23437

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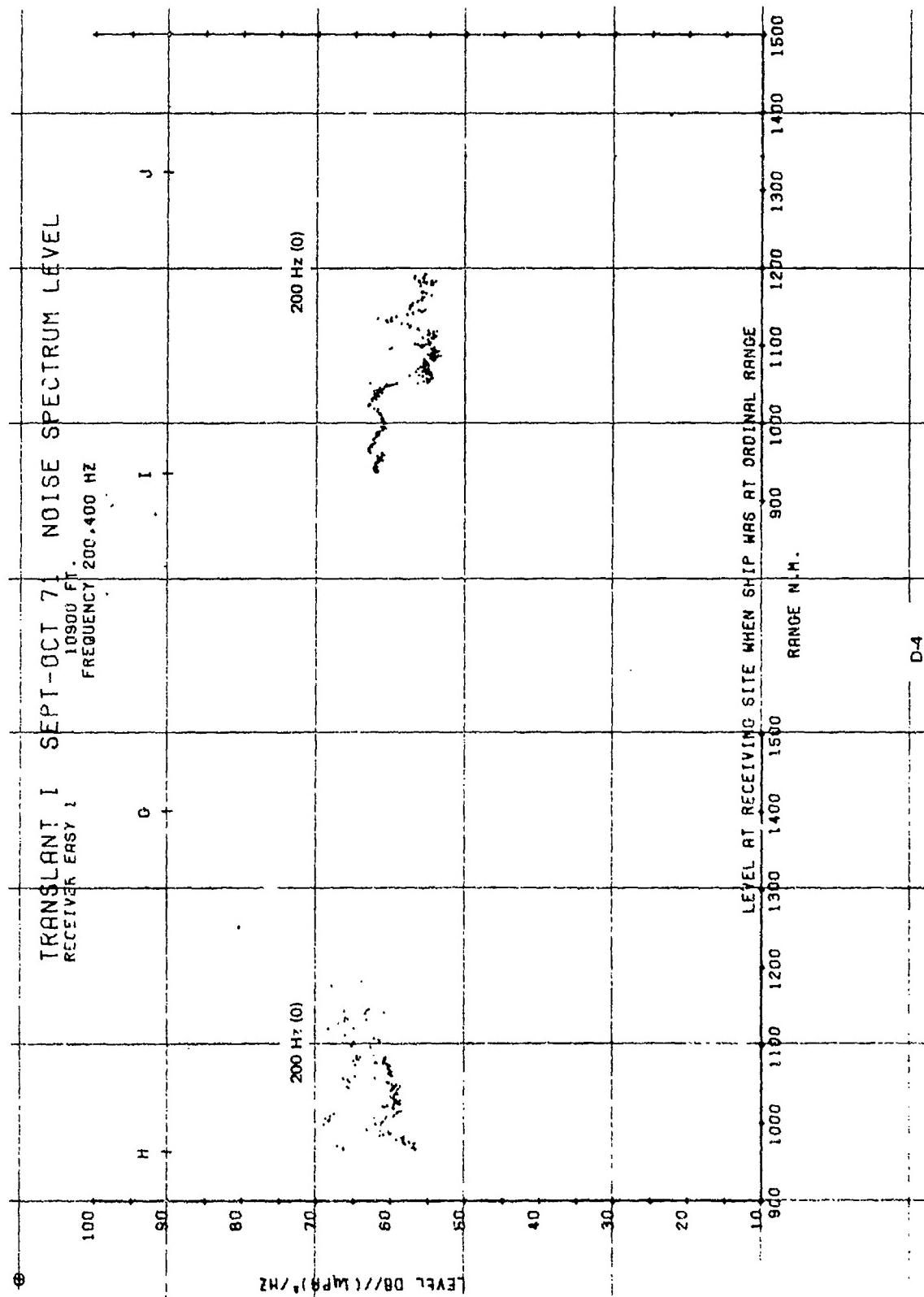
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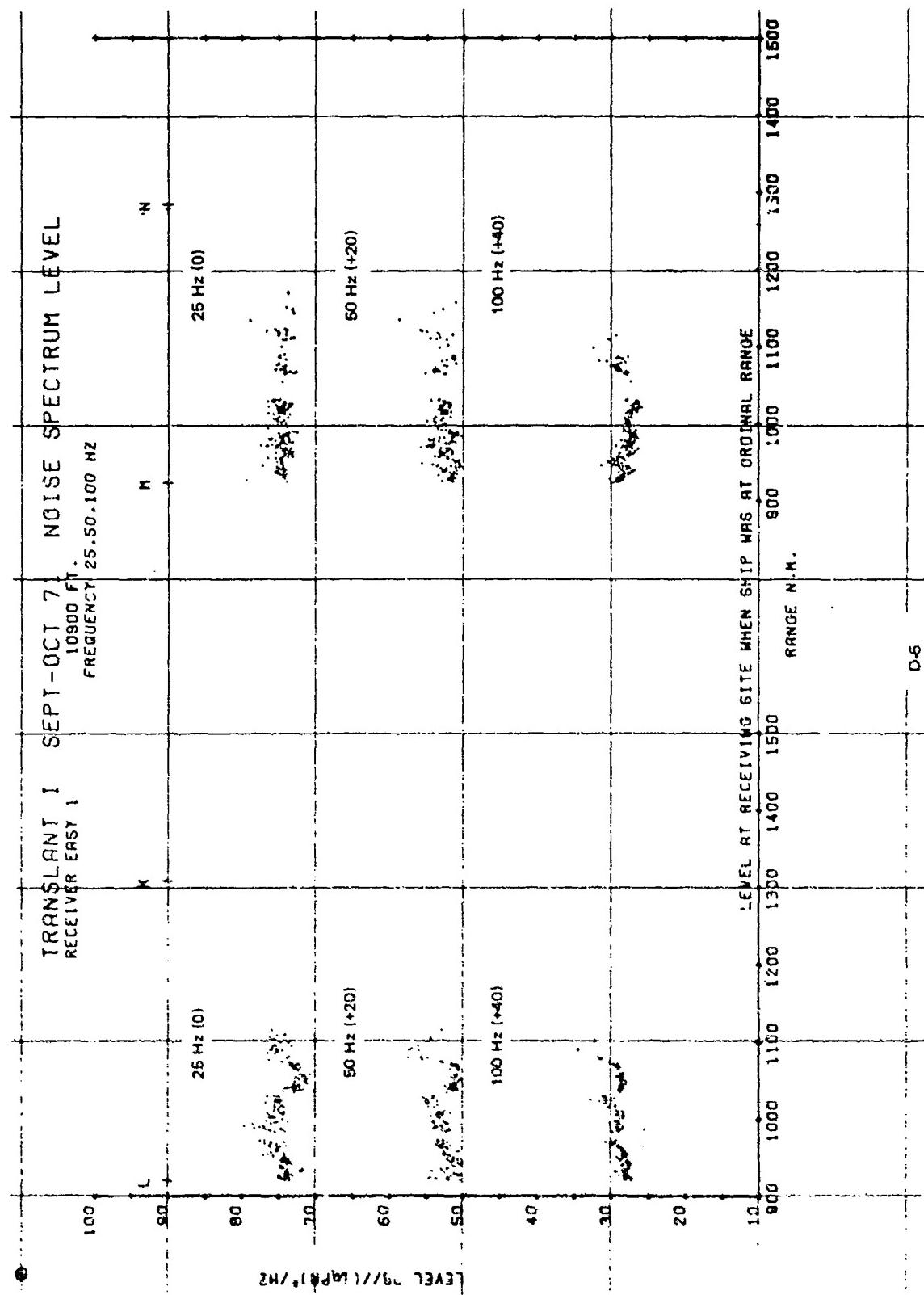


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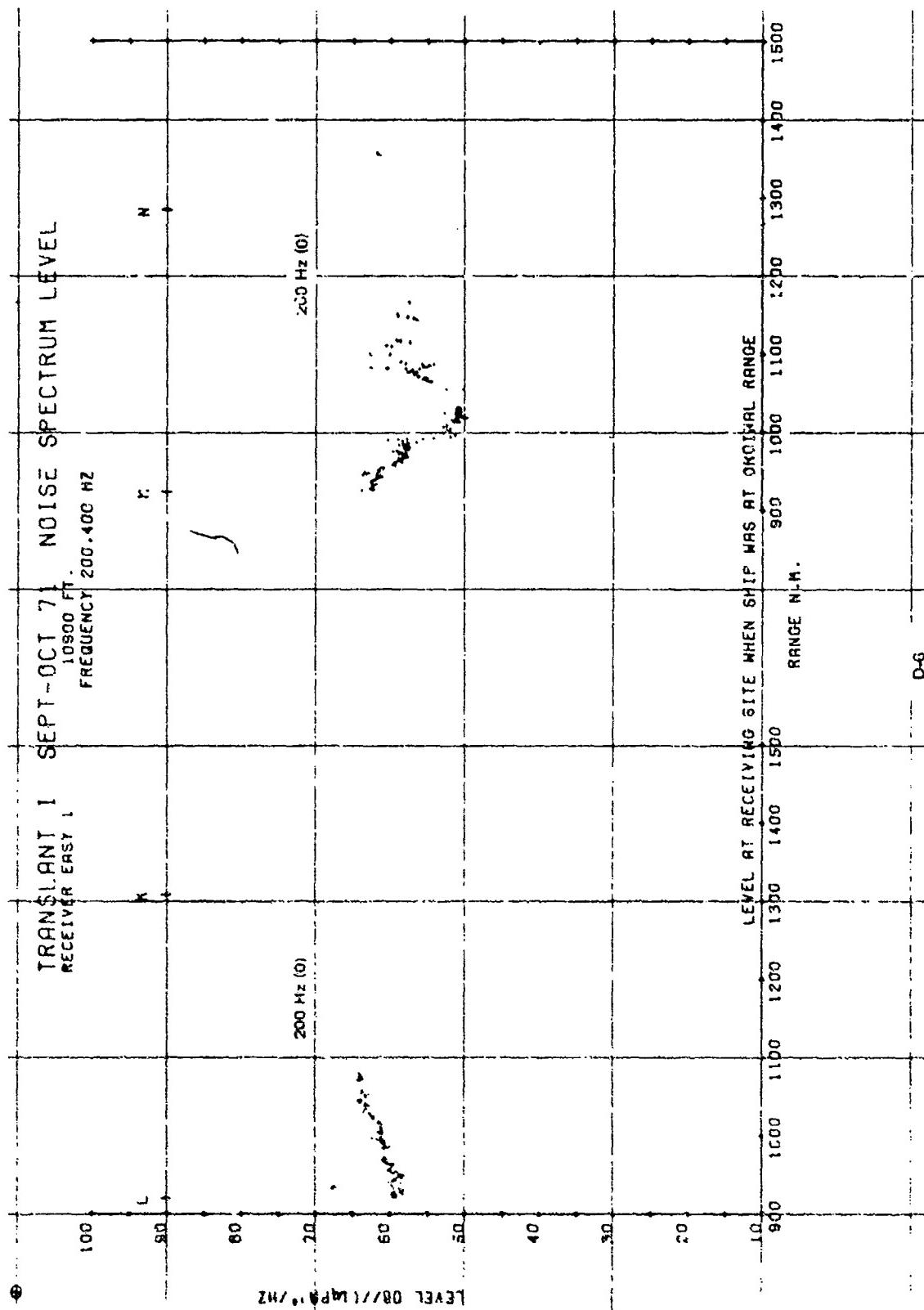
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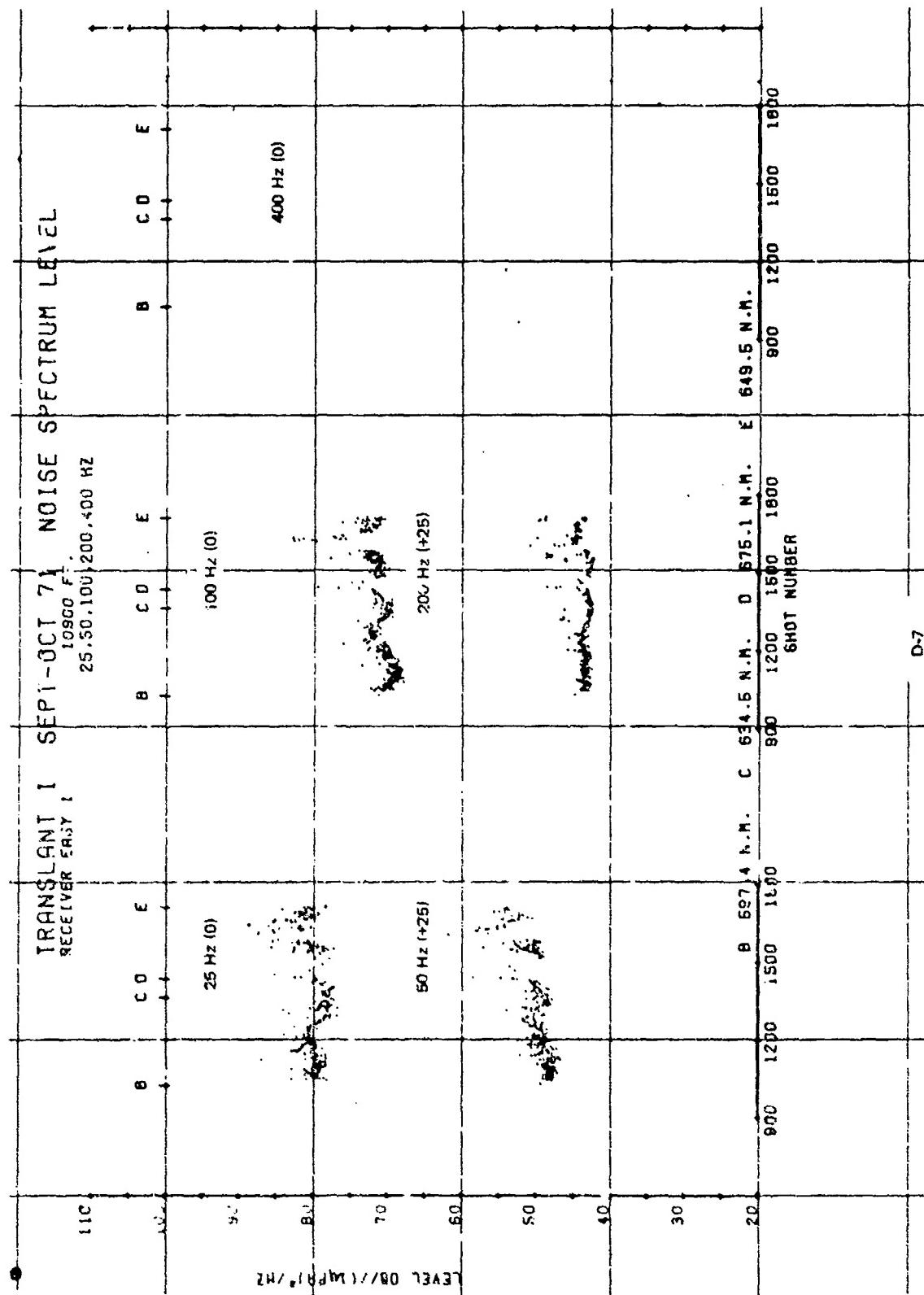


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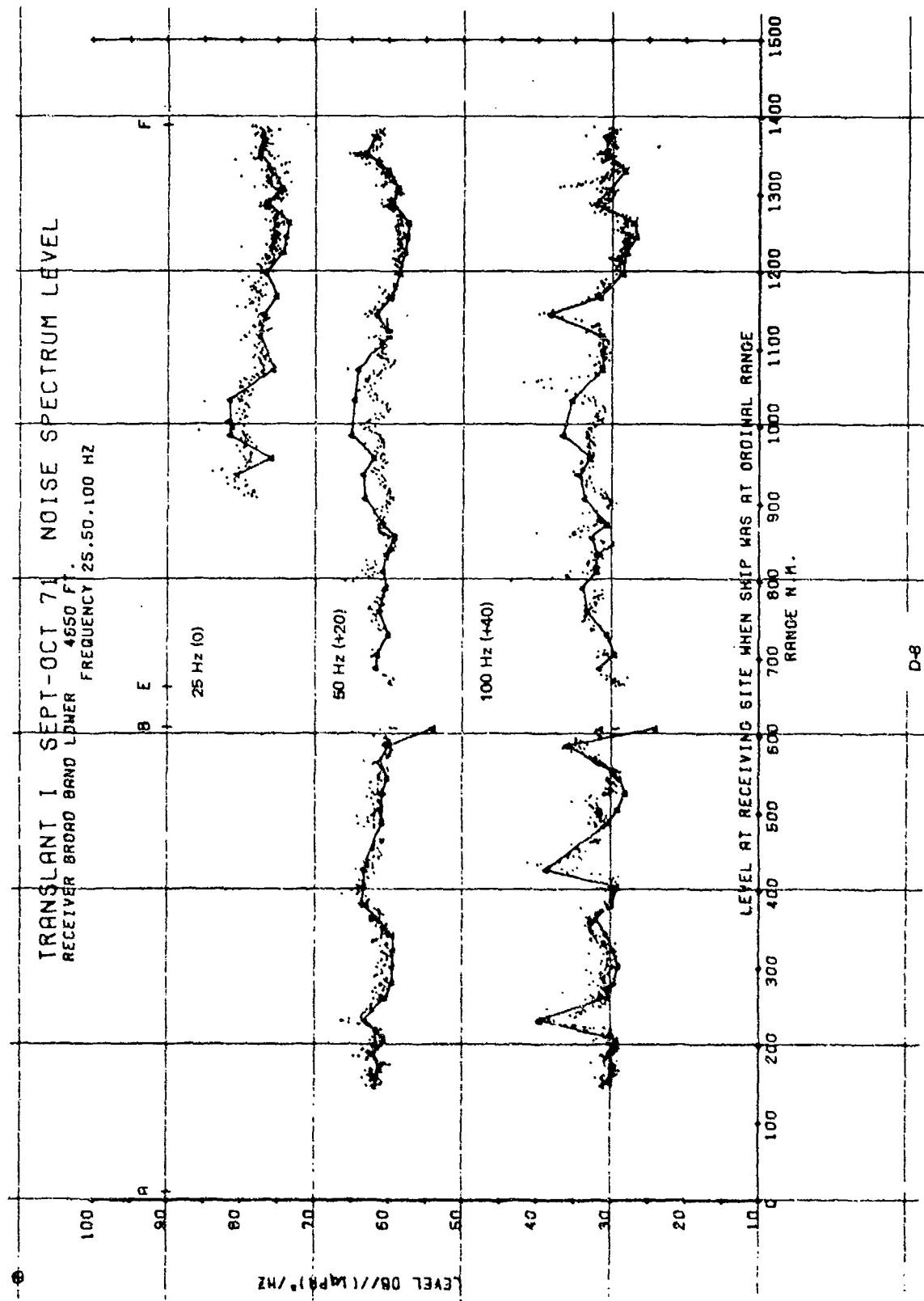
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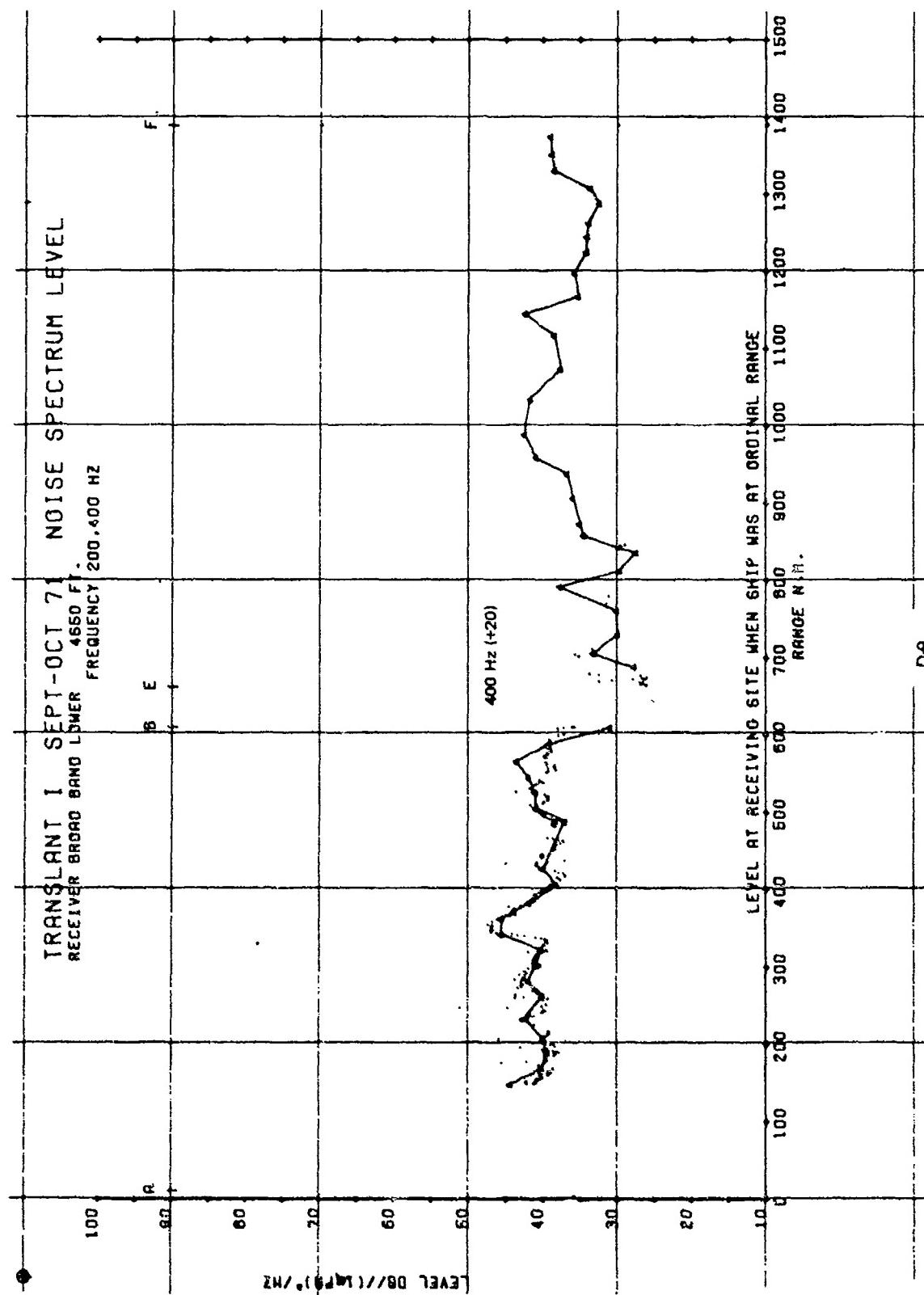


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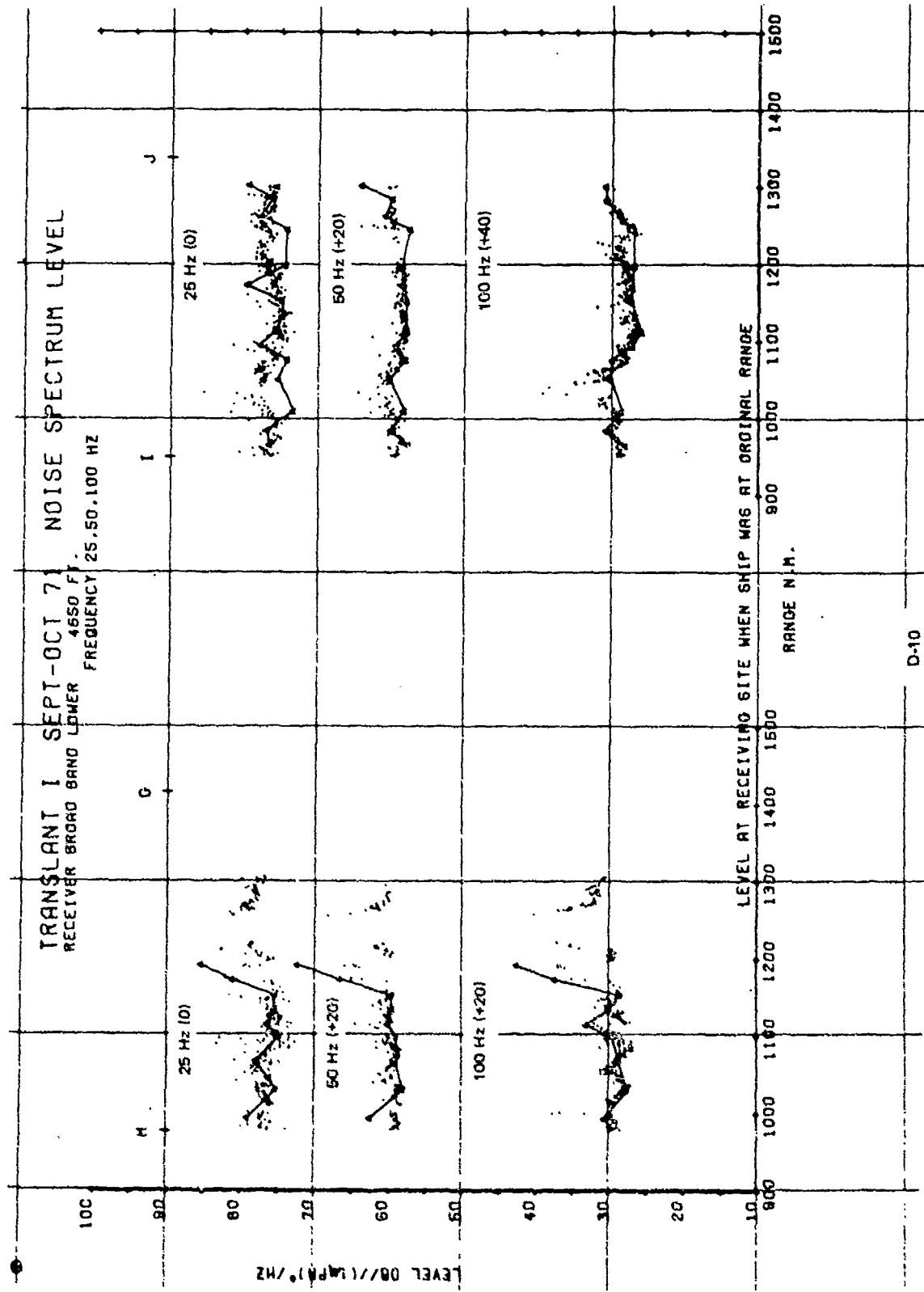


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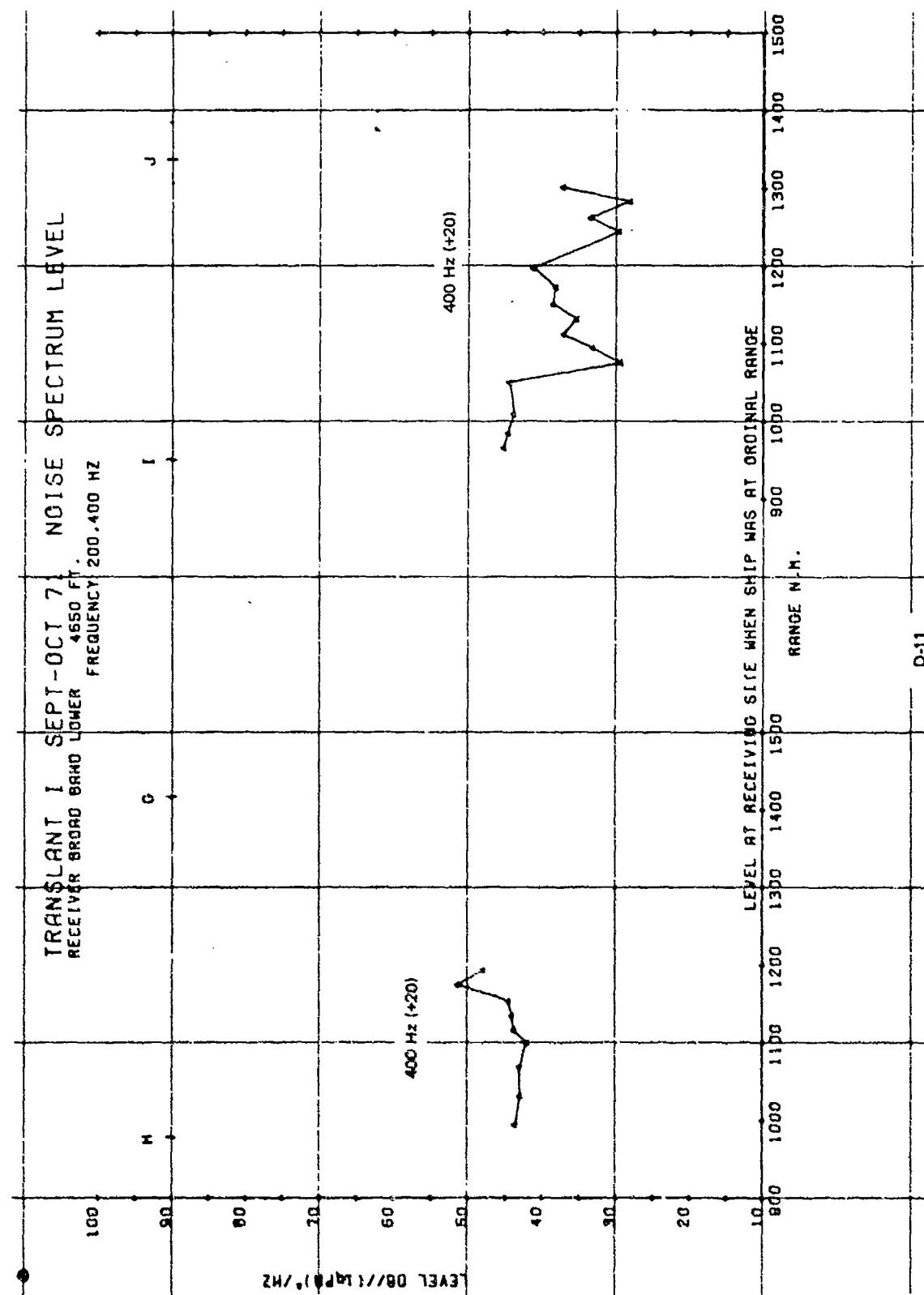


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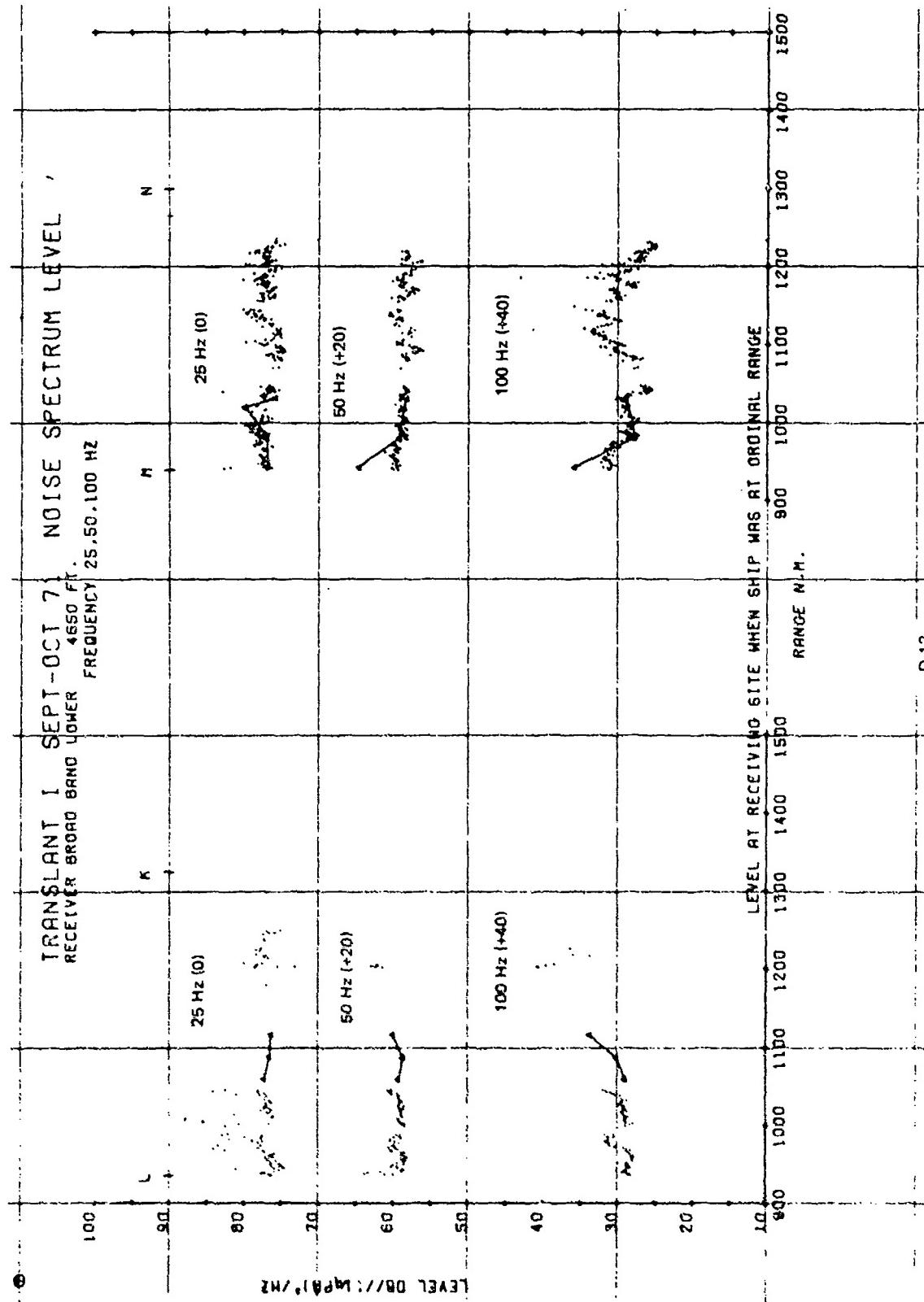


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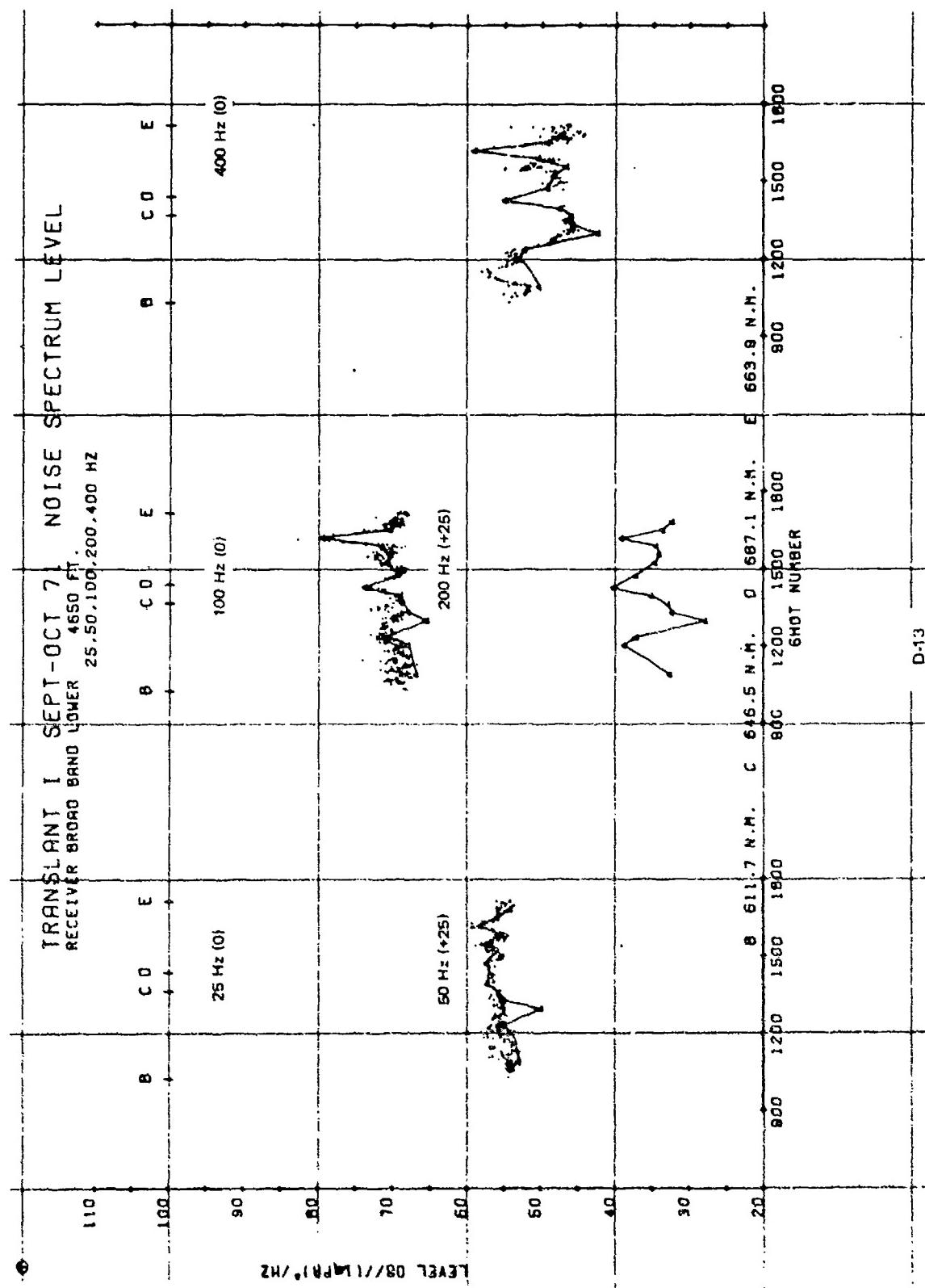


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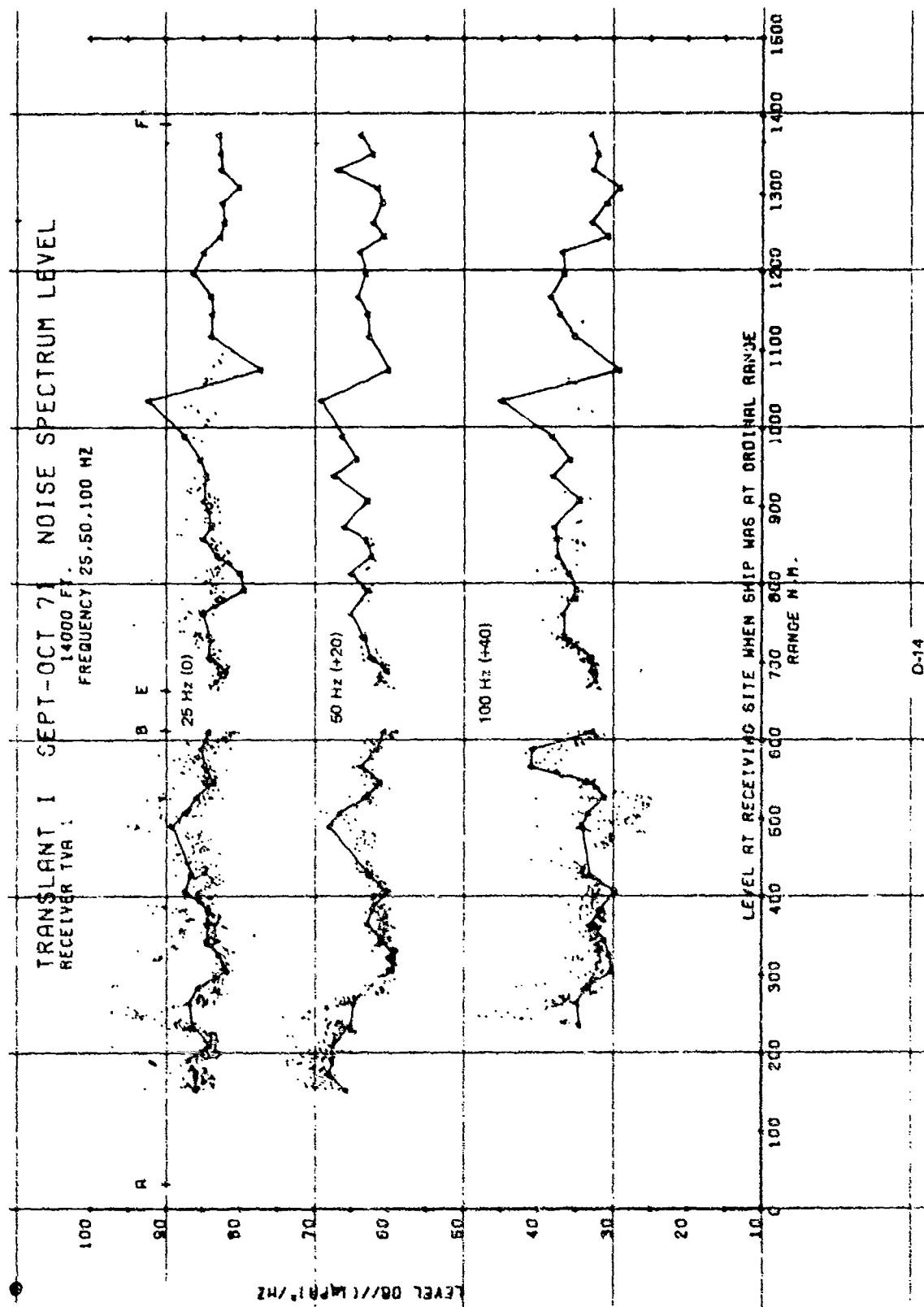


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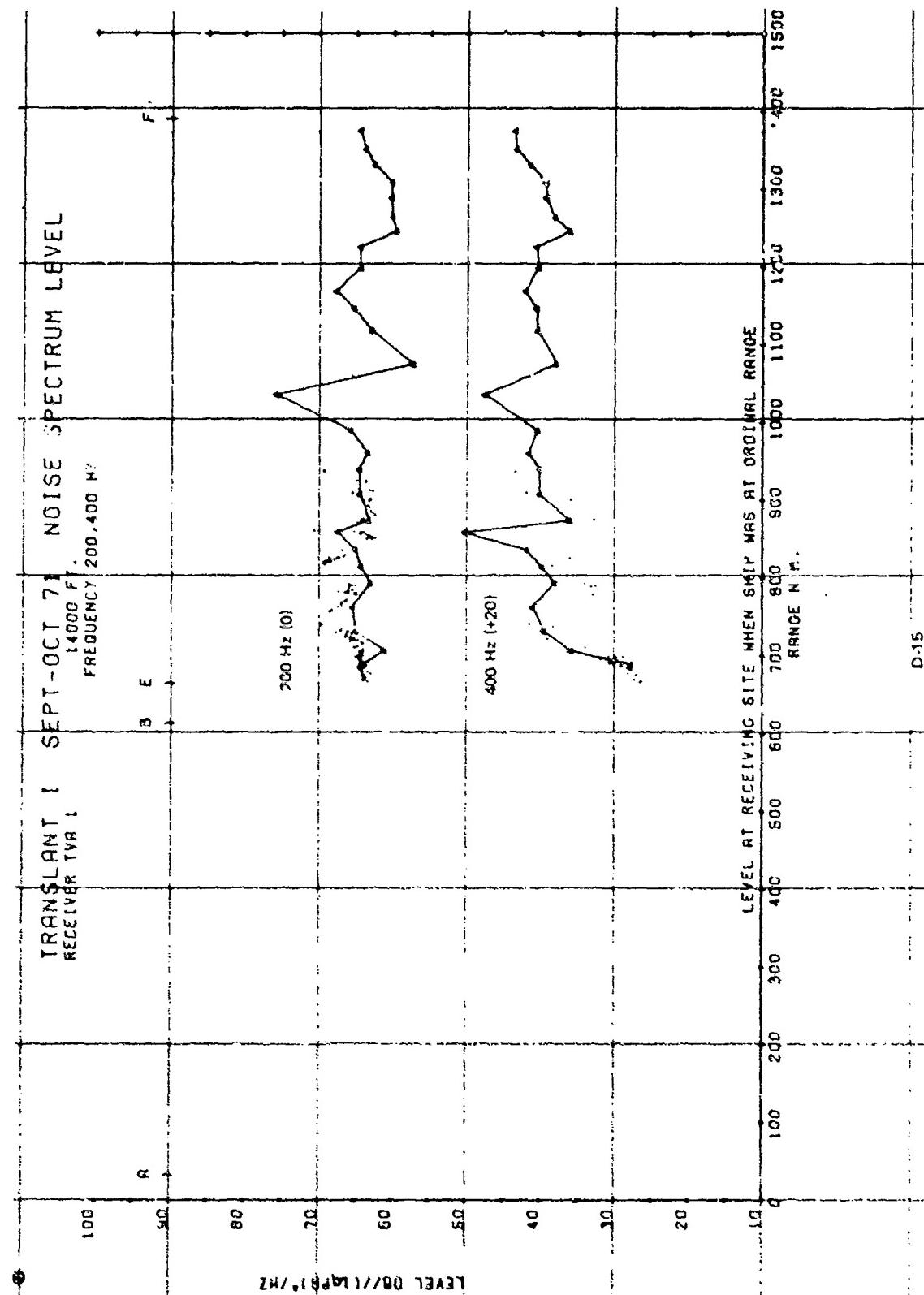


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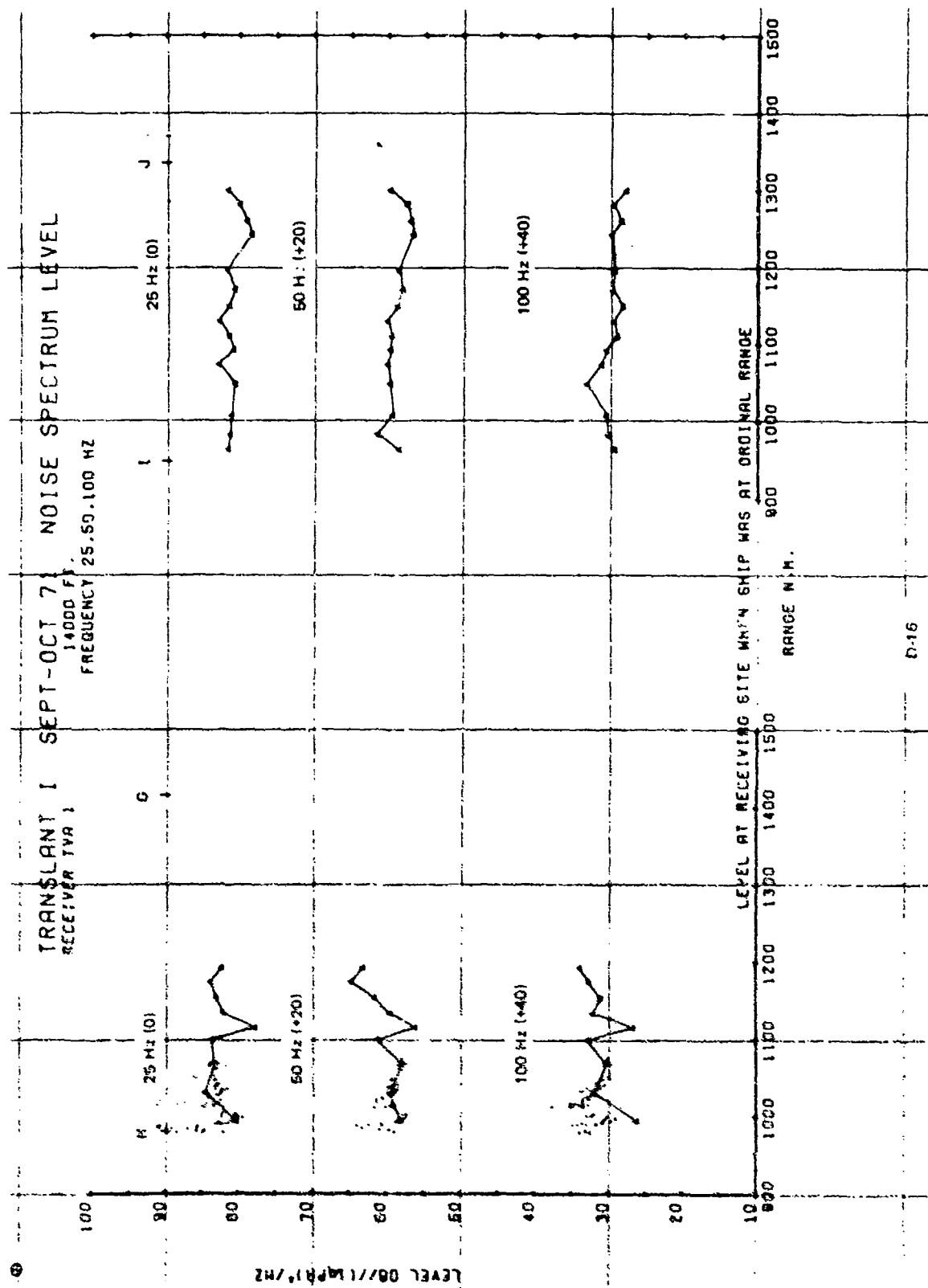


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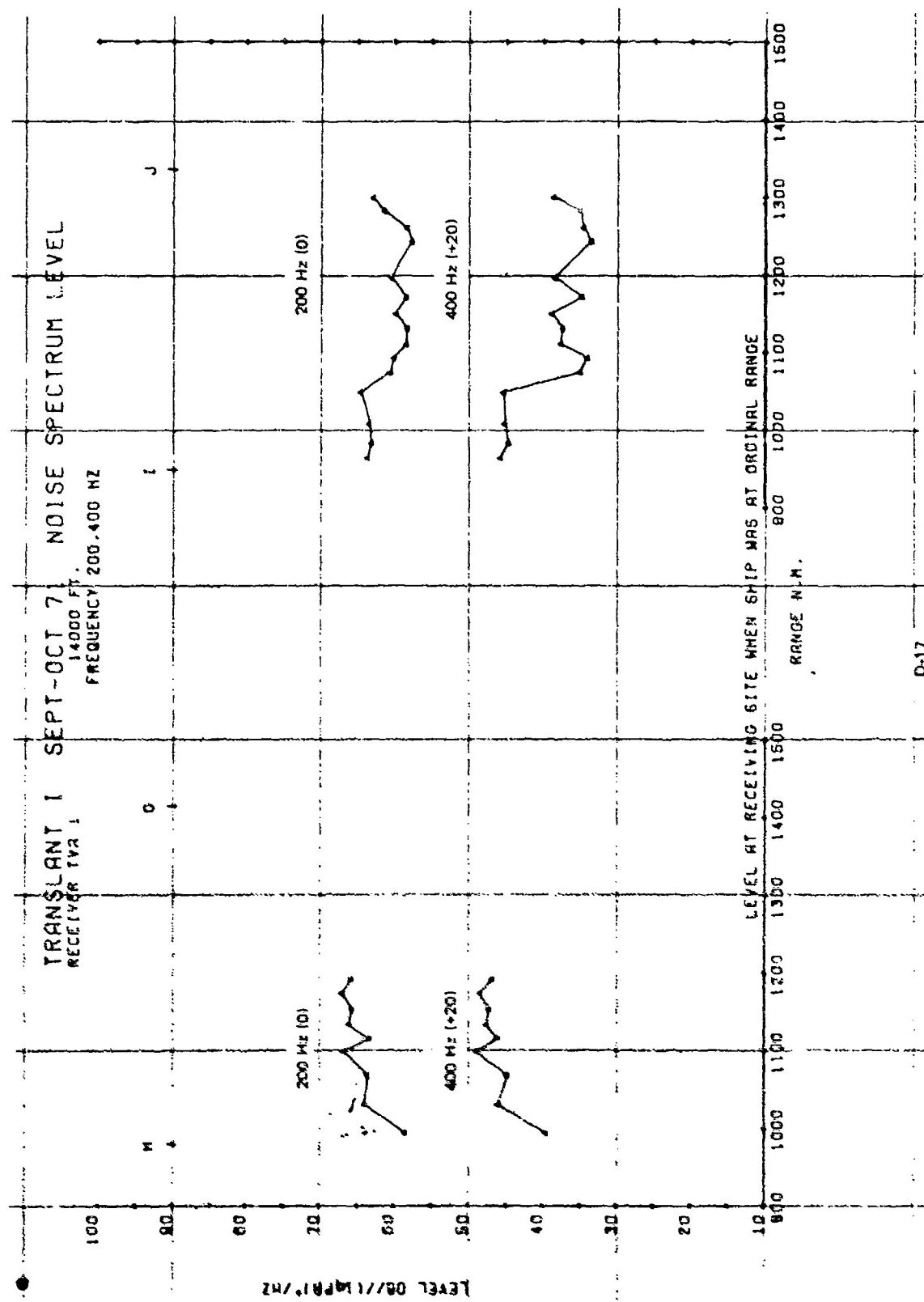


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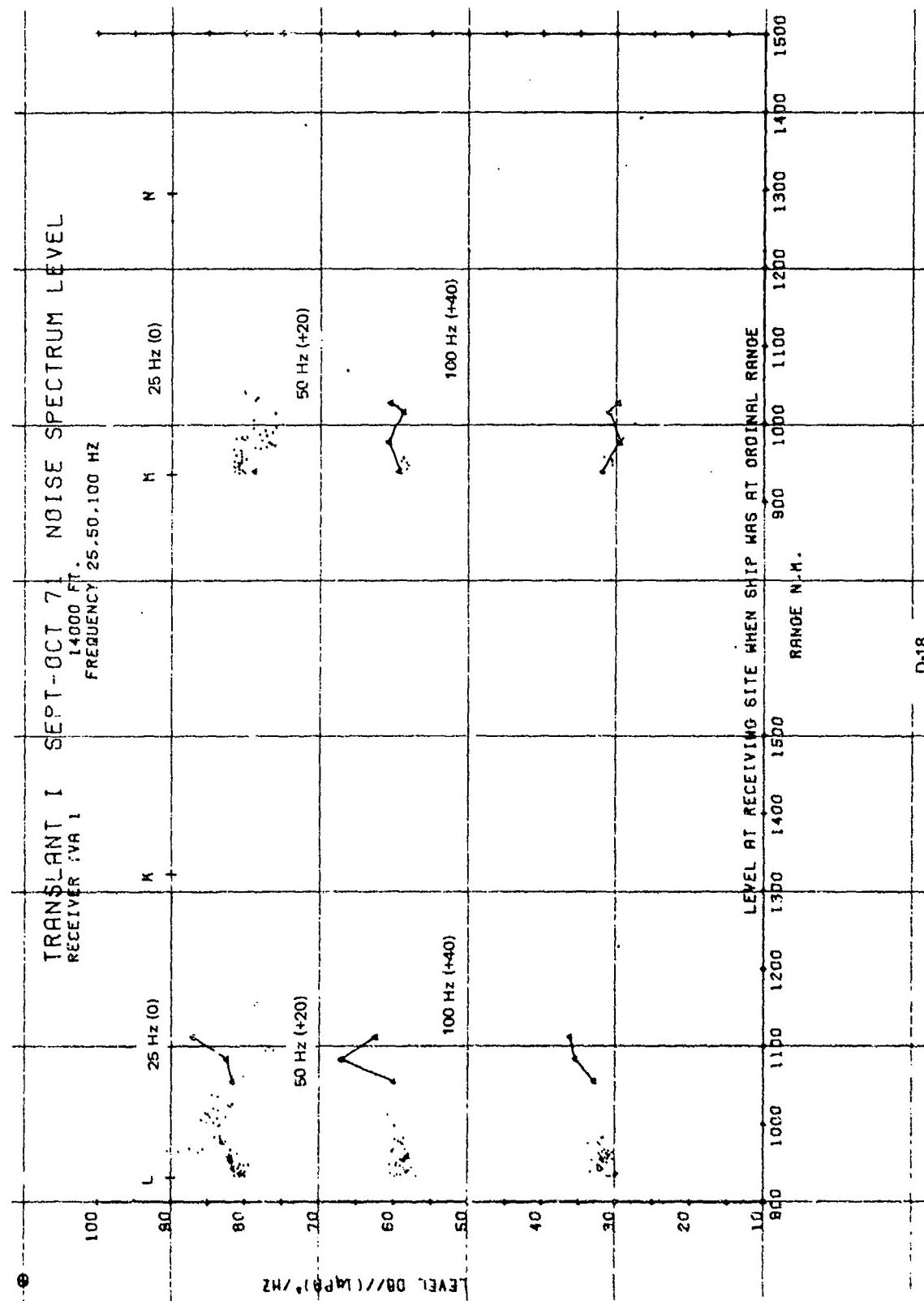


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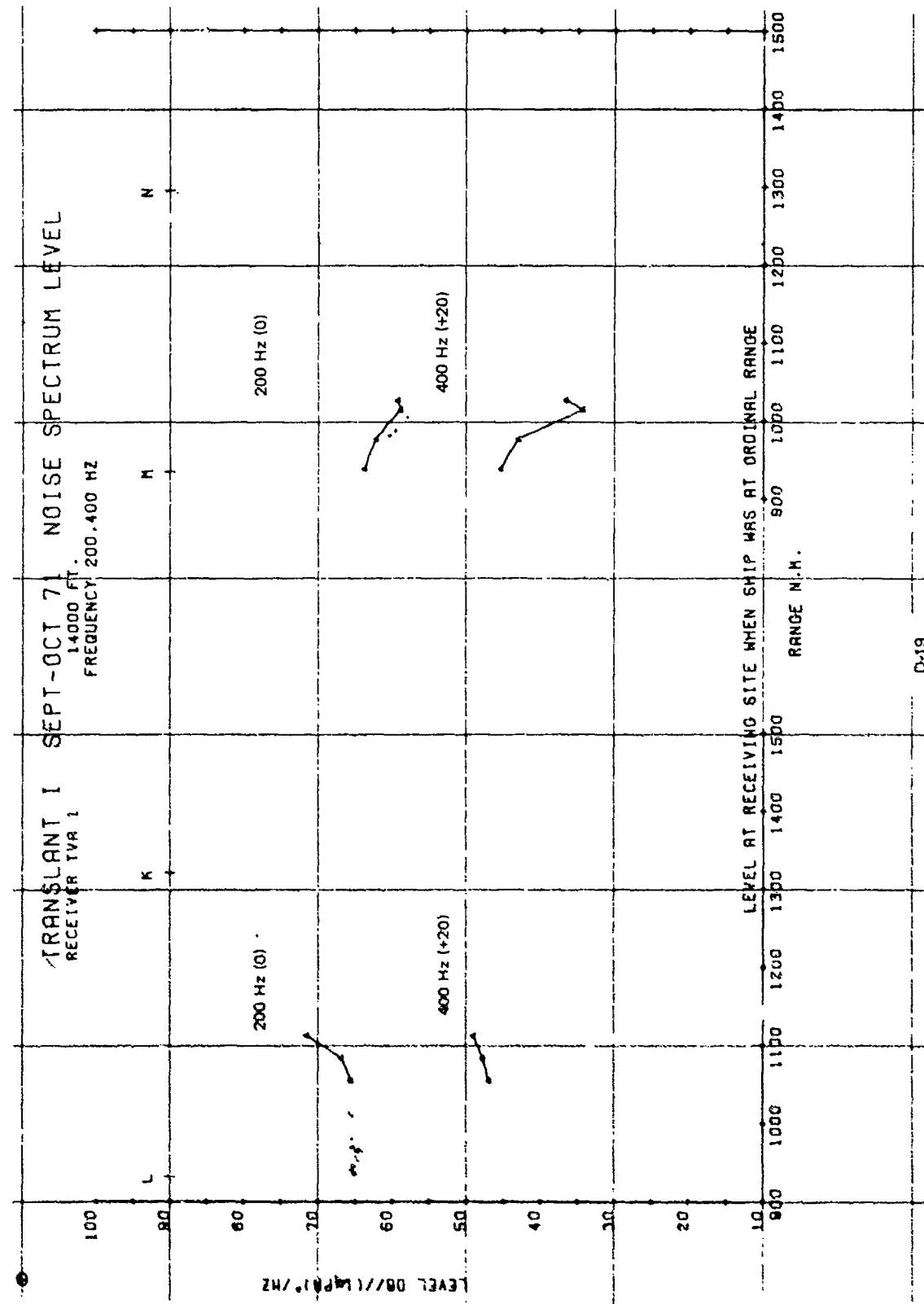
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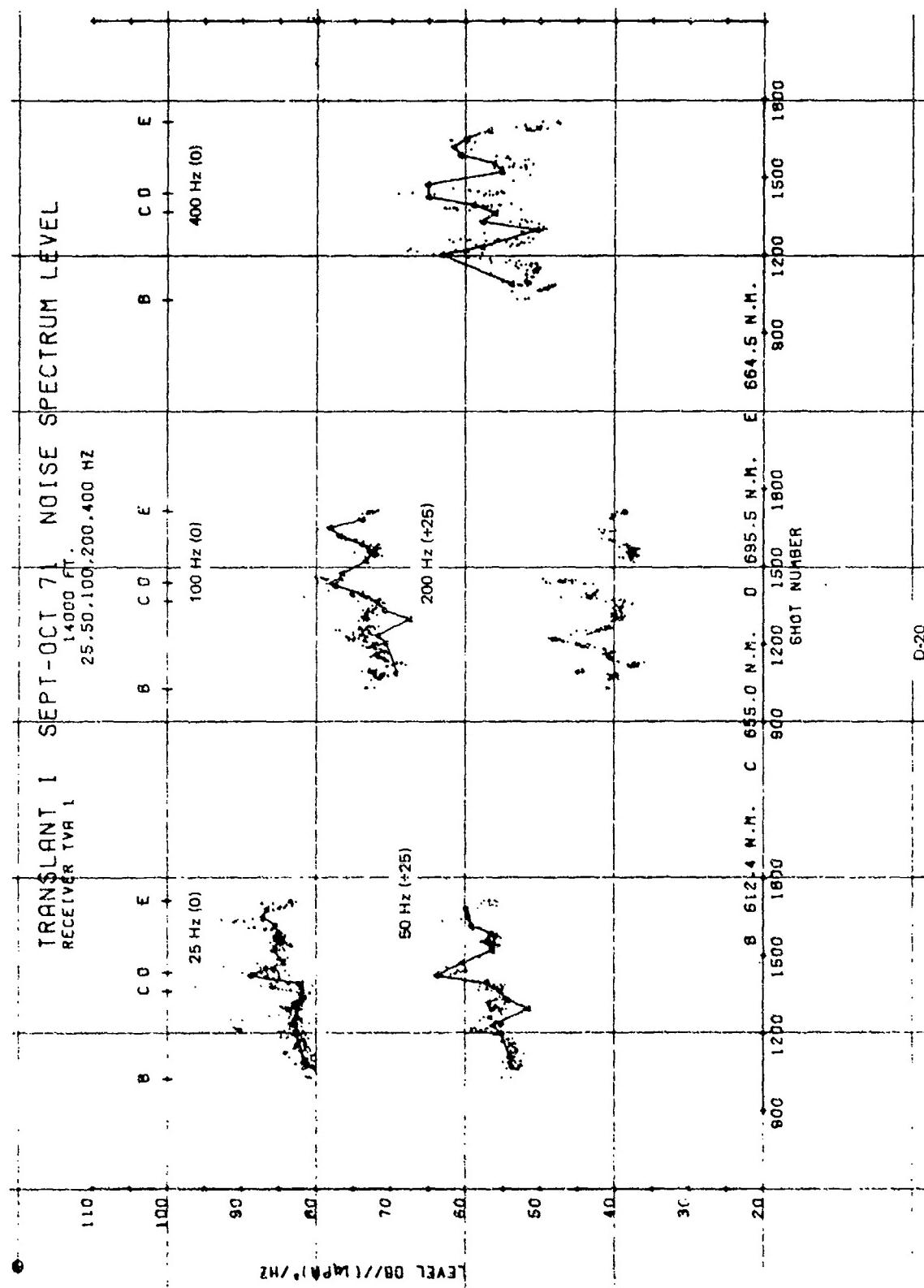
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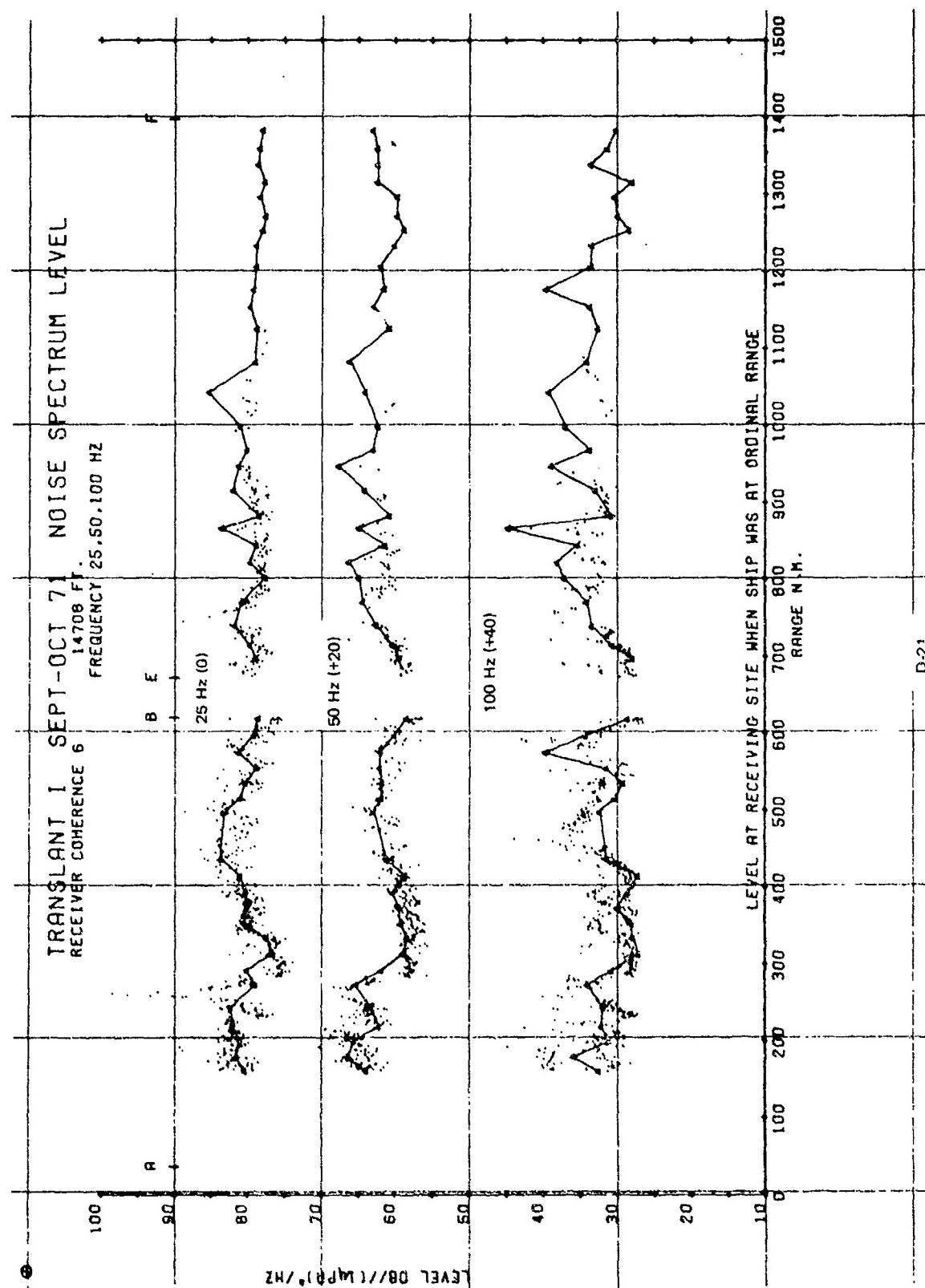
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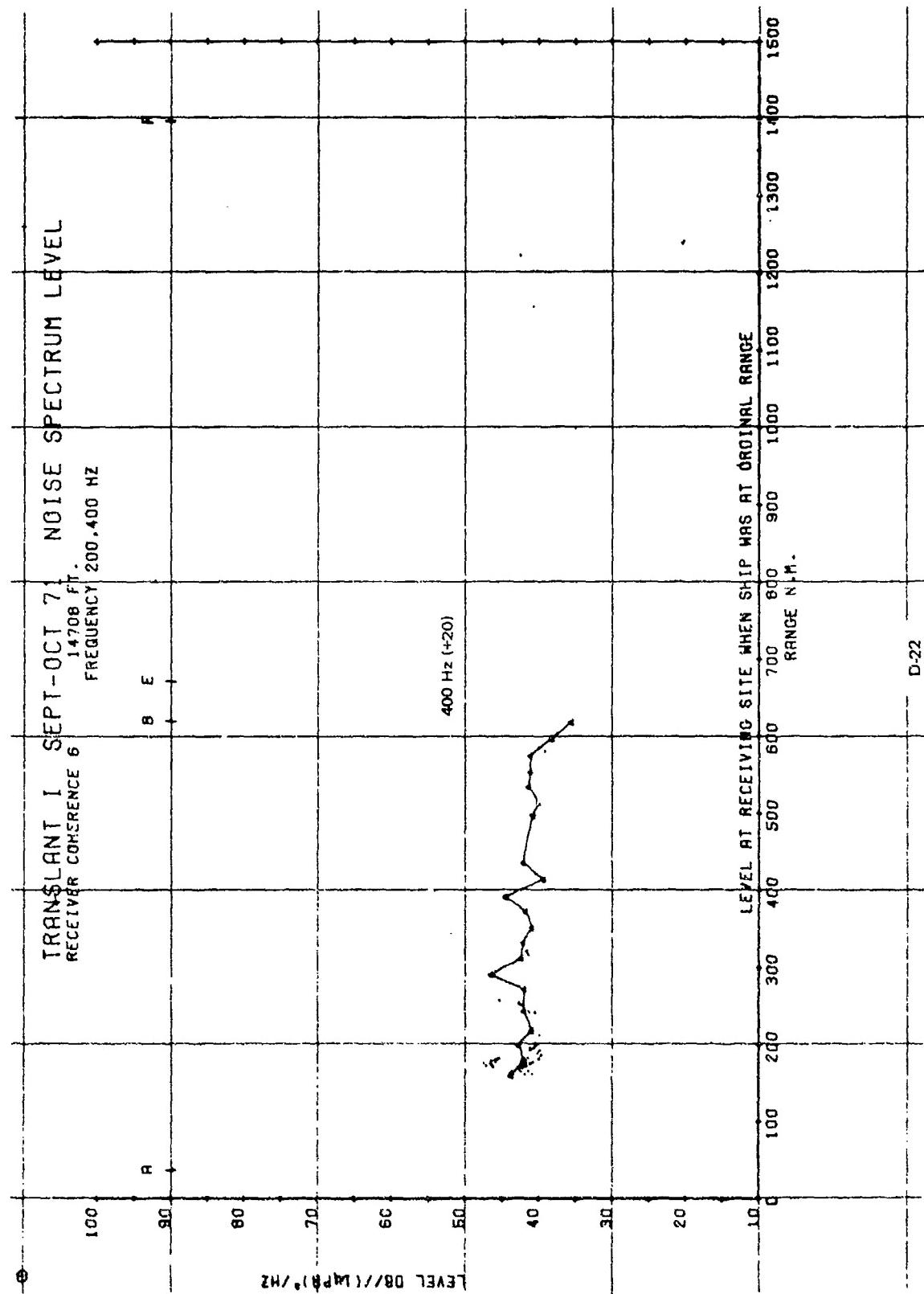
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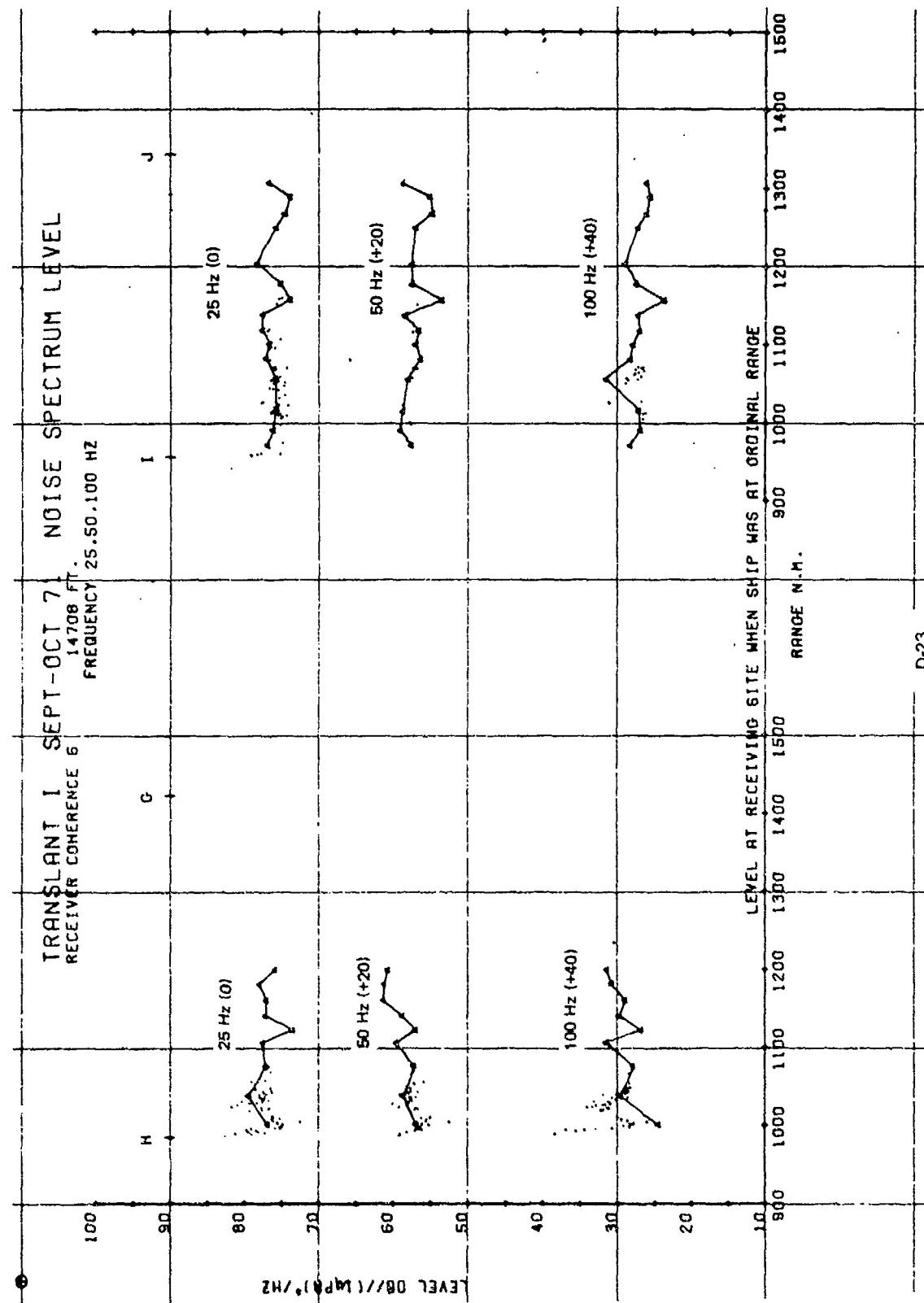
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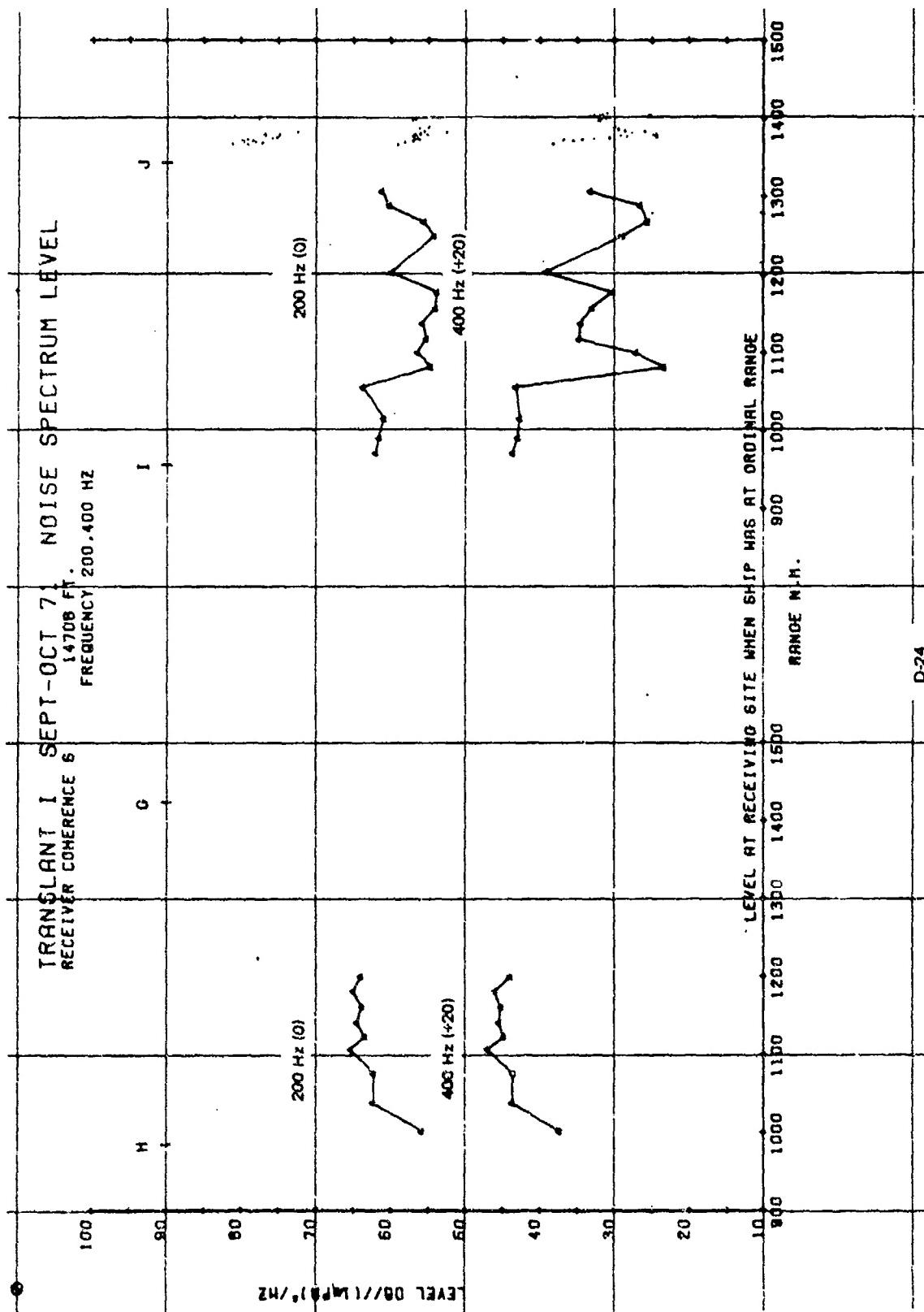


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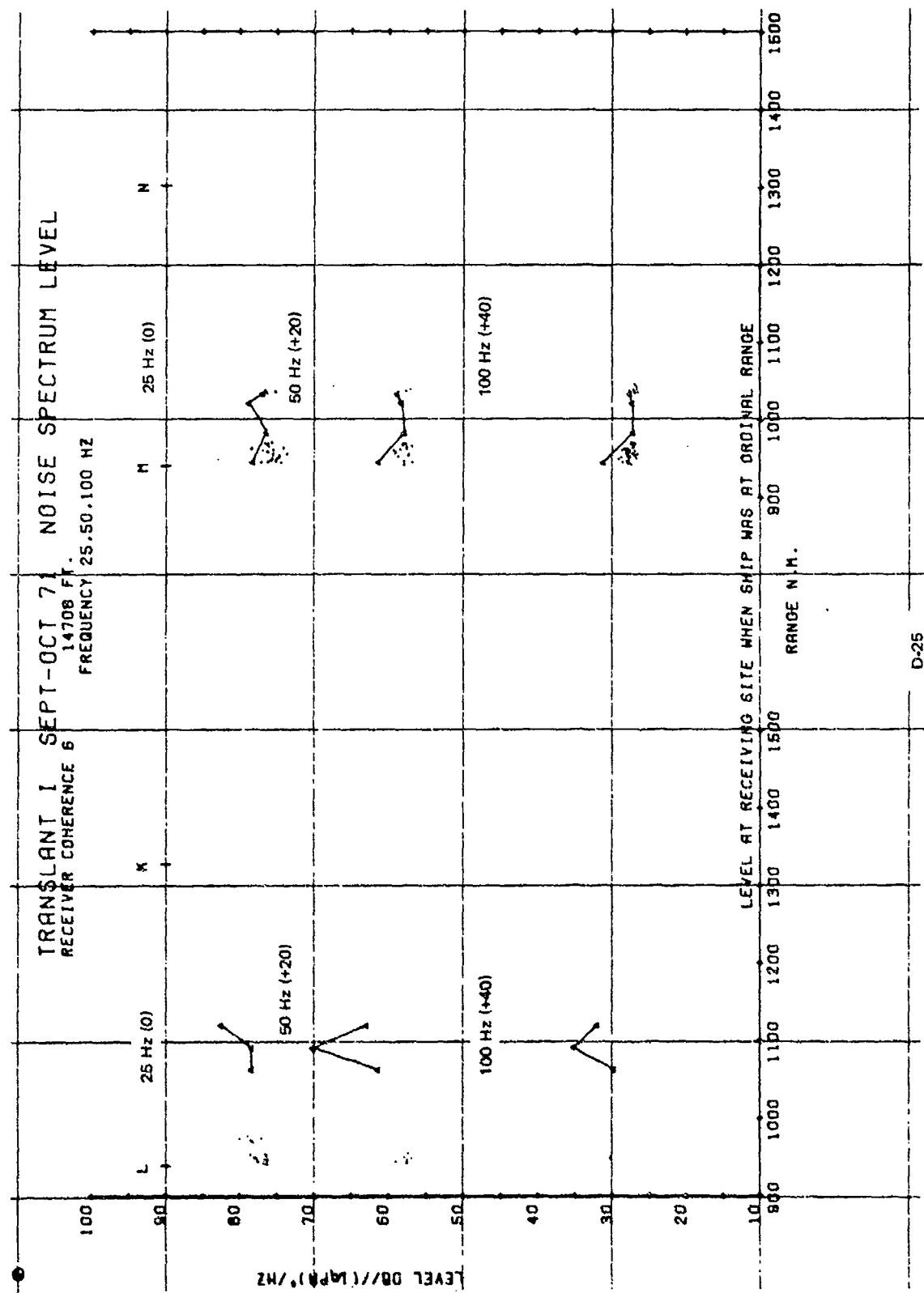


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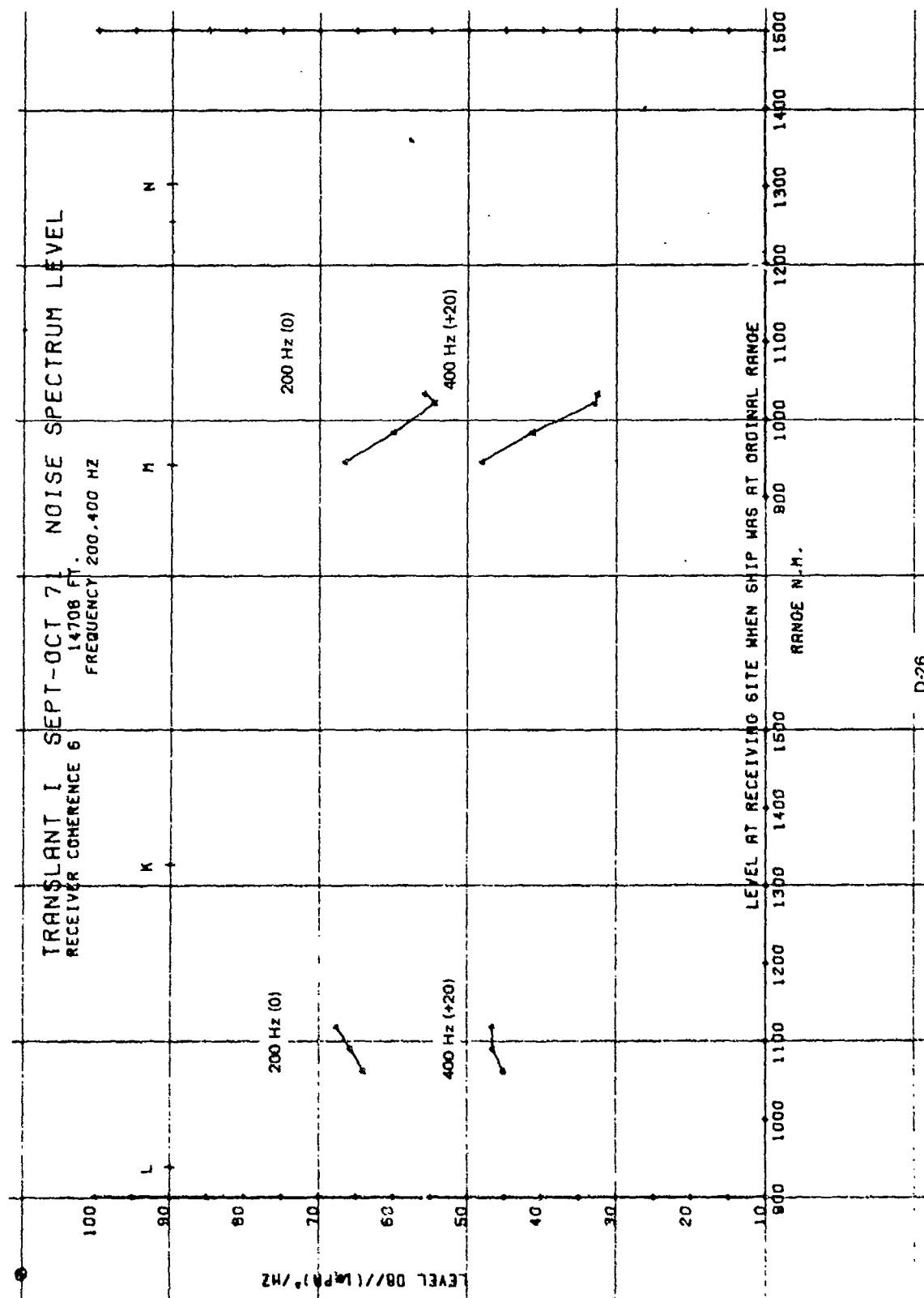


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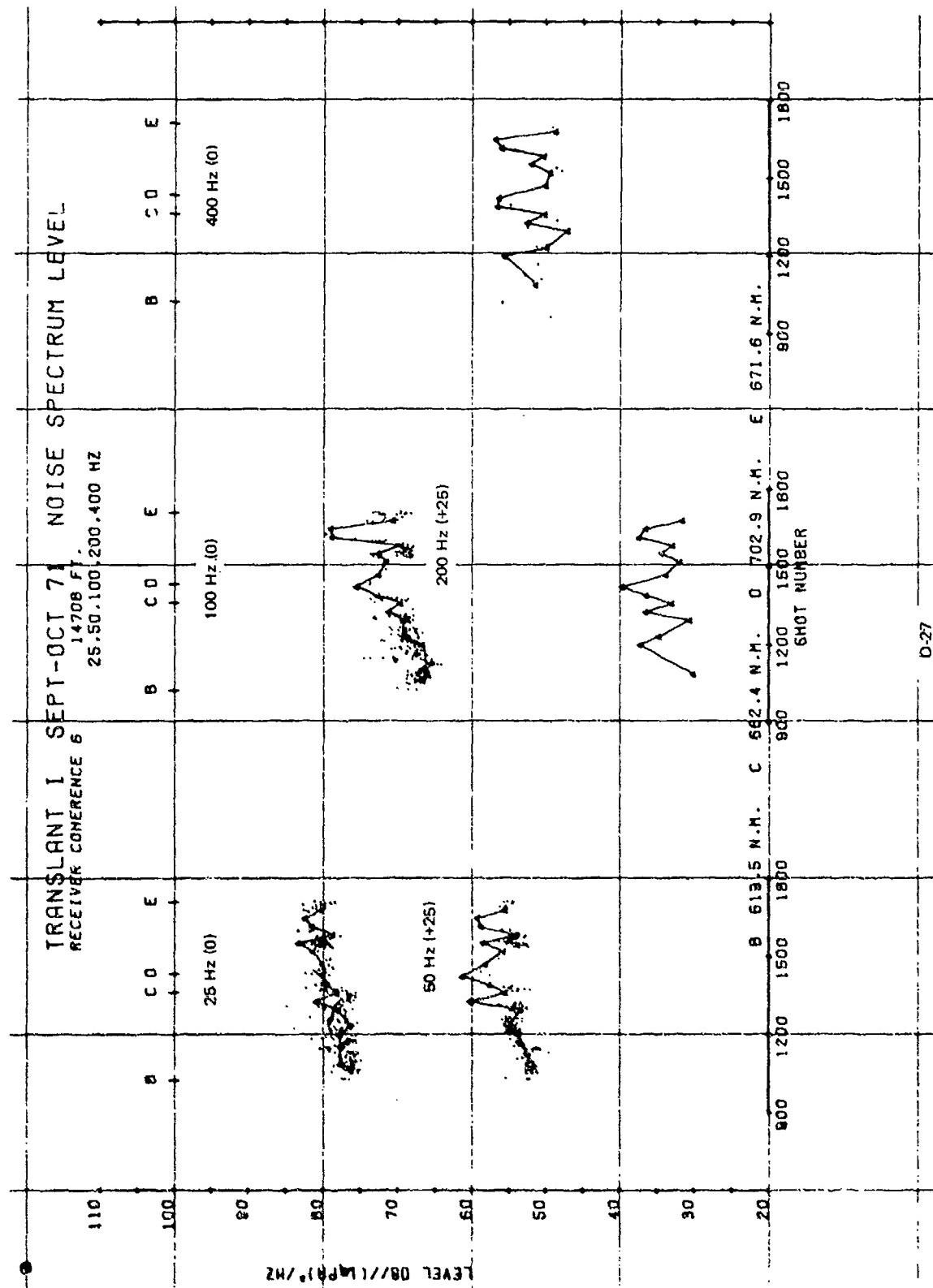


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TR 4635

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D-28

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TR 4635

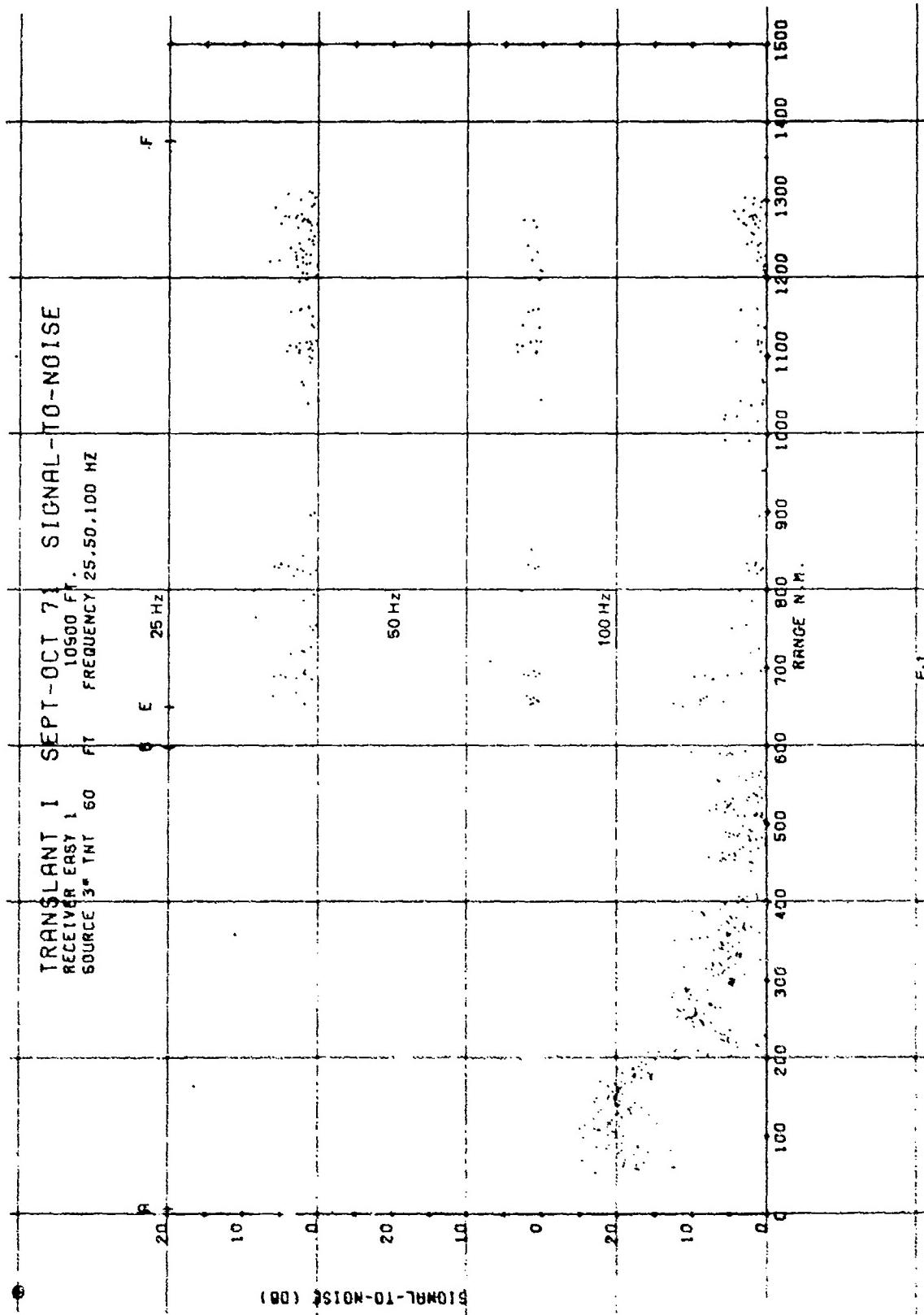
Appendix E
TRANSLANT I SIGNAL-TO-NOISE LEVELS

The signal-to-noise ratios for the TRANSLANT I measurements are shown on the following pages.

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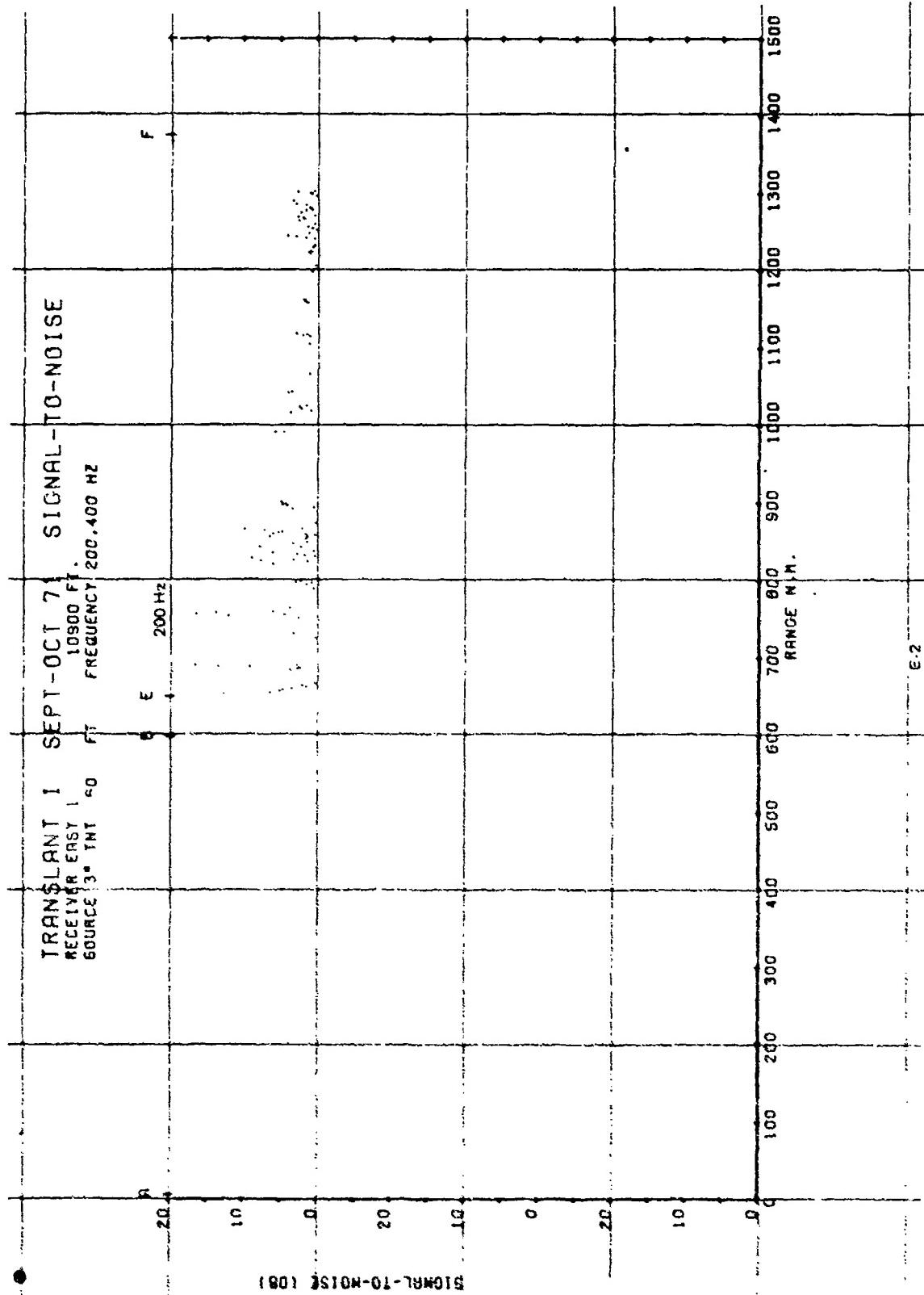
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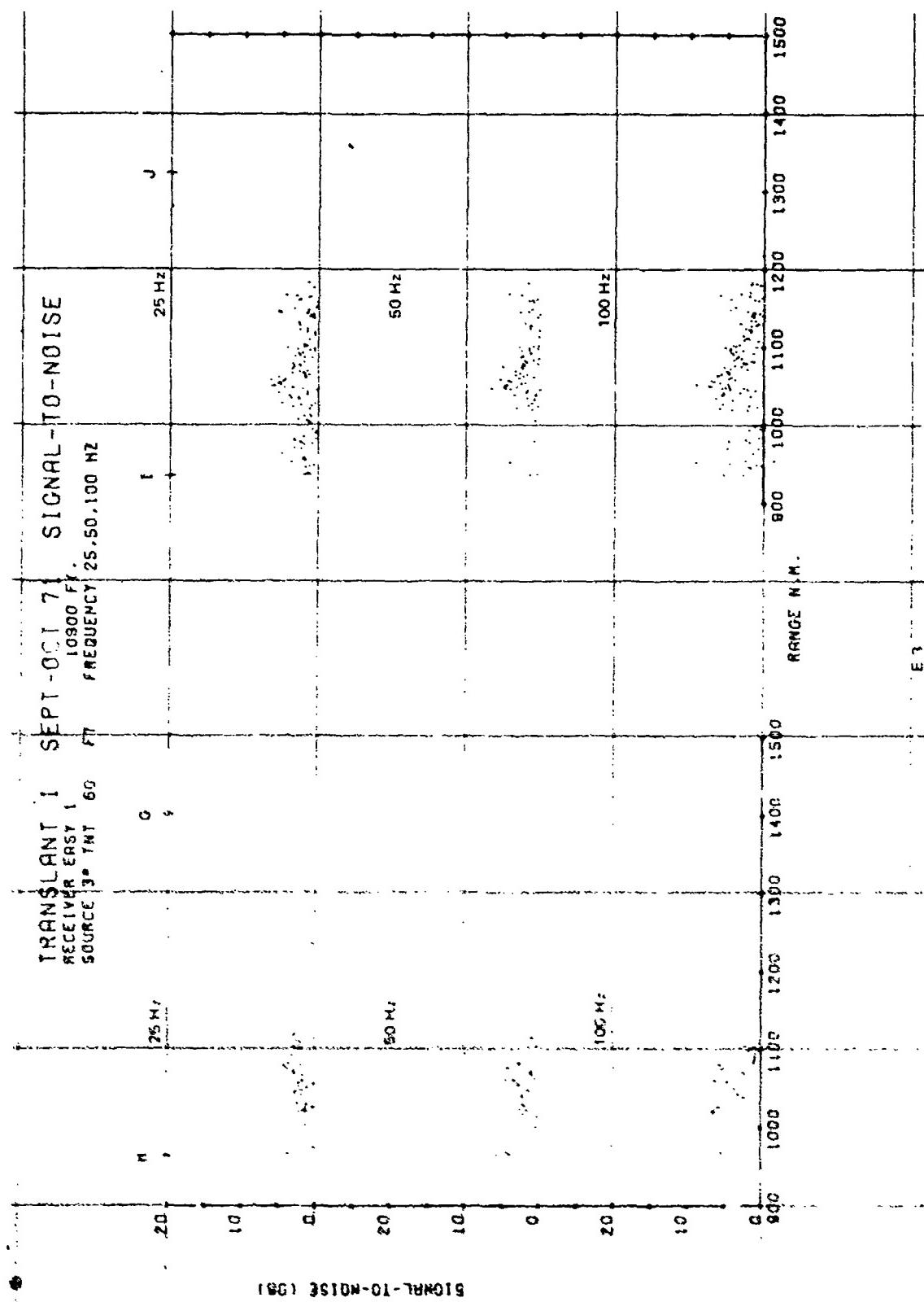
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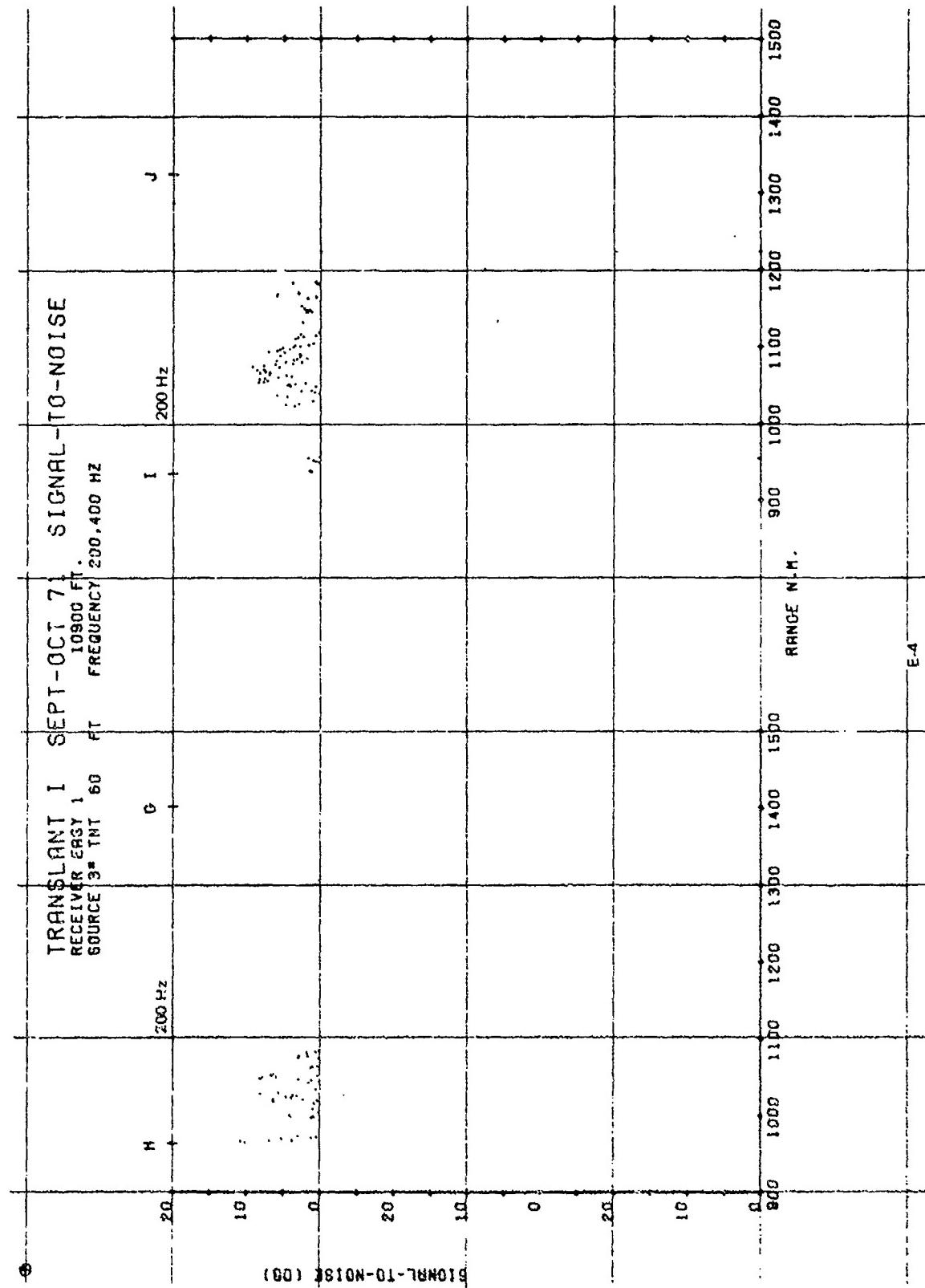
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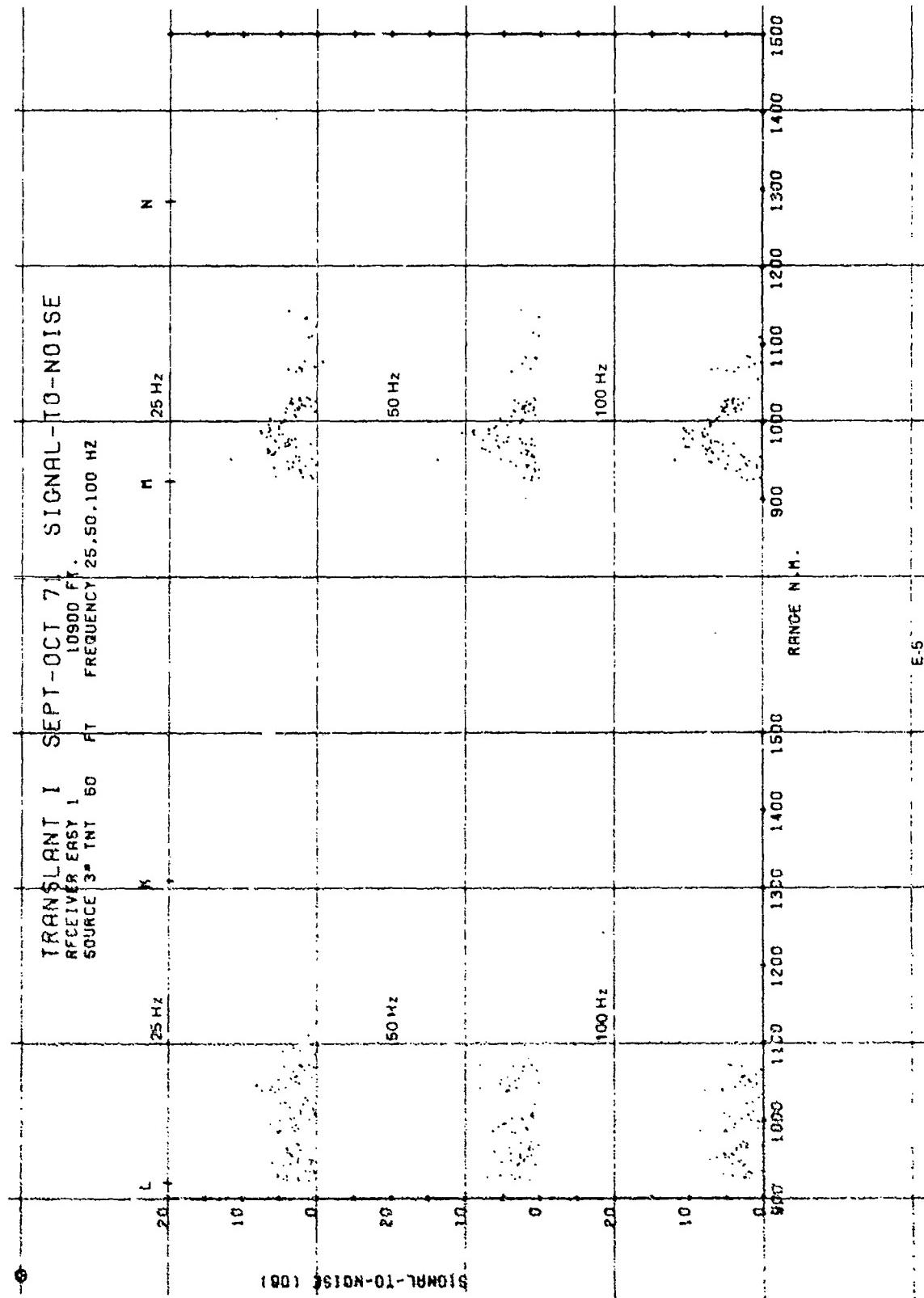
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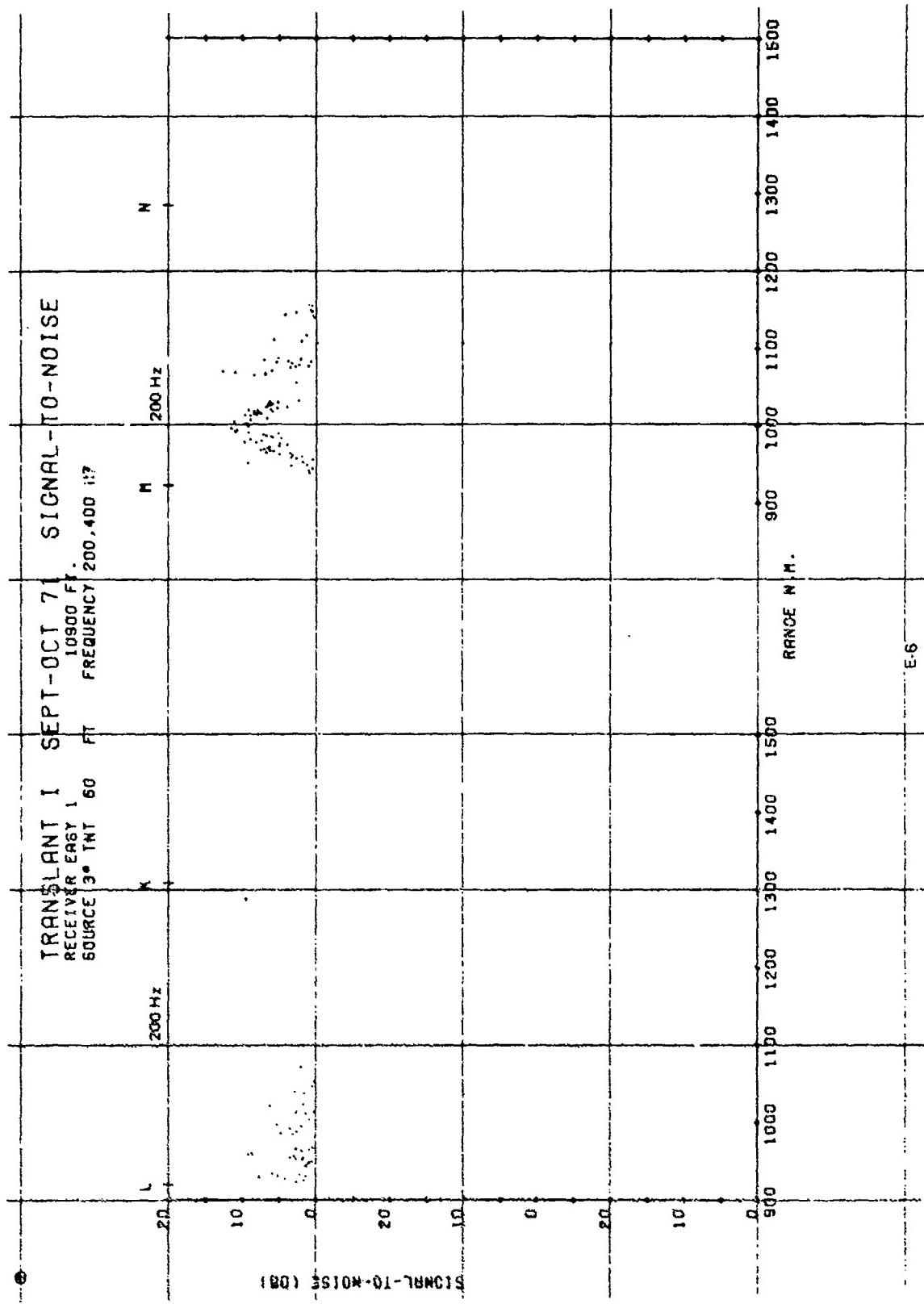
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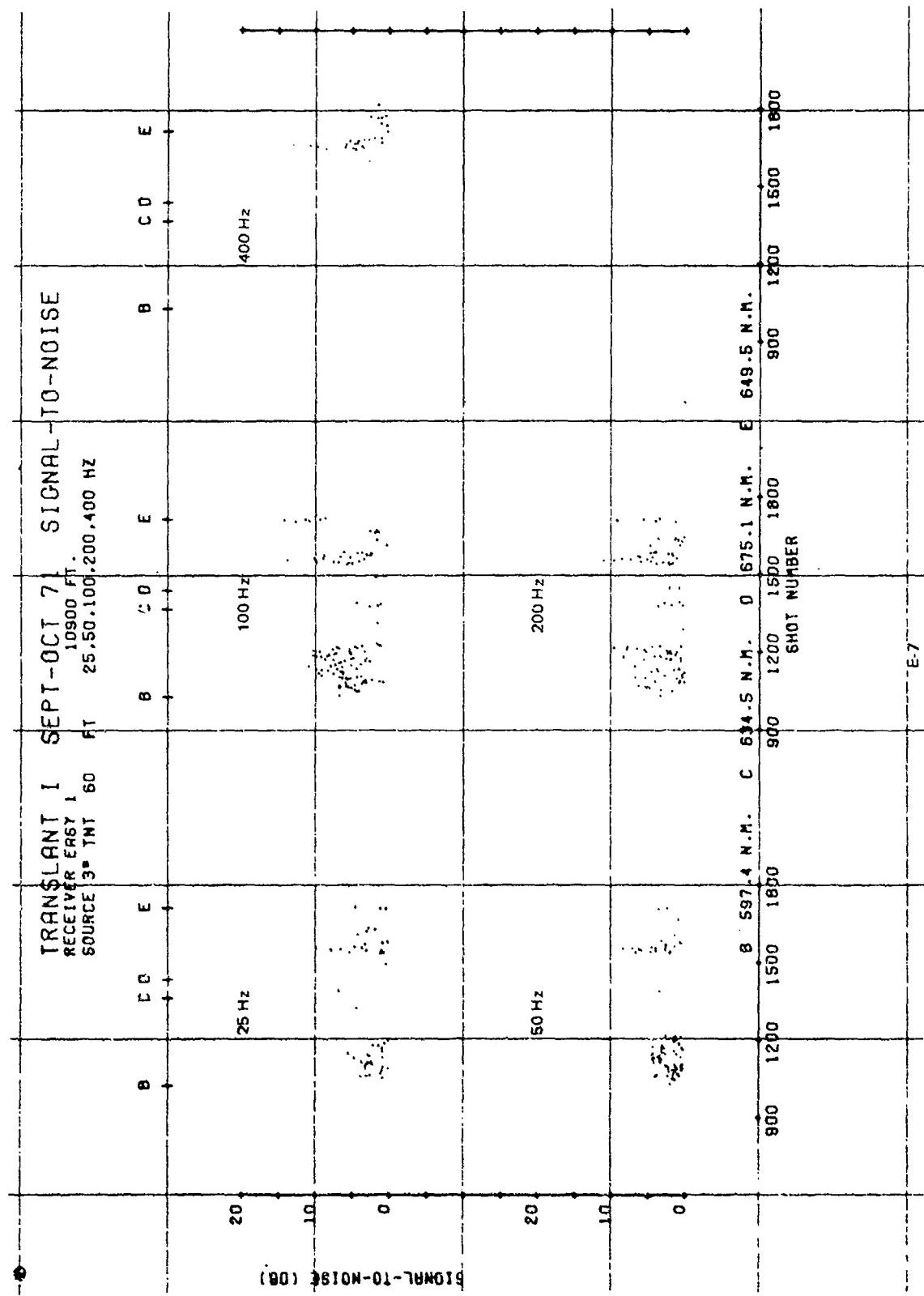
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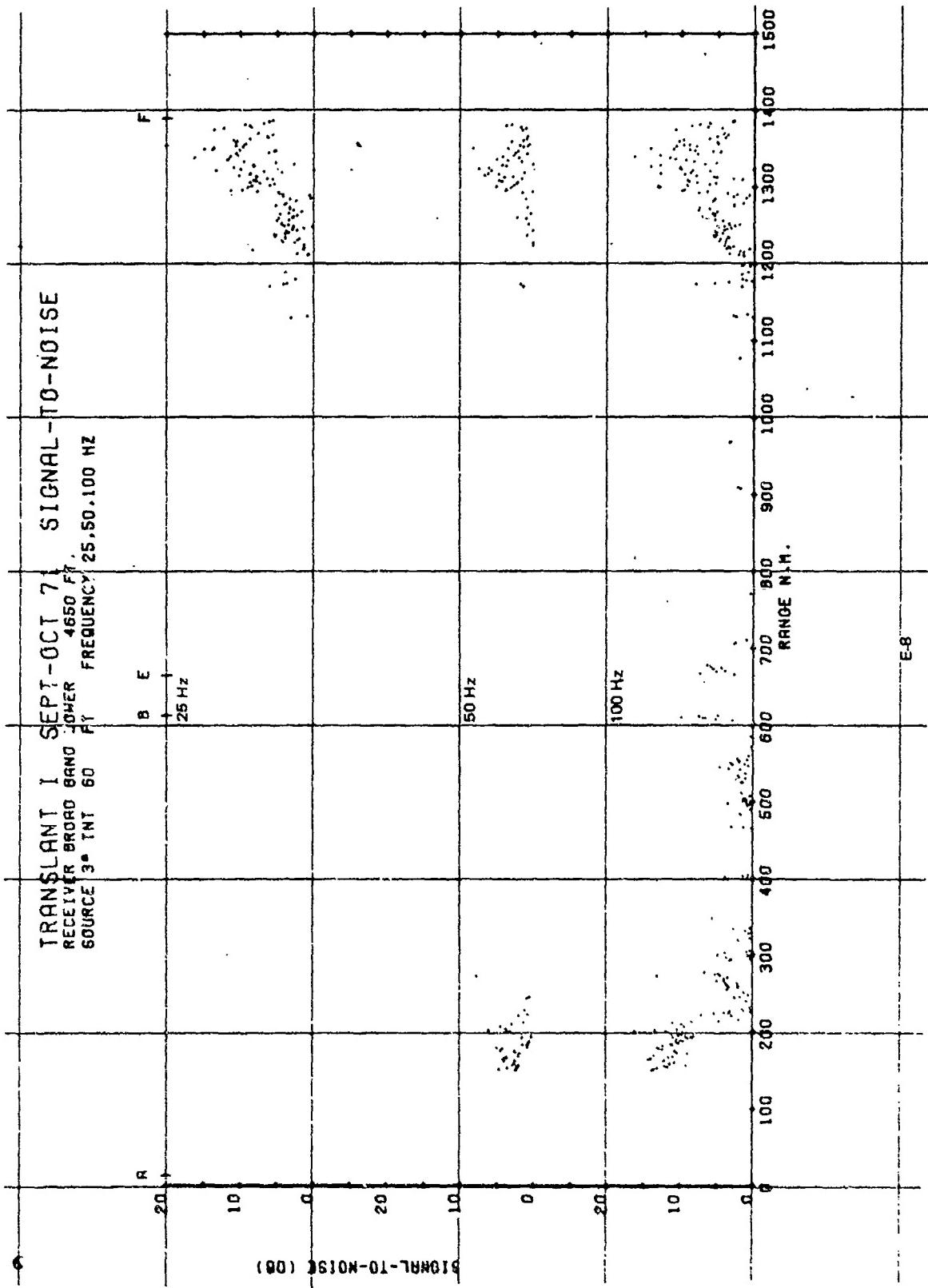
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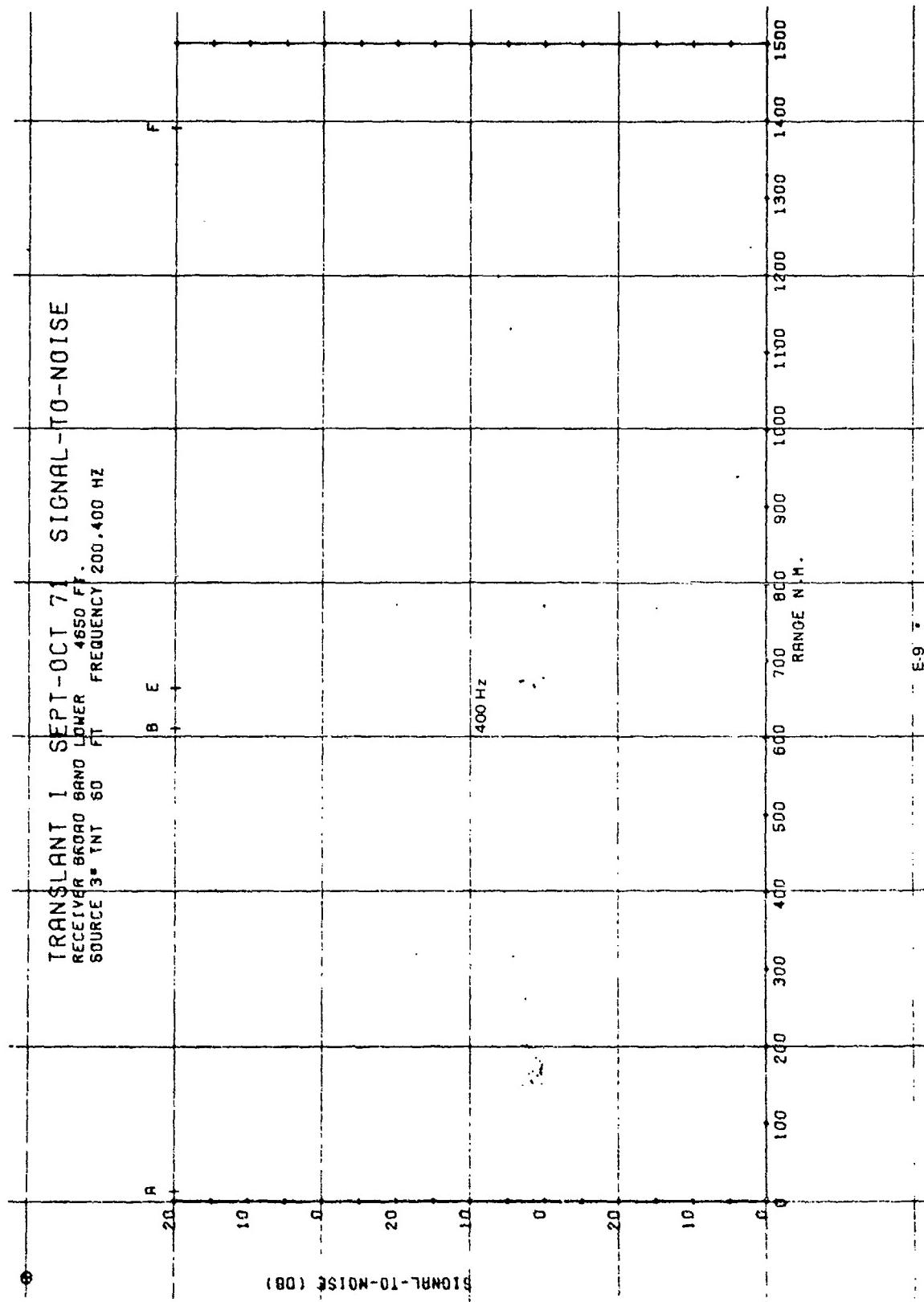
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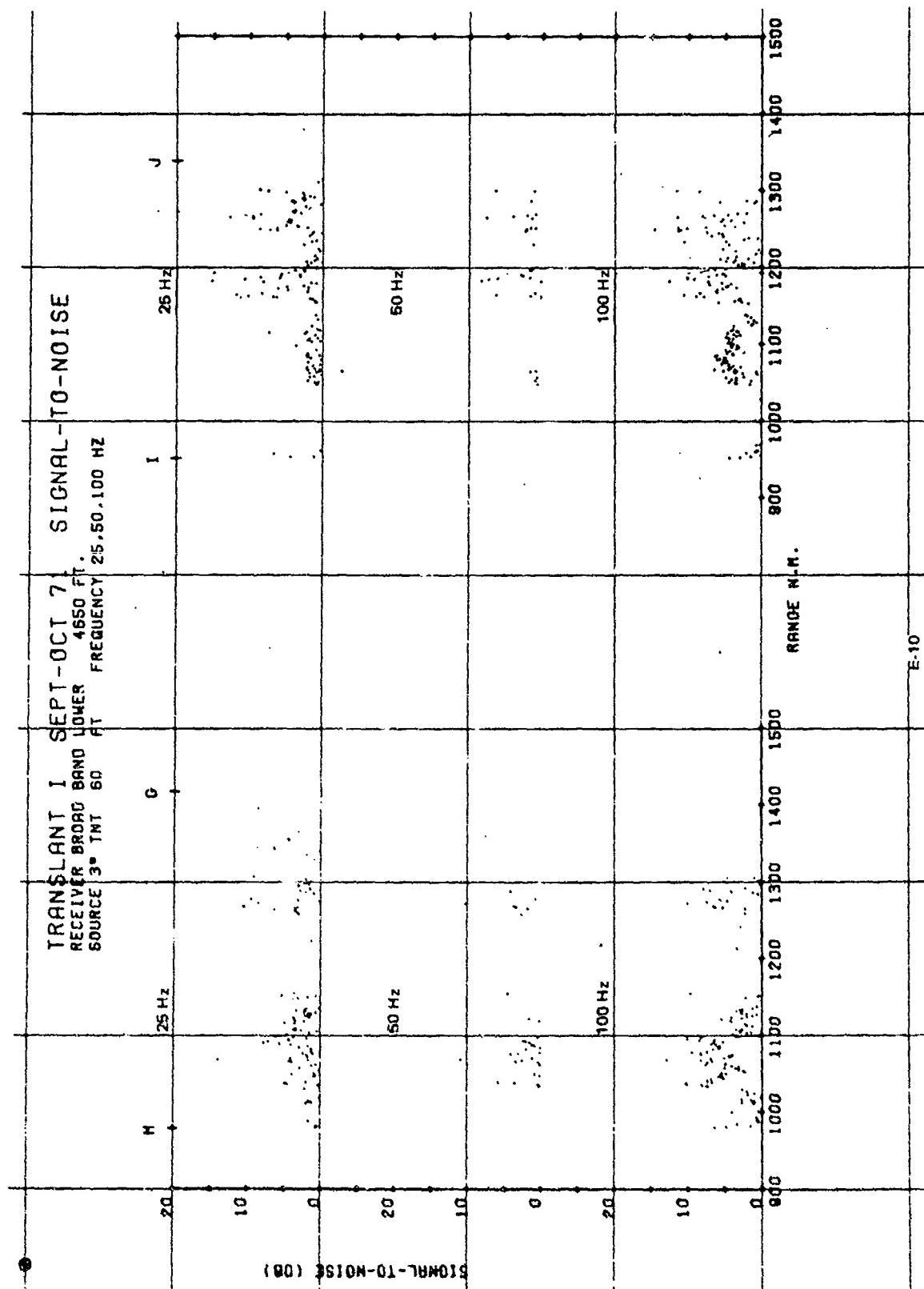
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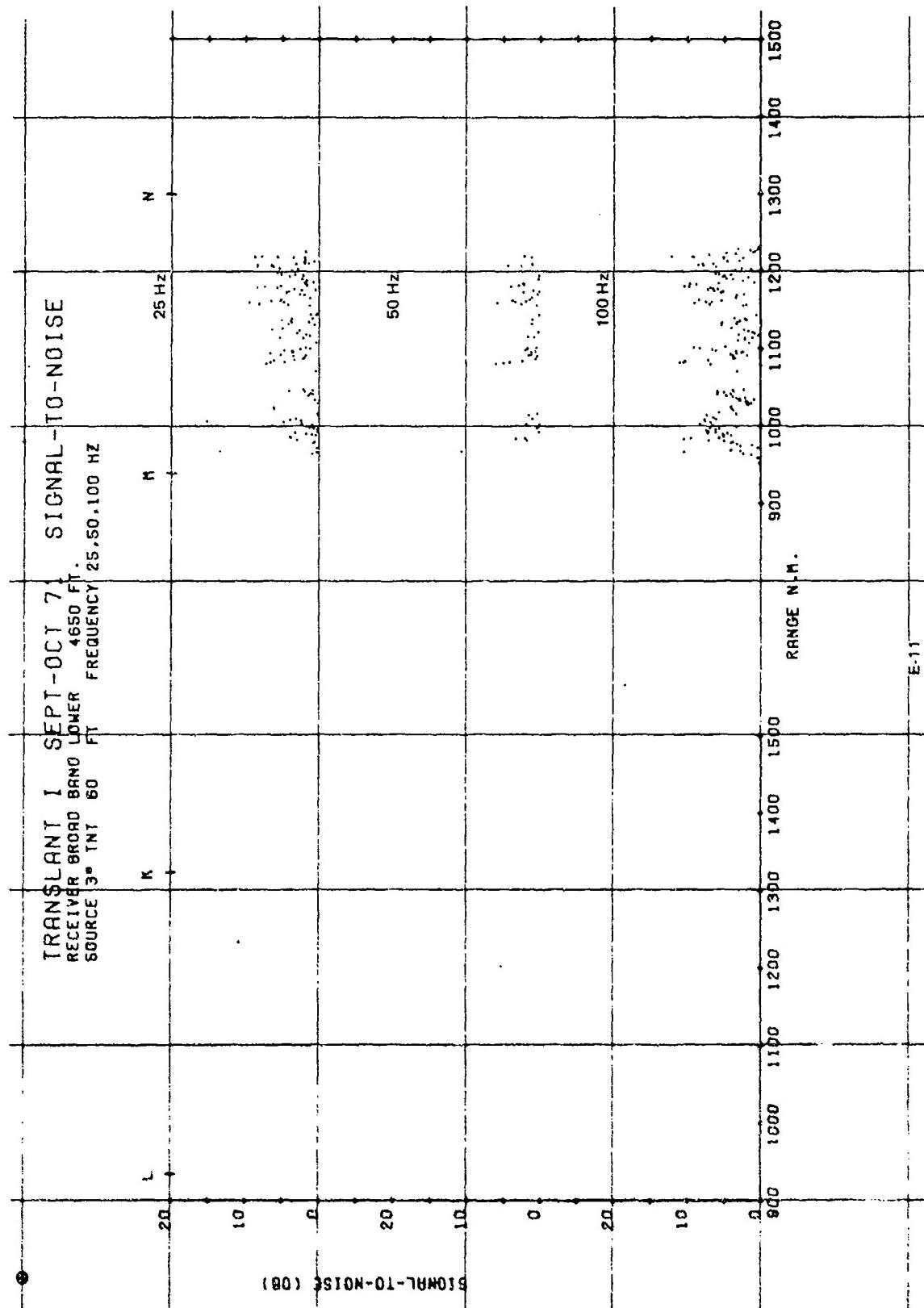
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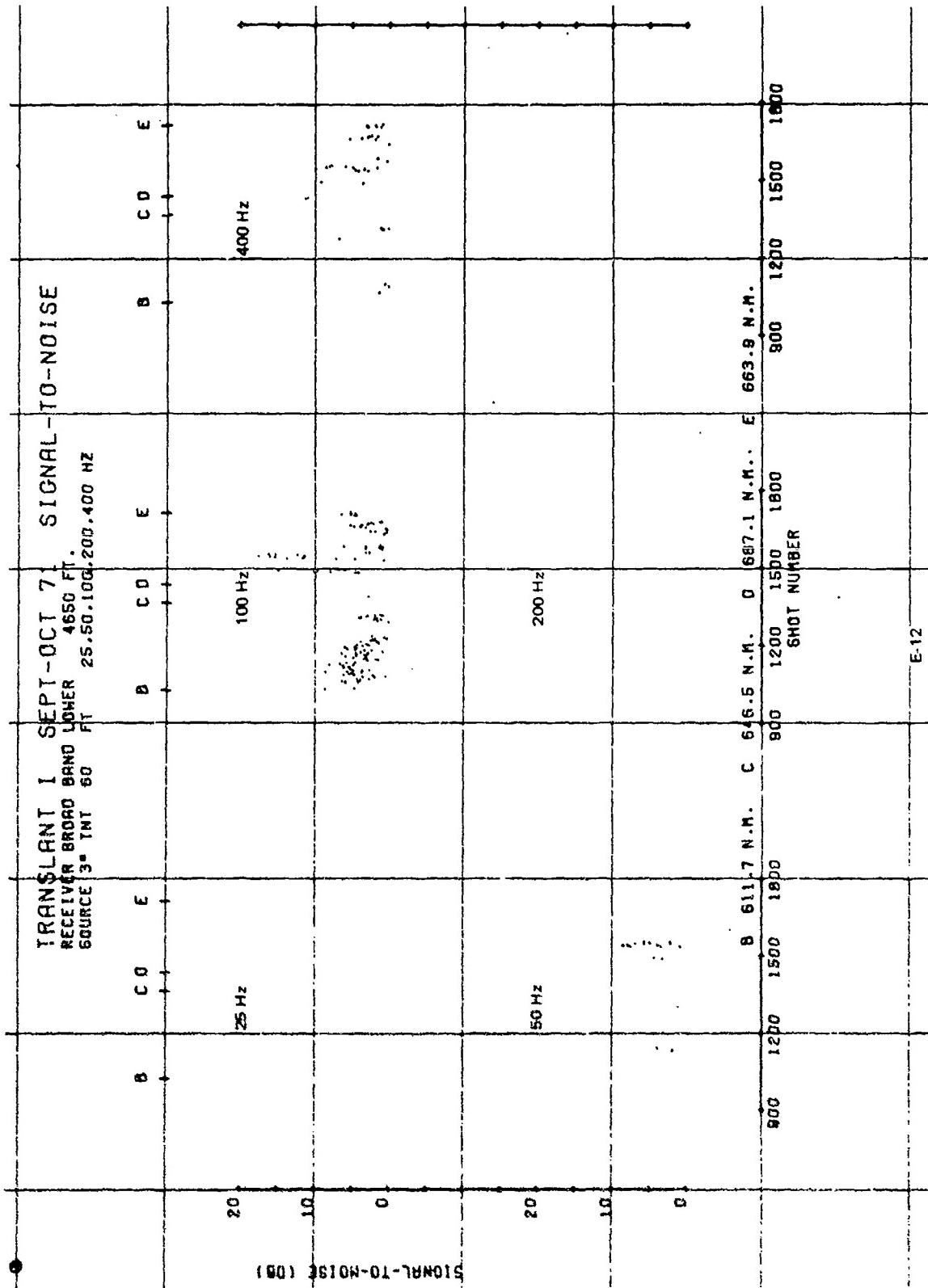
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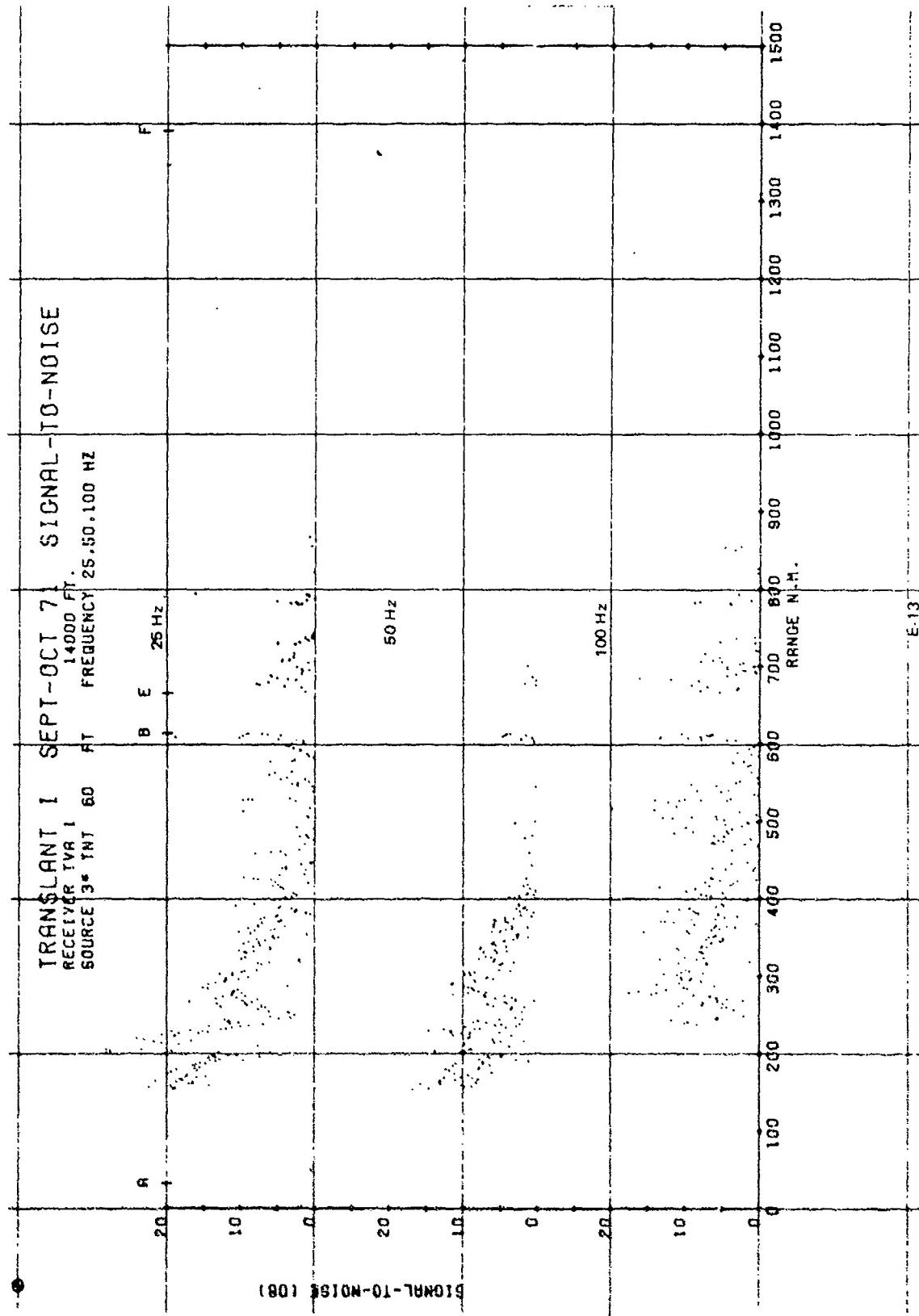
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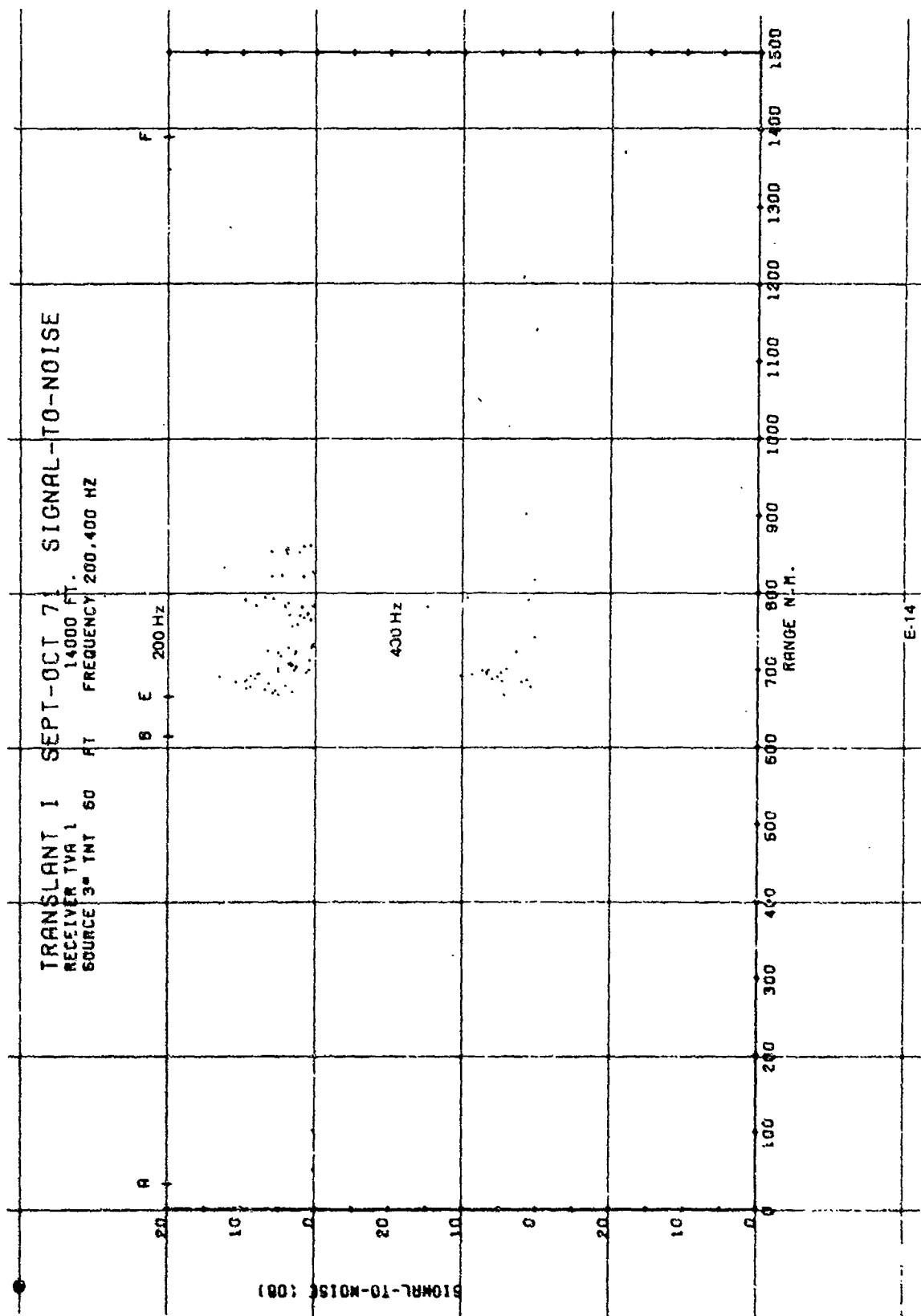
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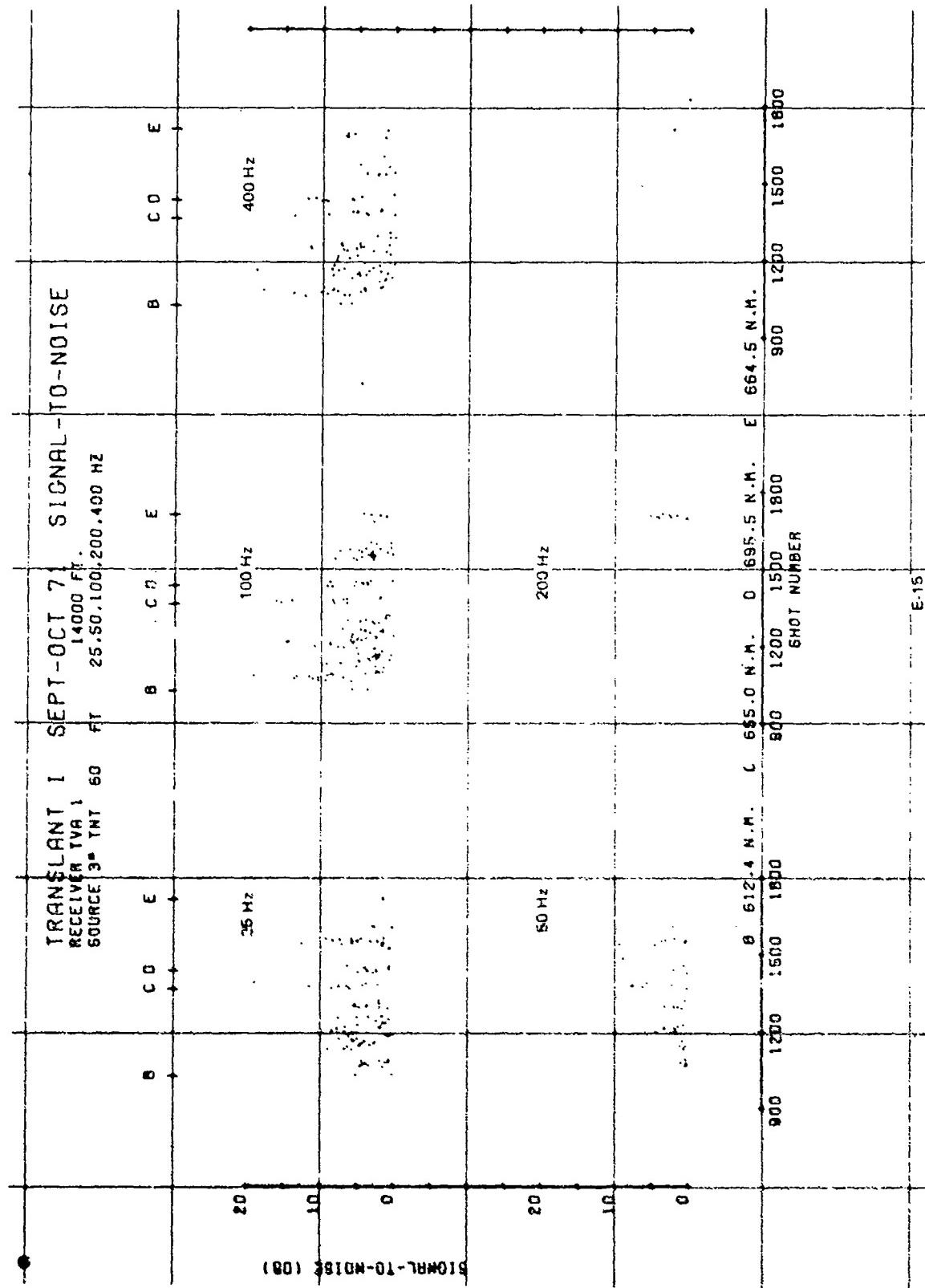
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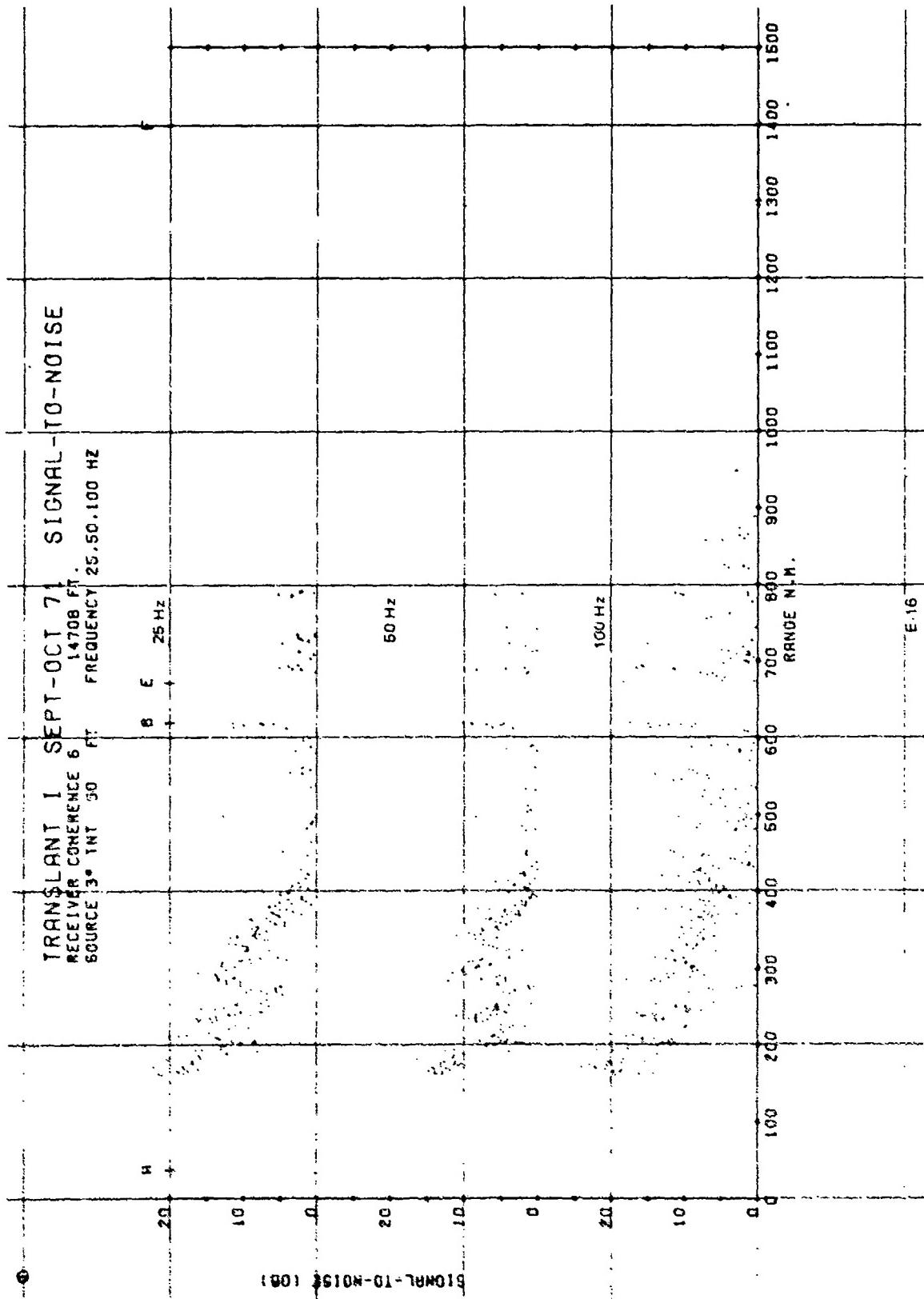
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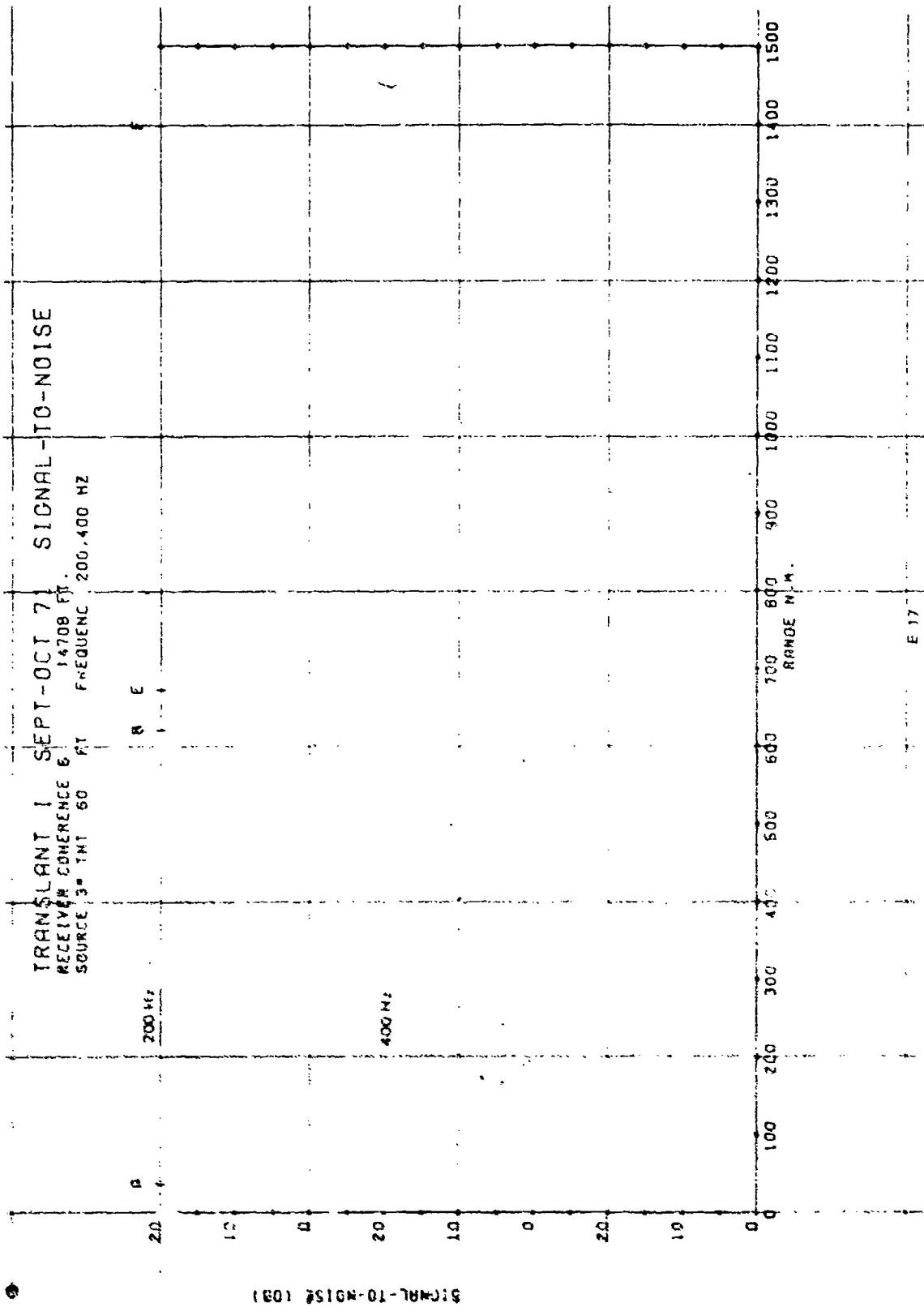


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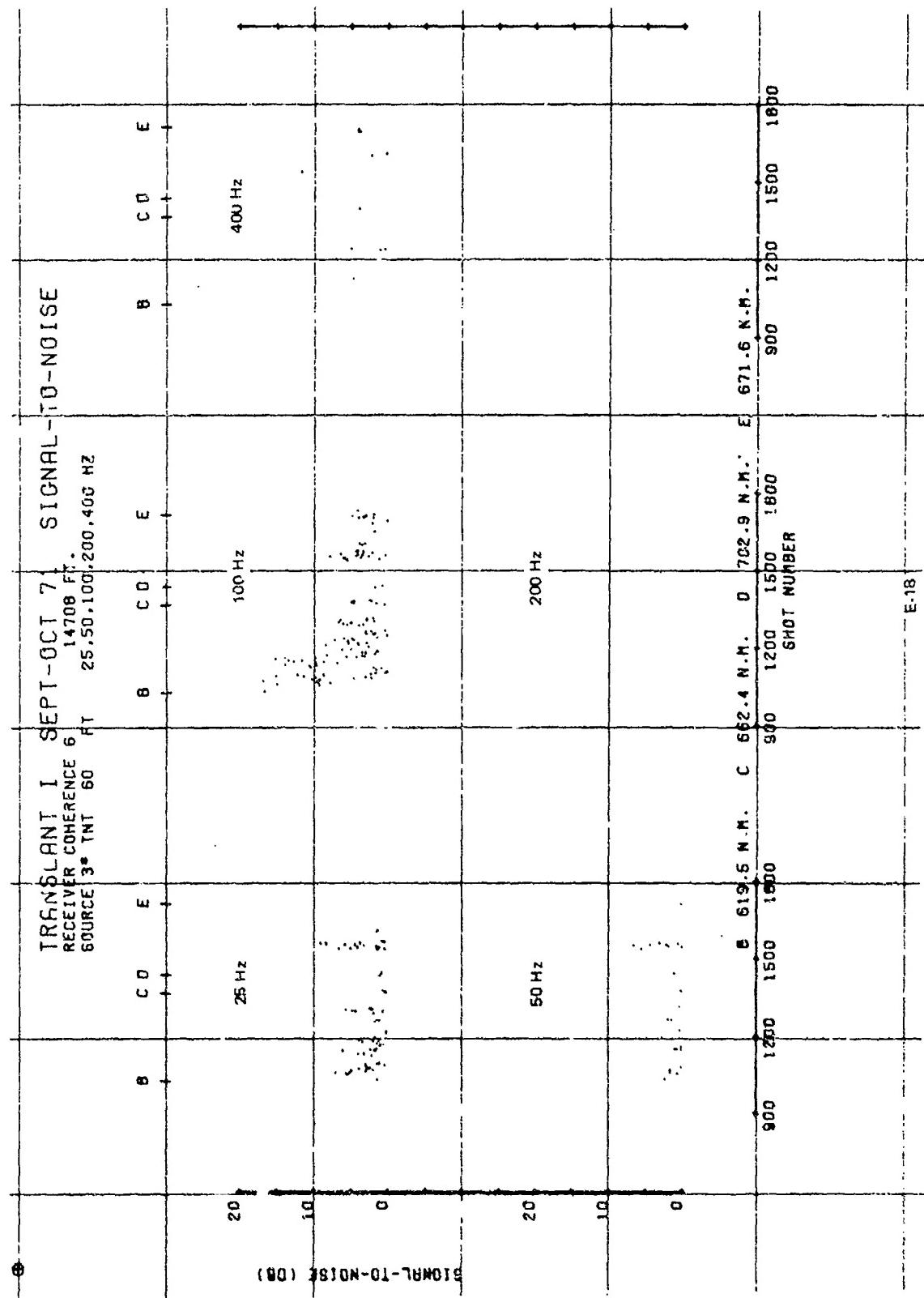
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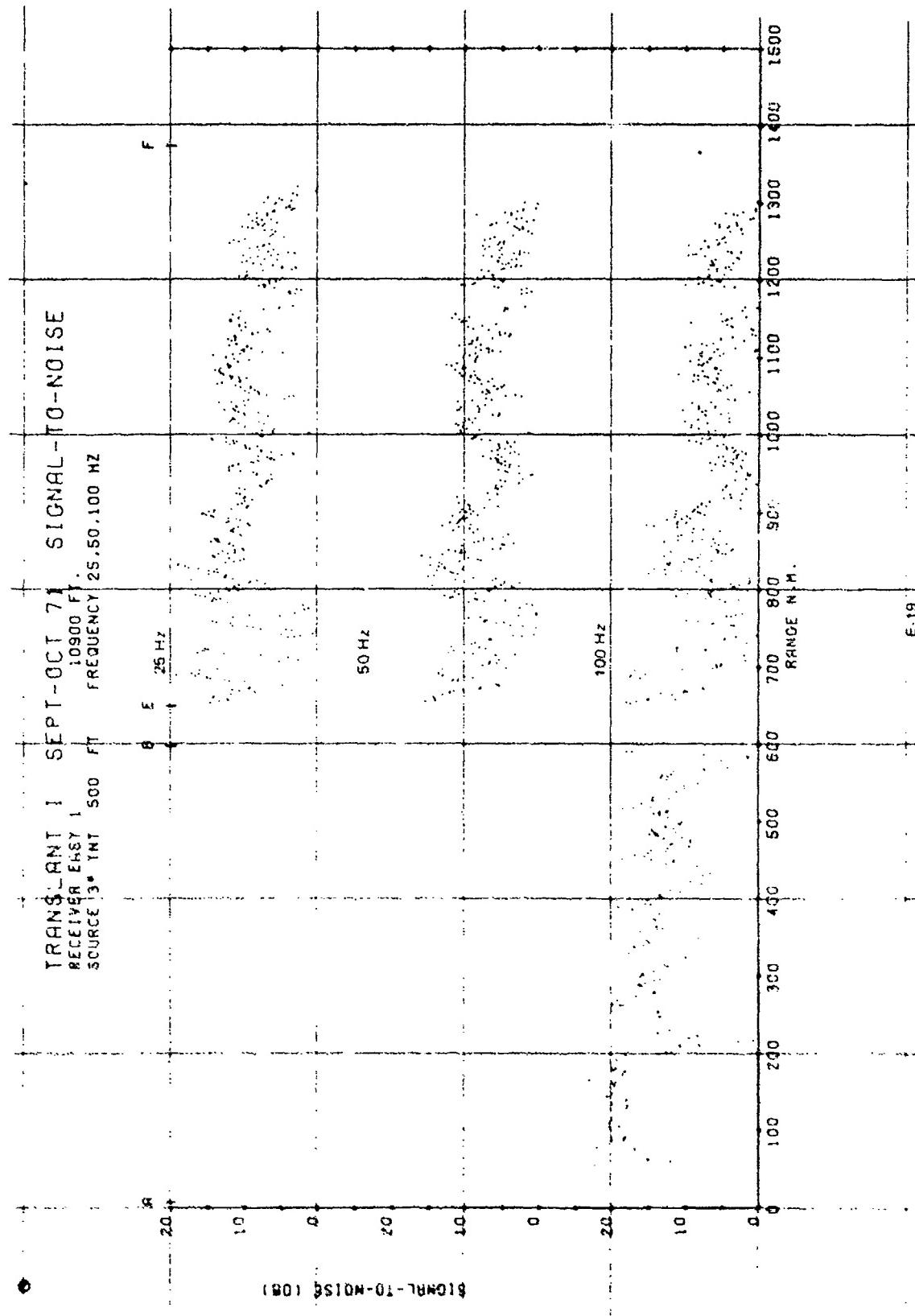
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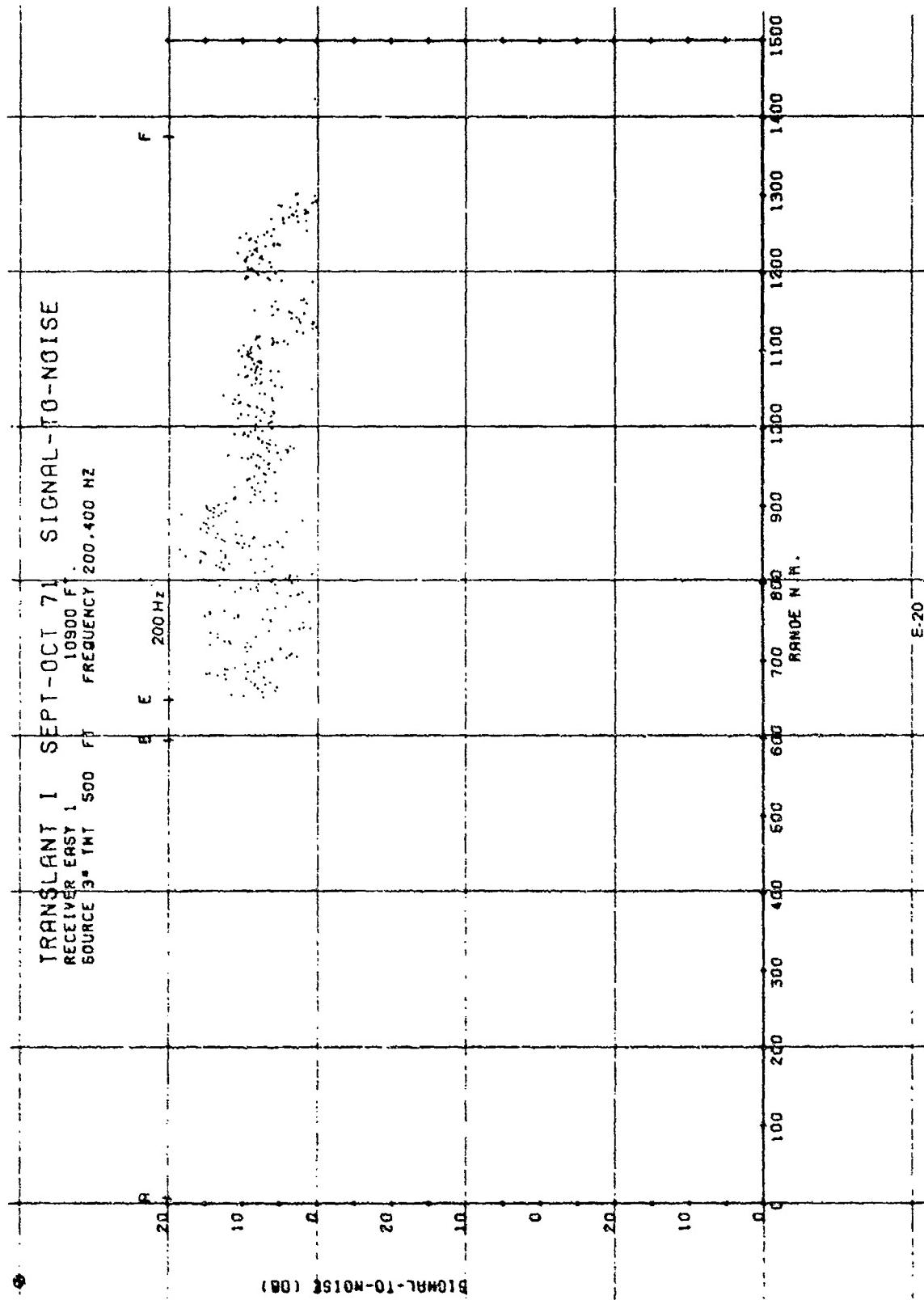
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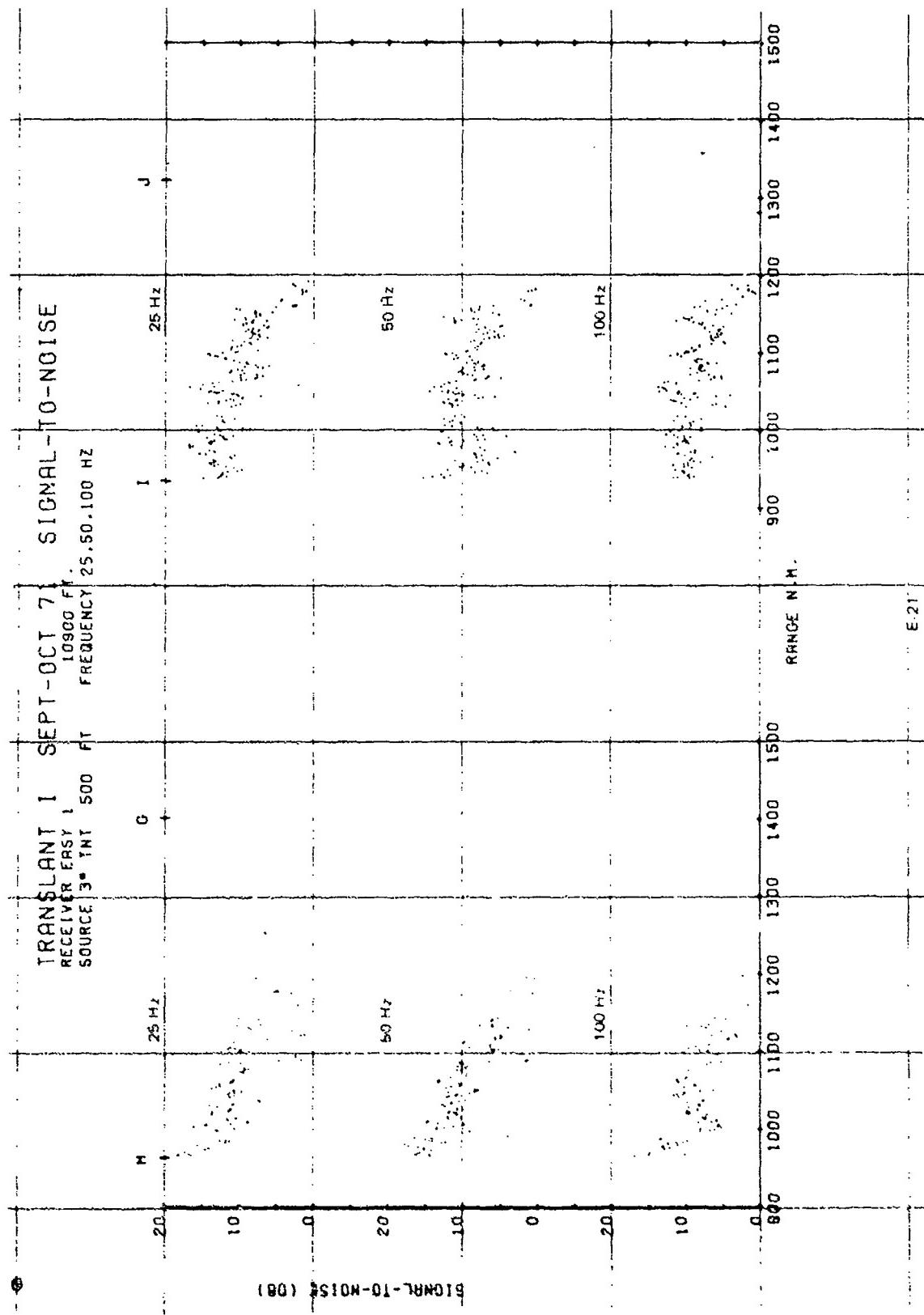
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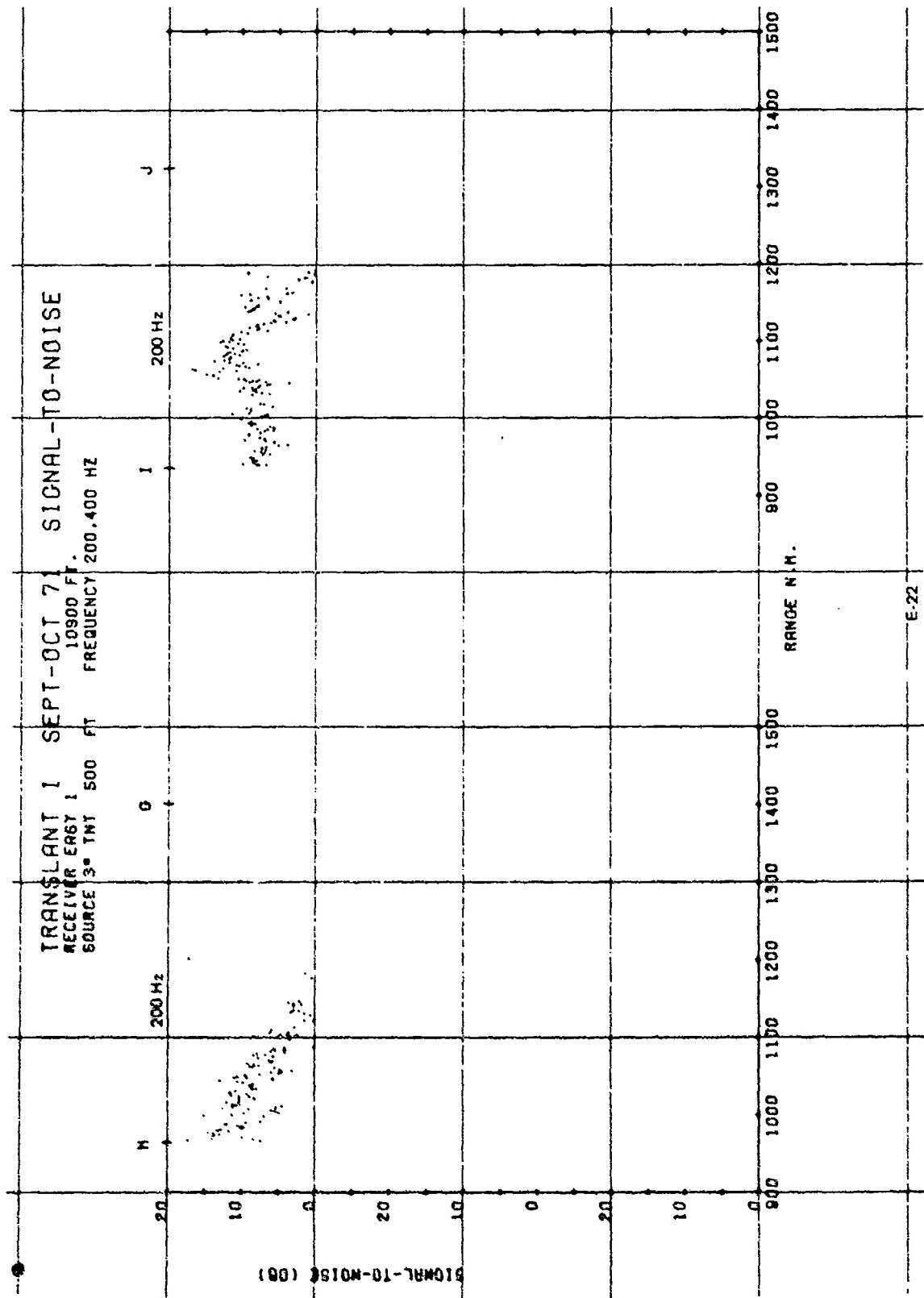
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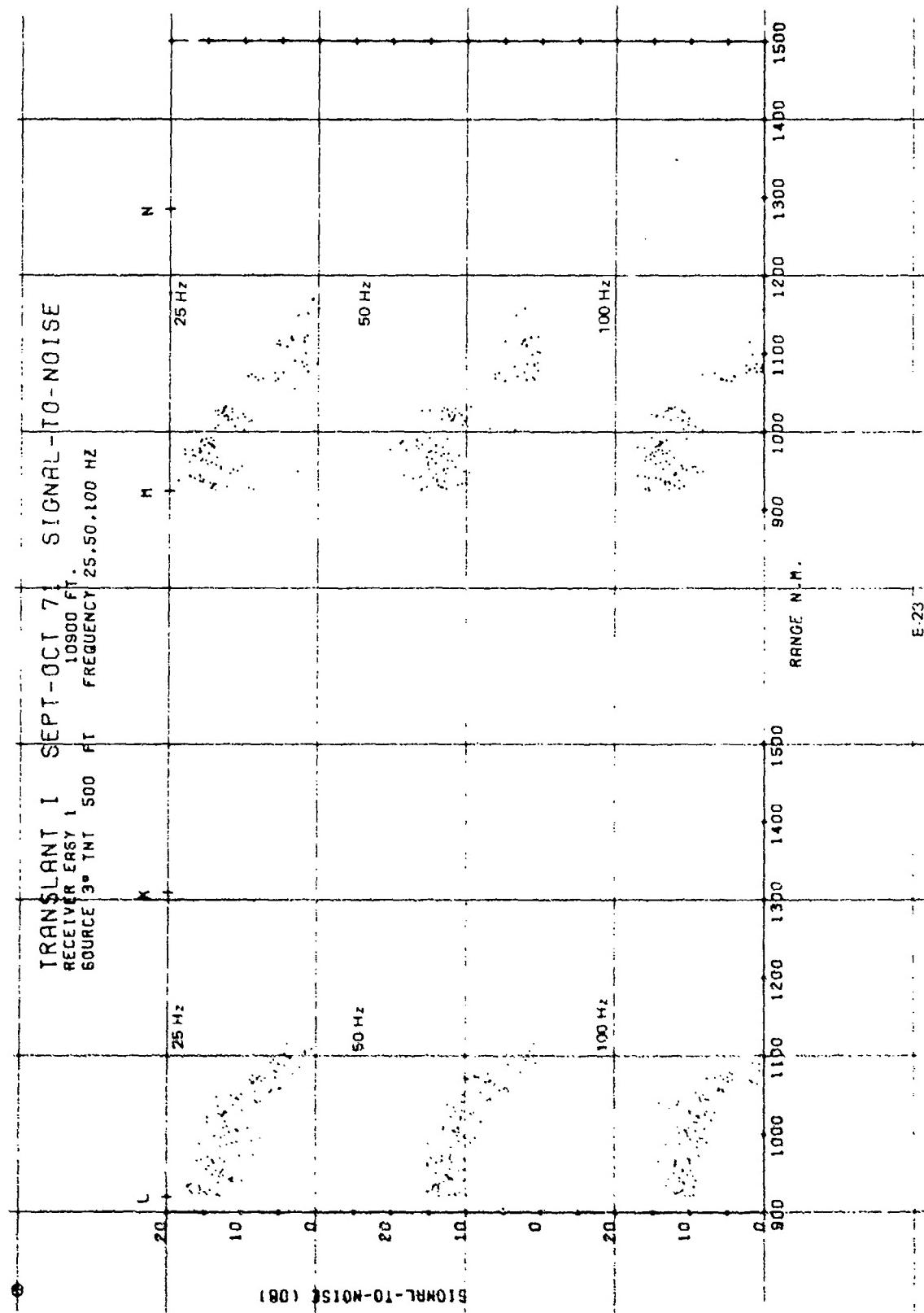
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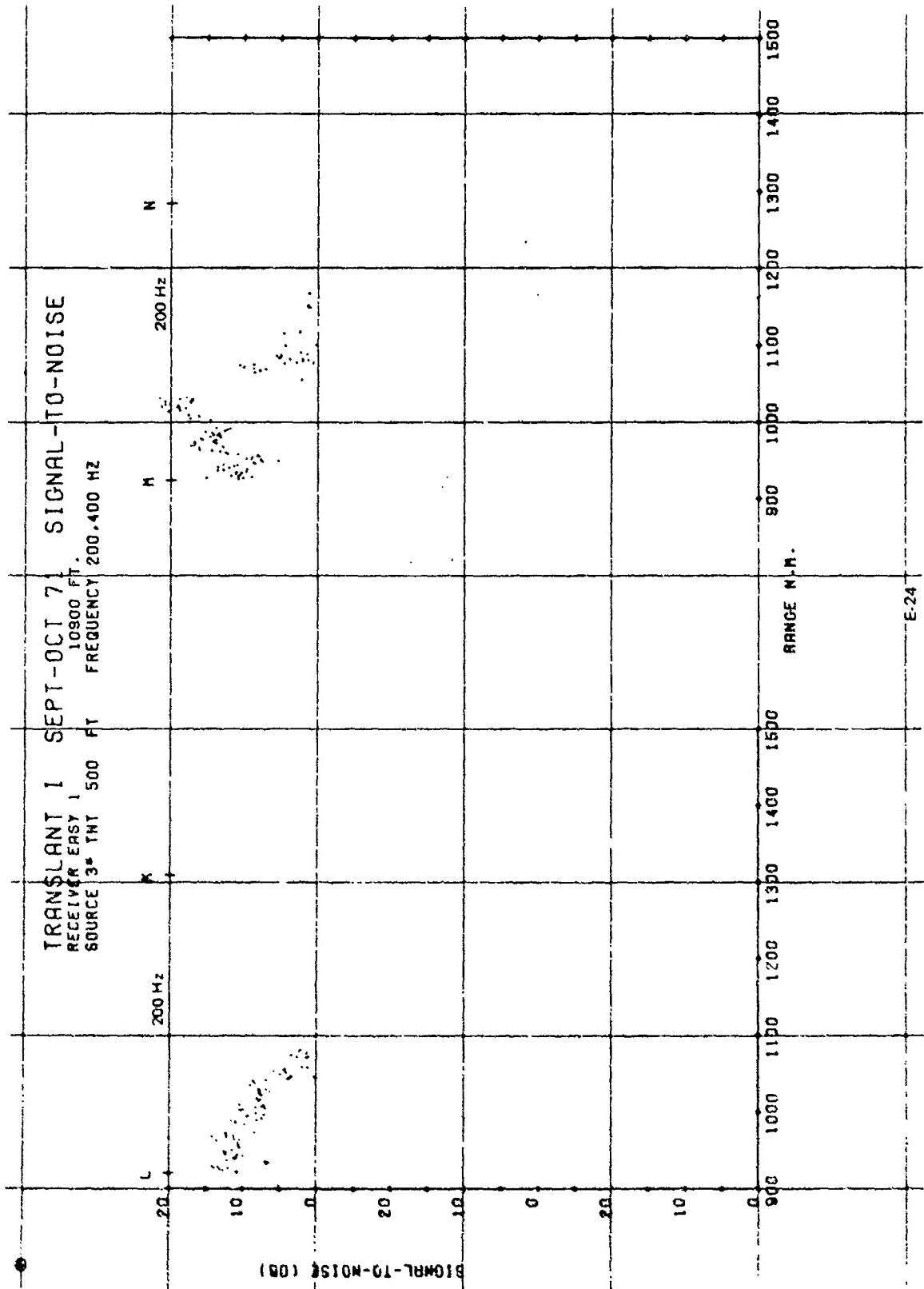


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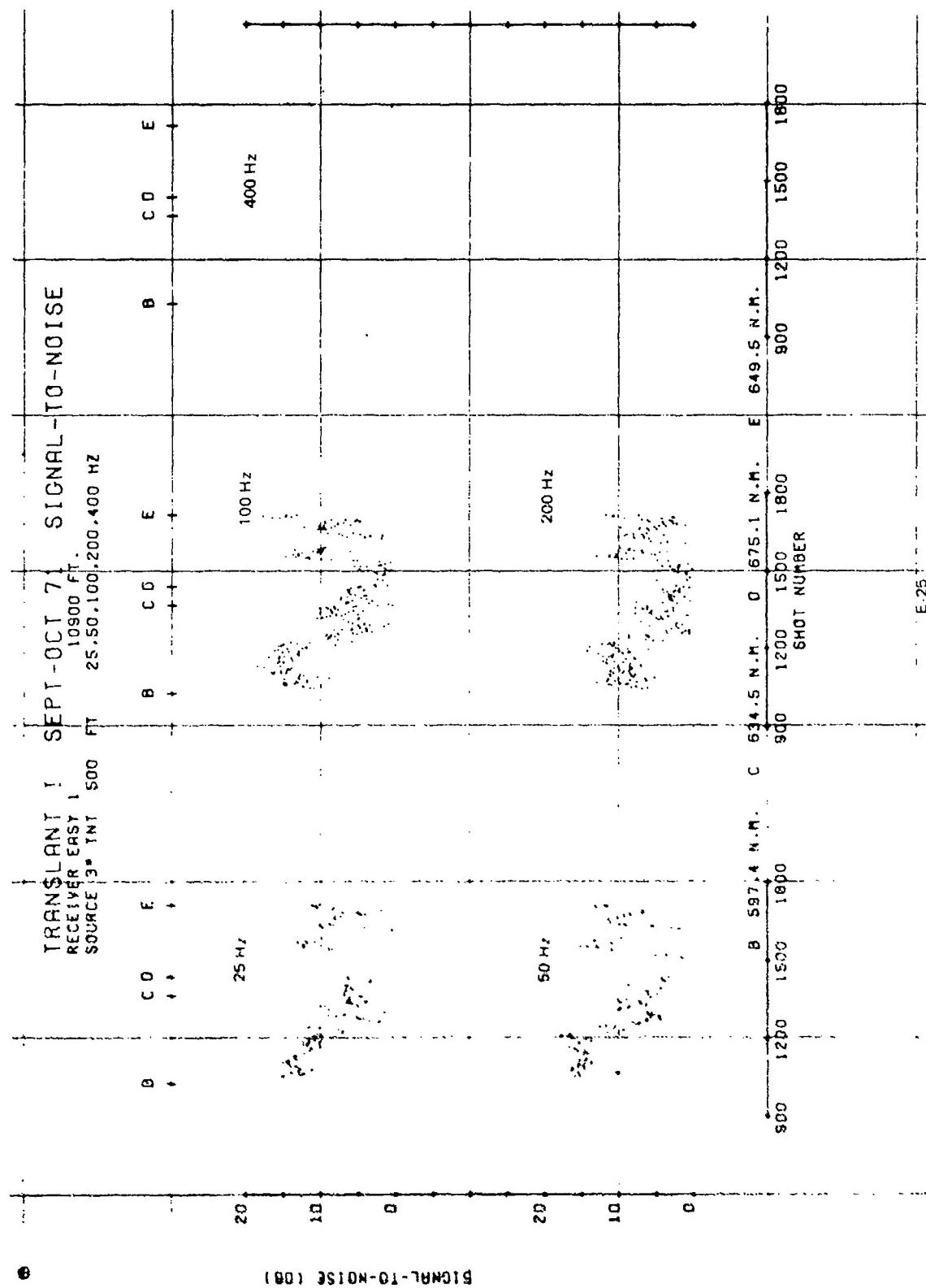
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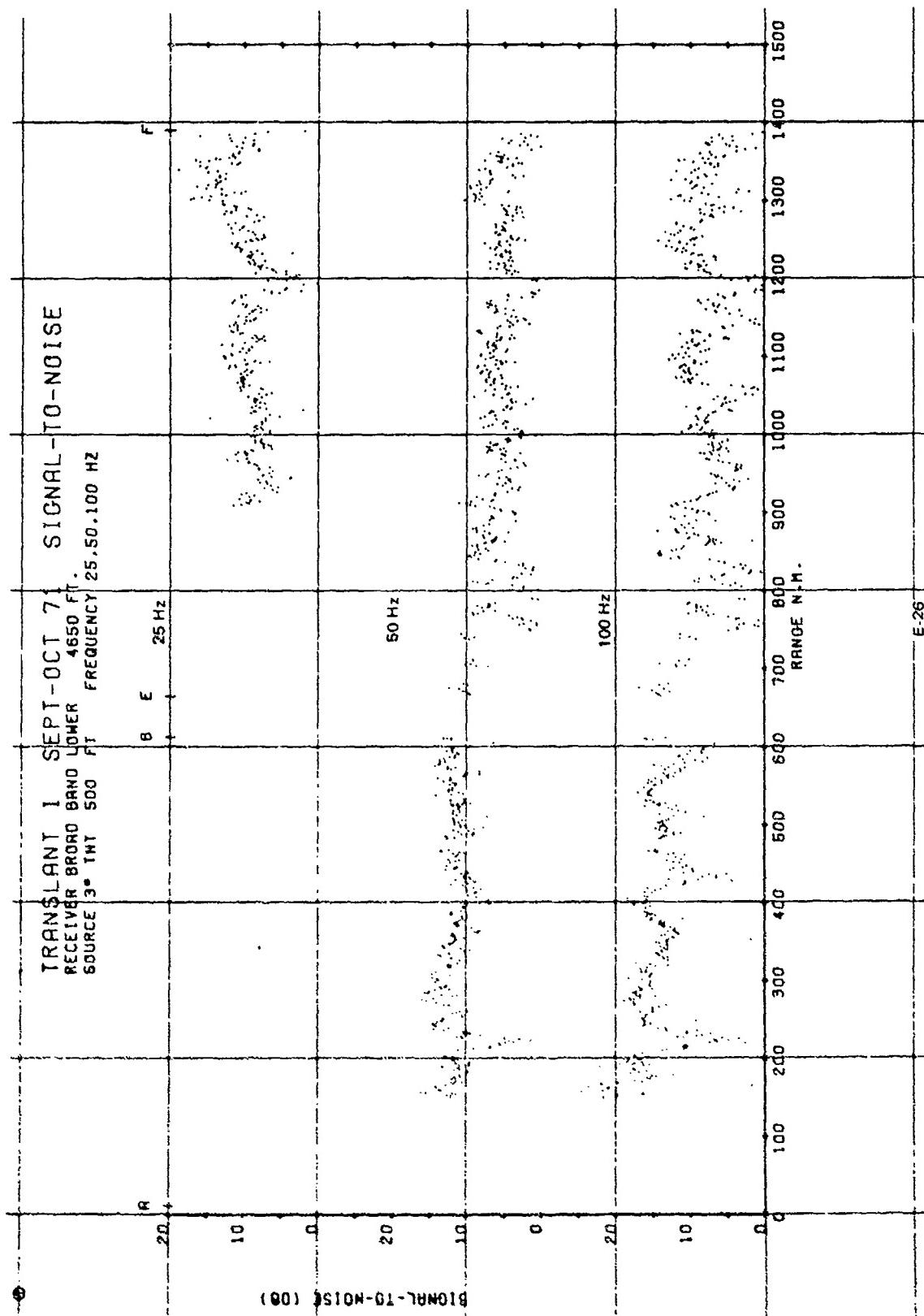
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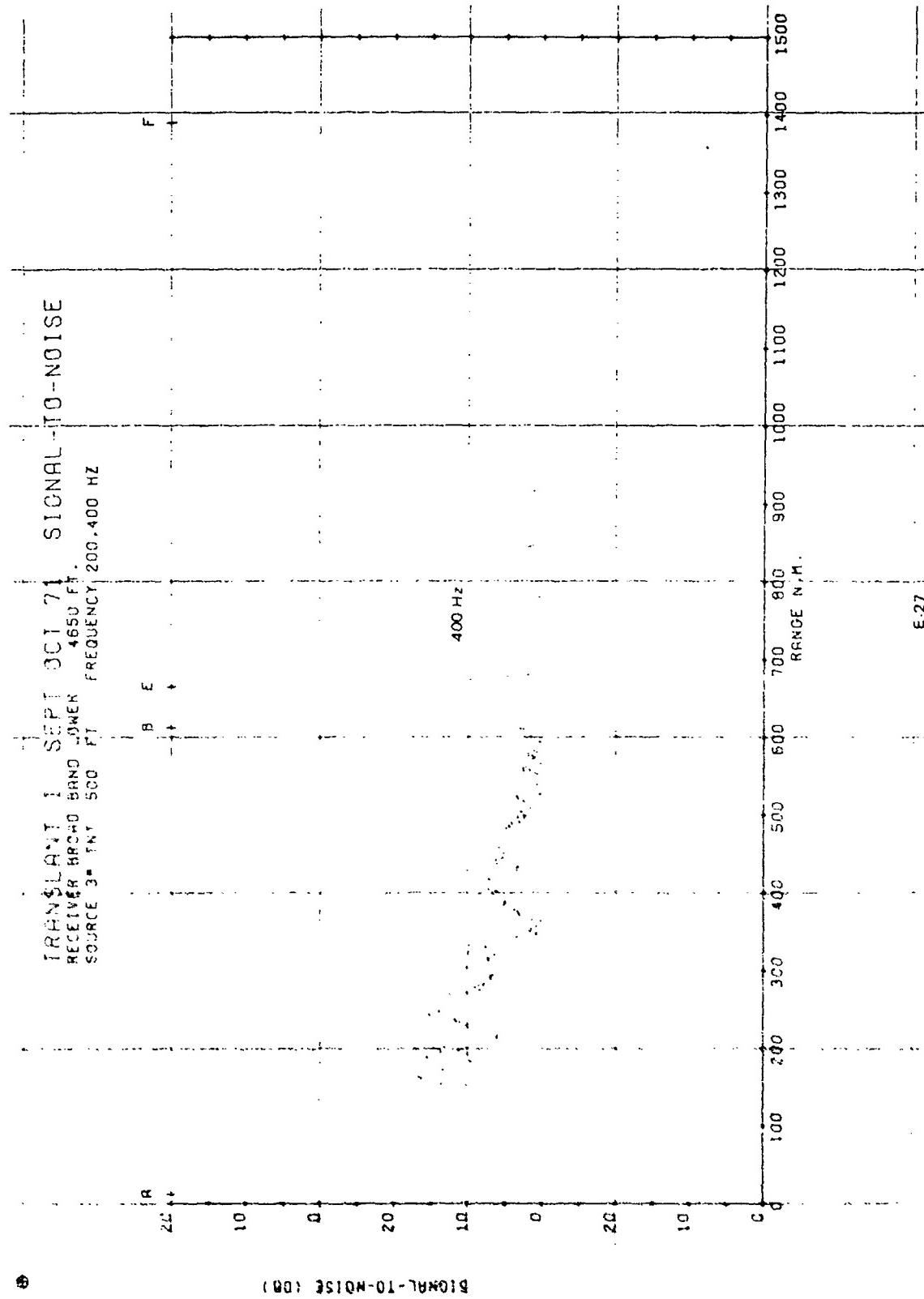
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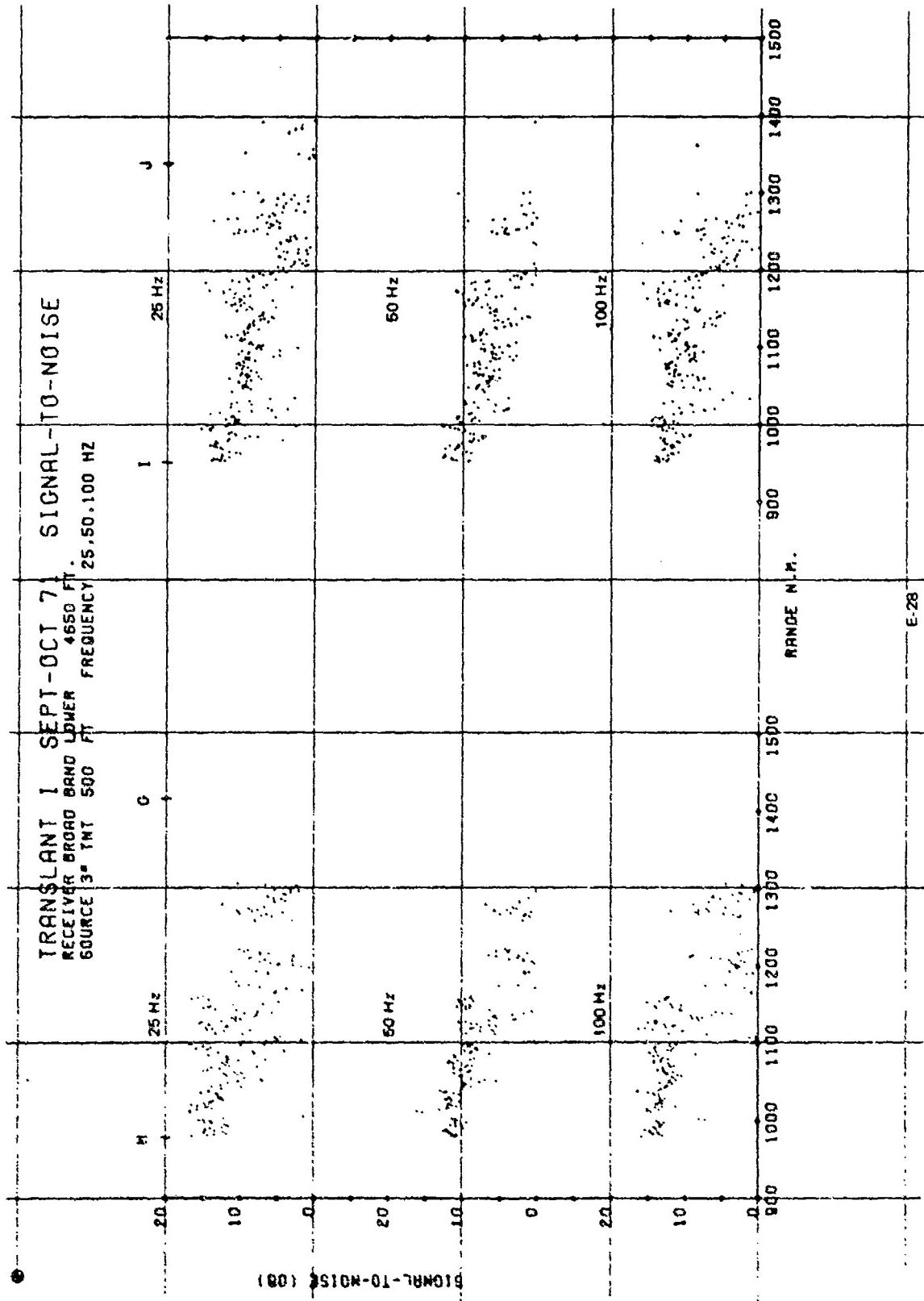
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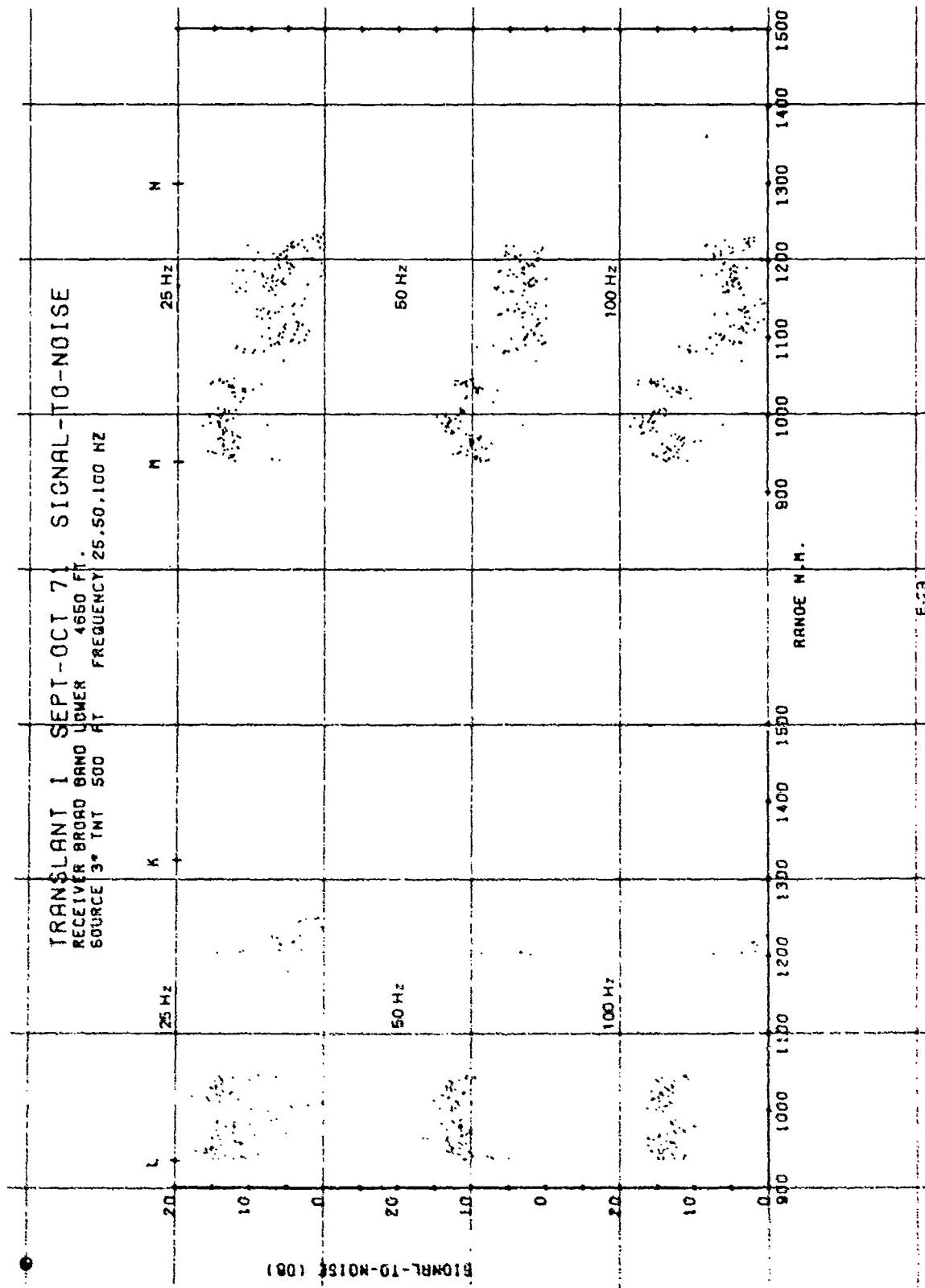
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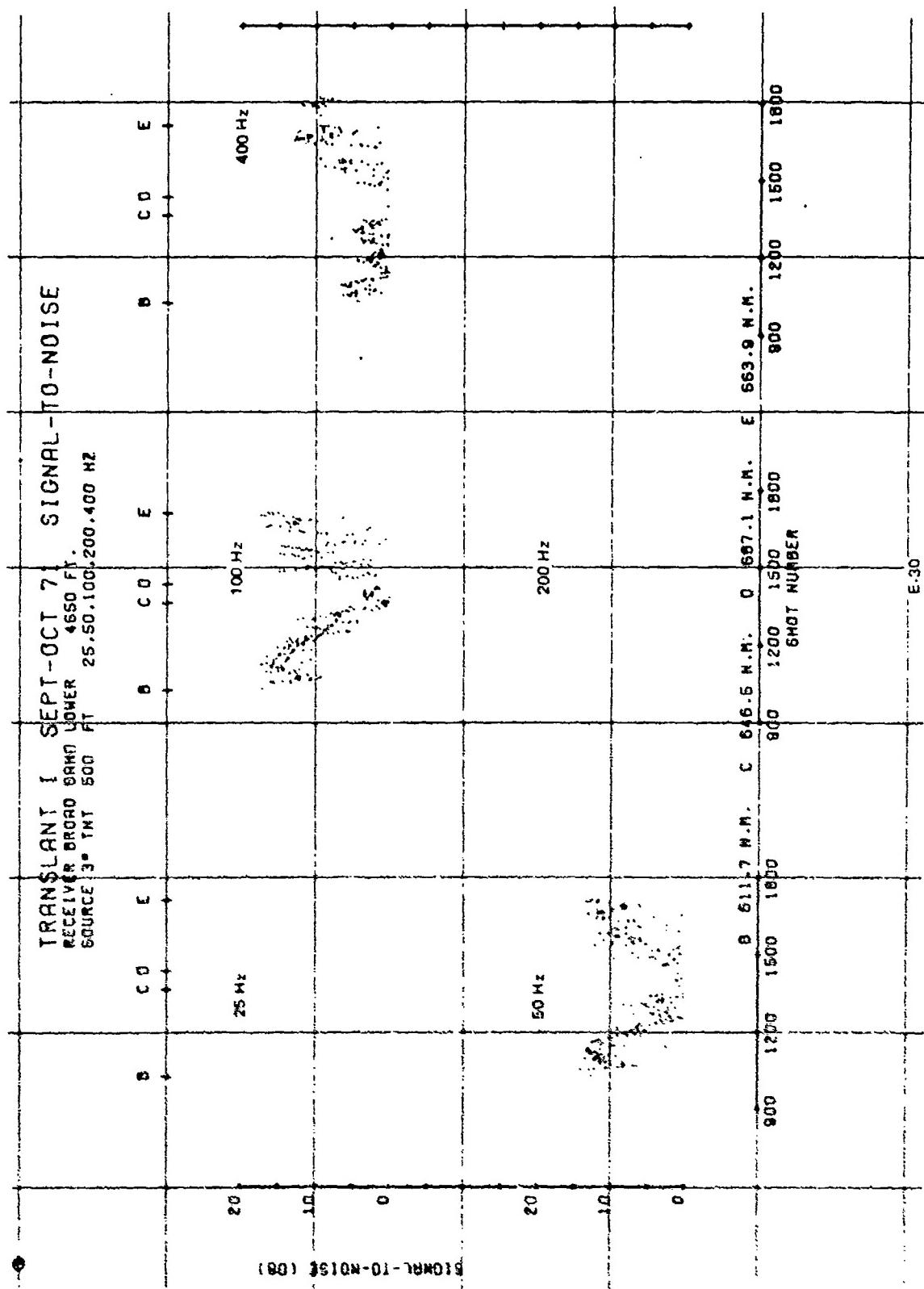
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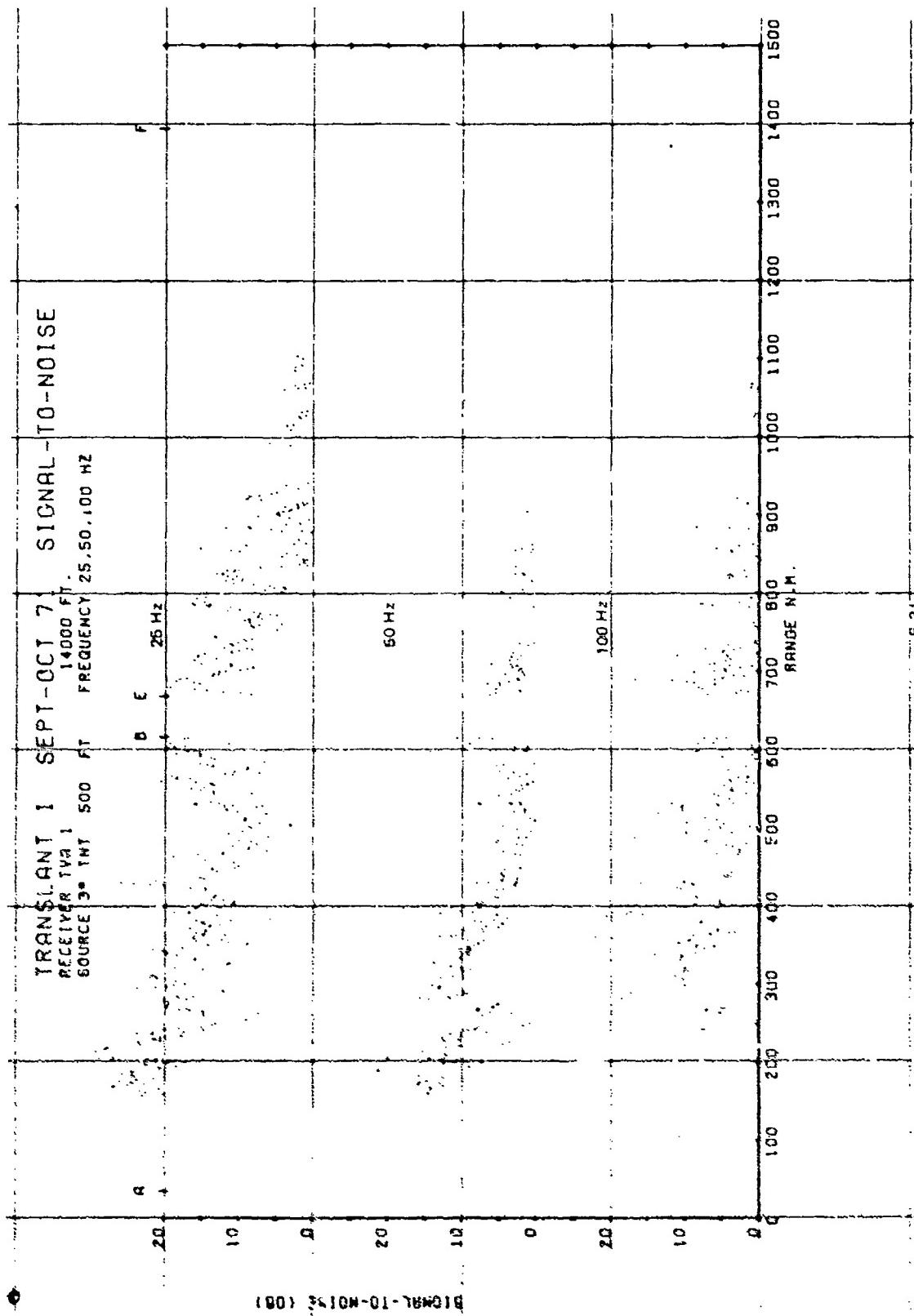
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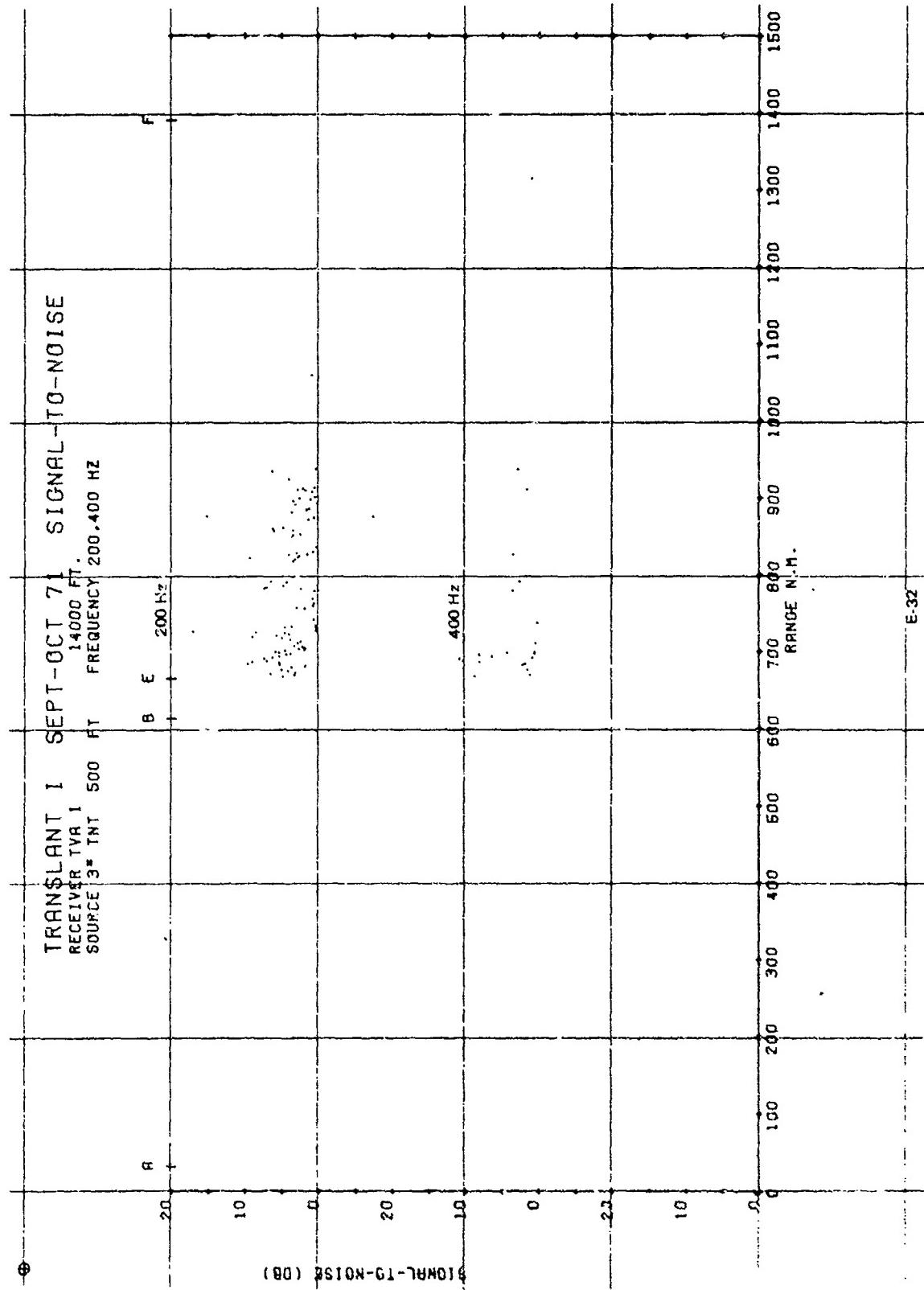


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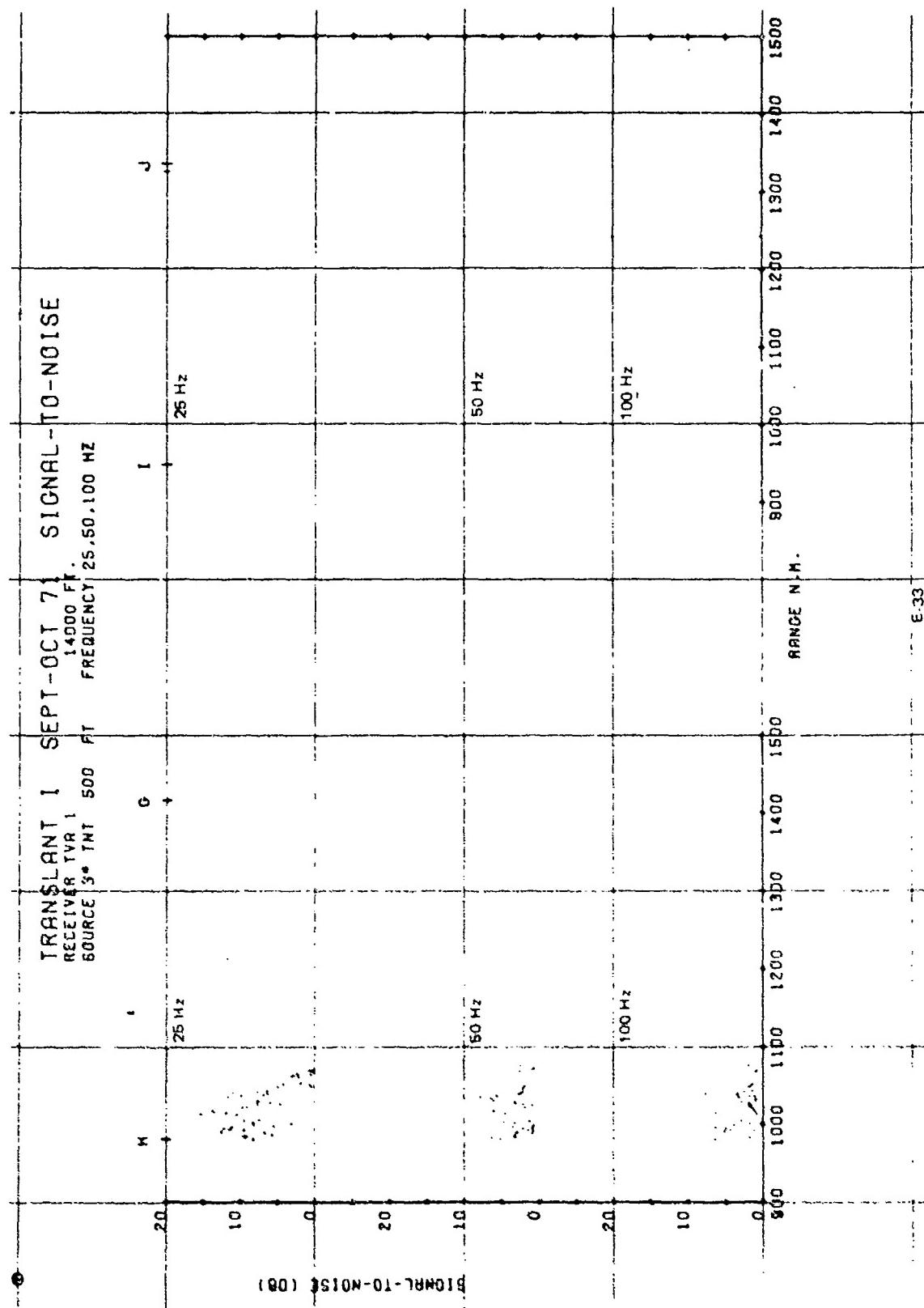
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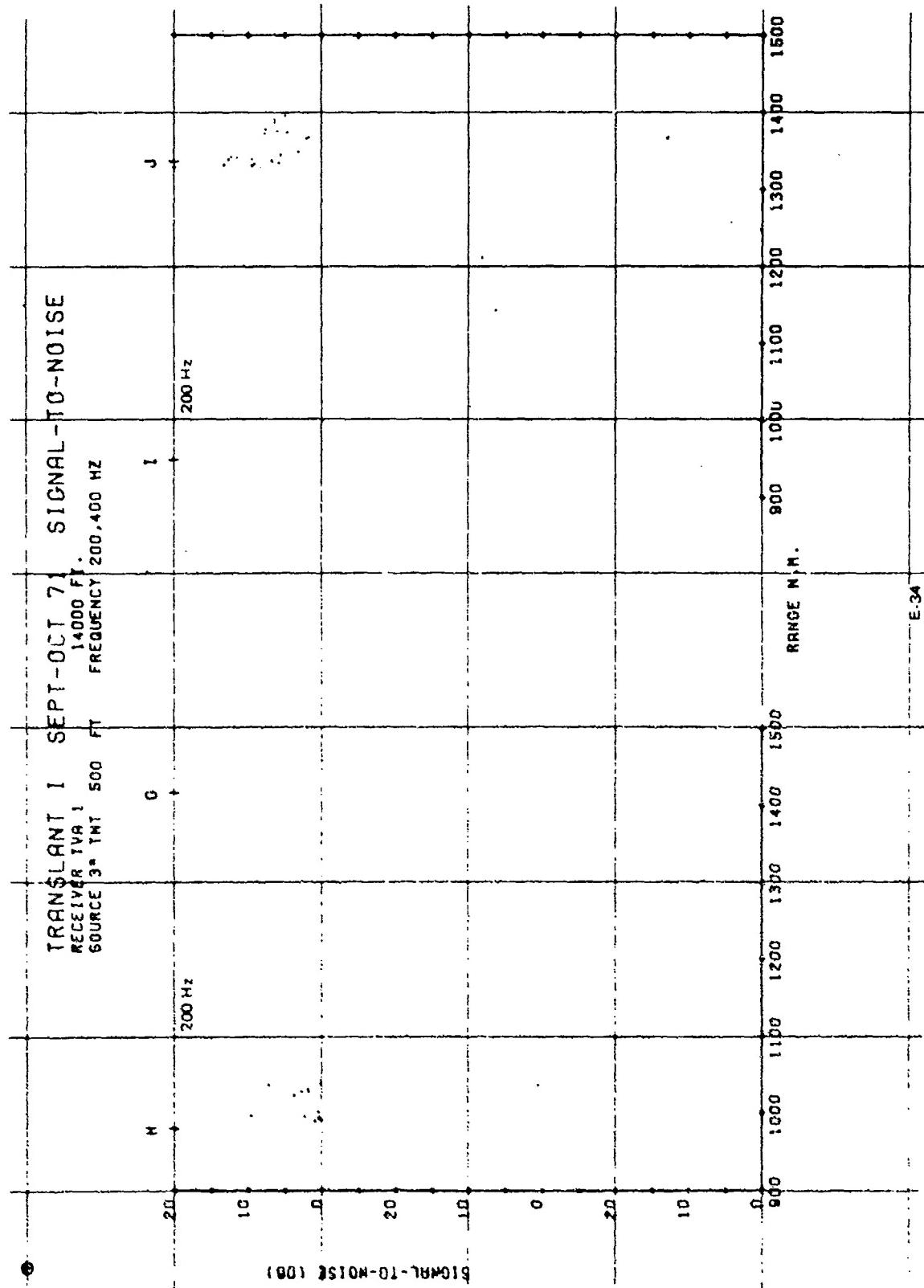
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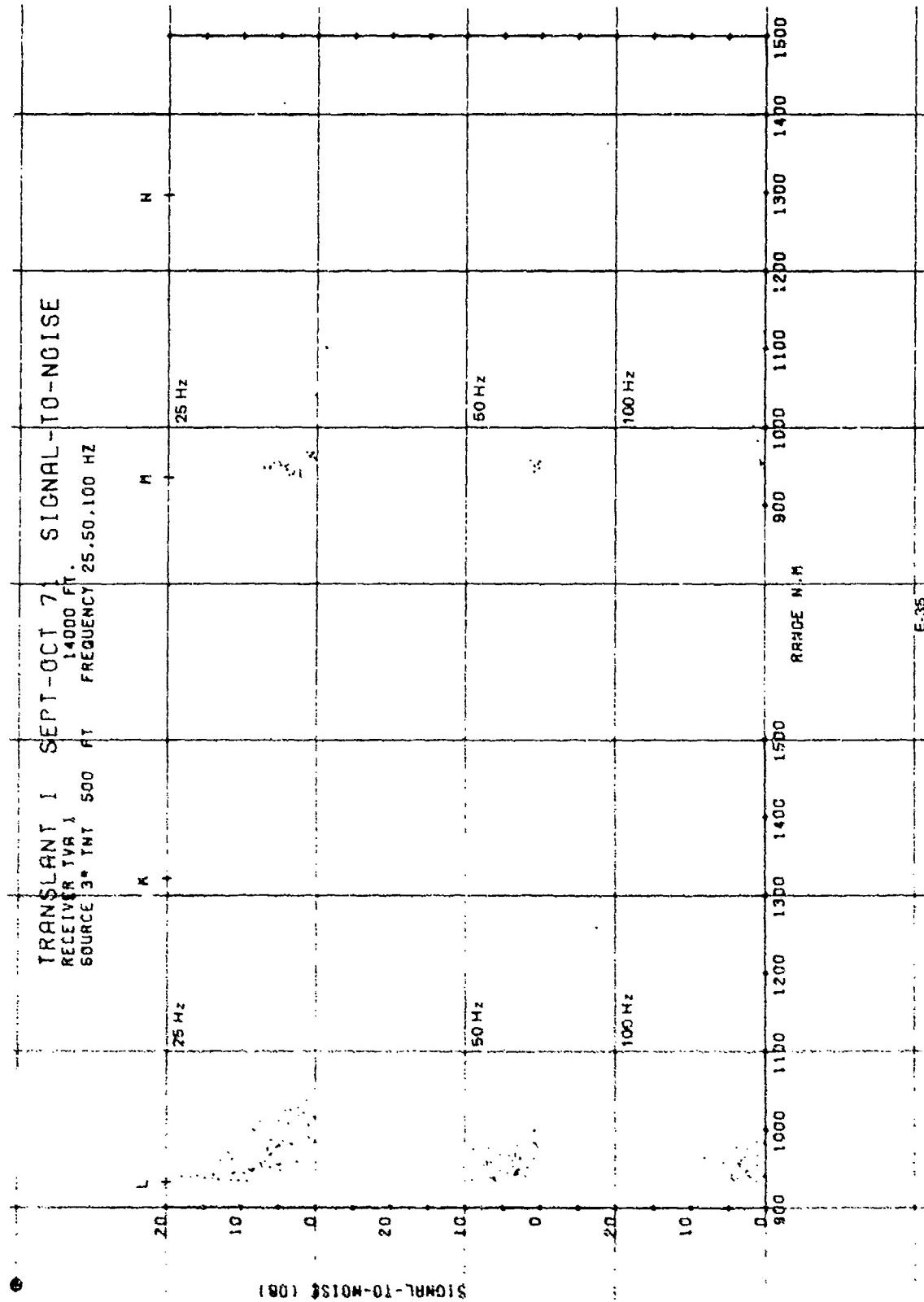
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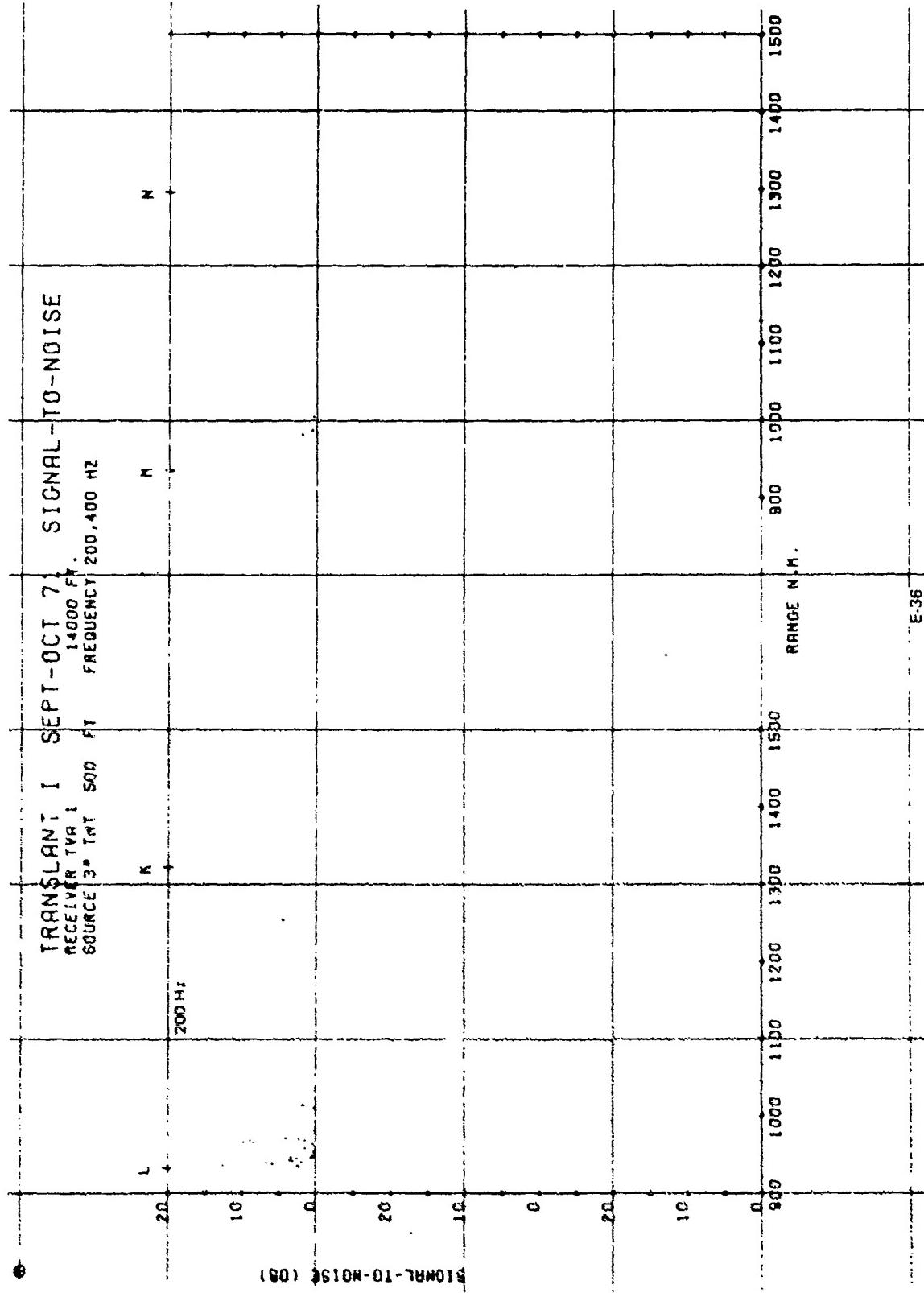
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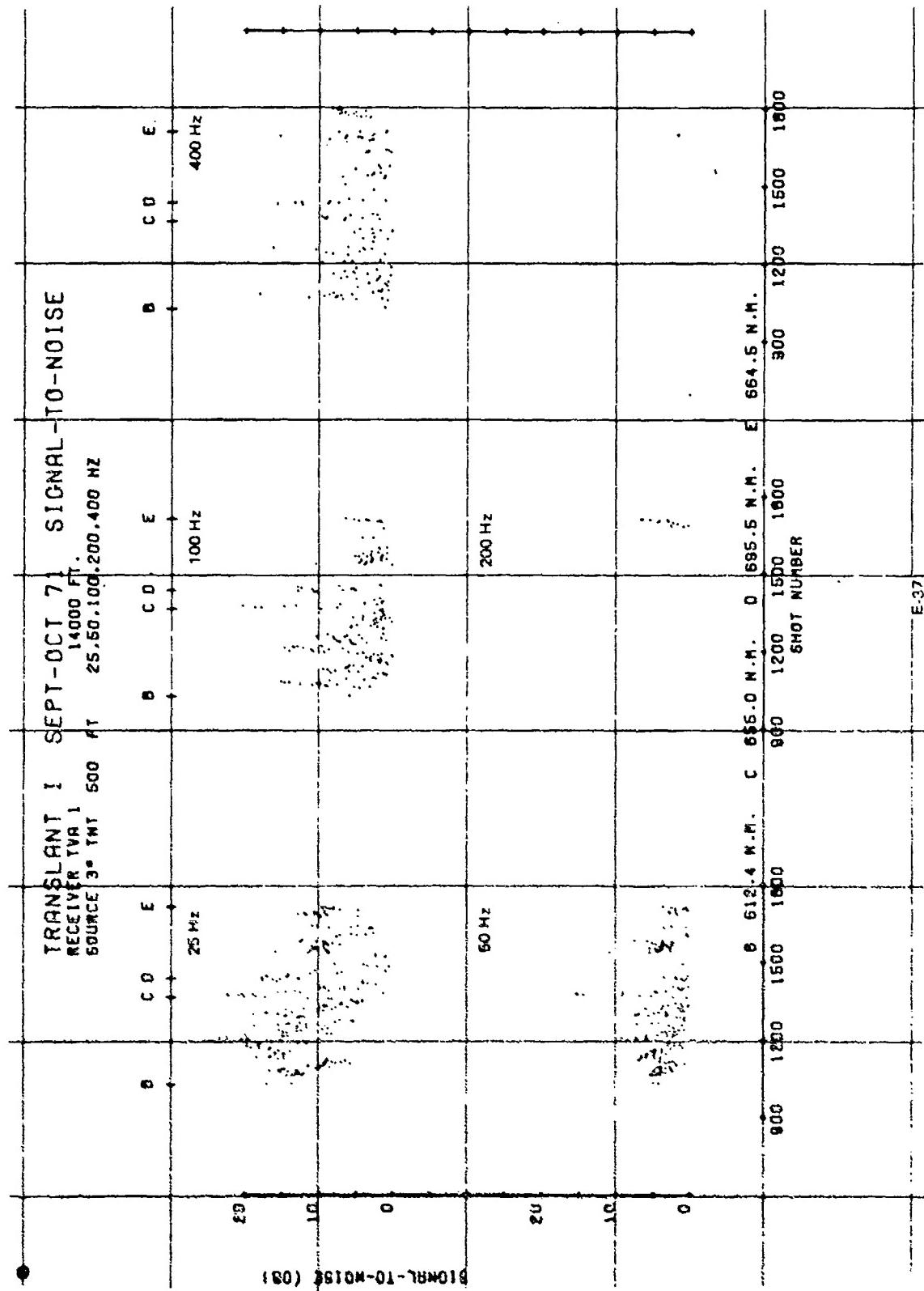
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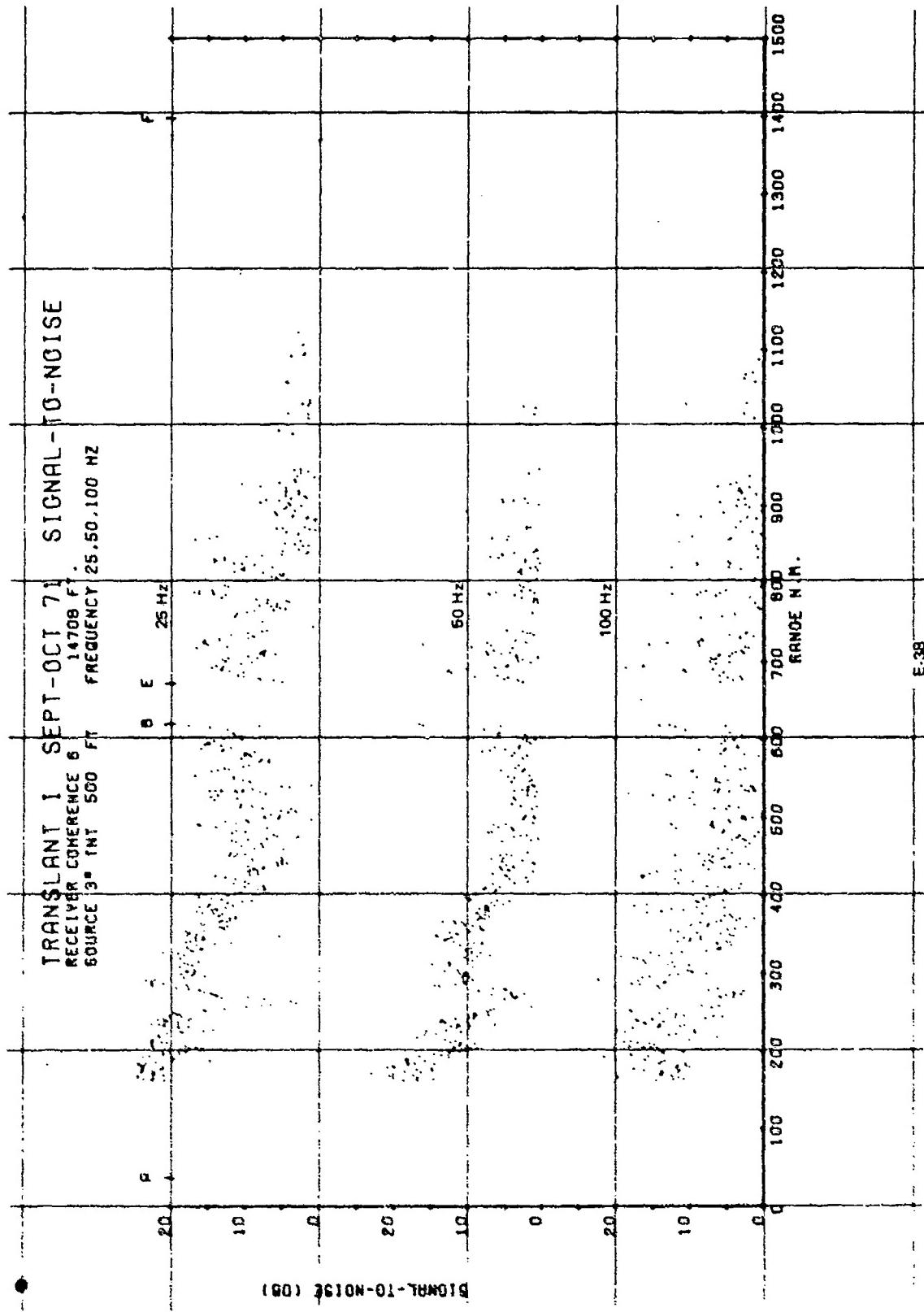
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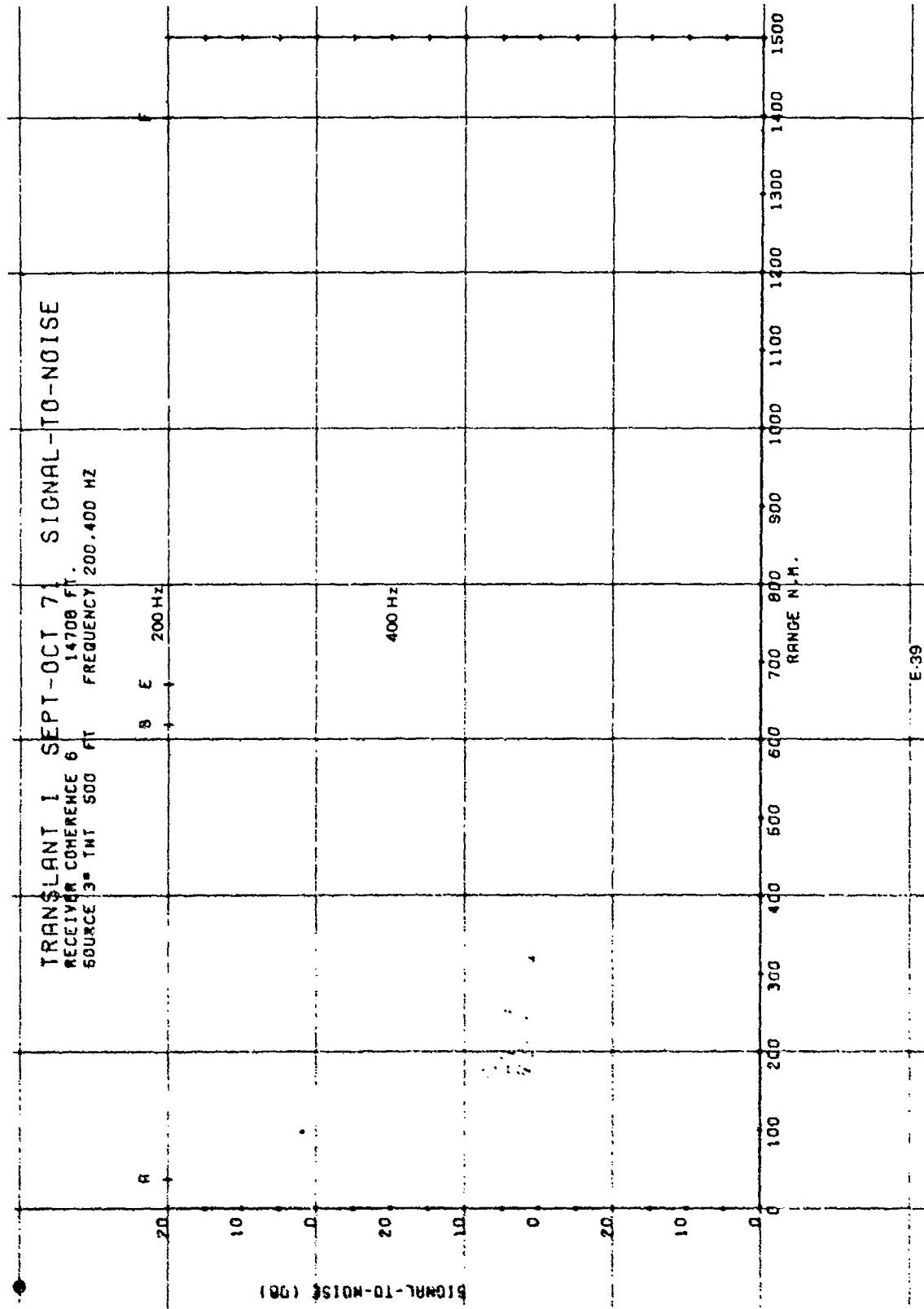
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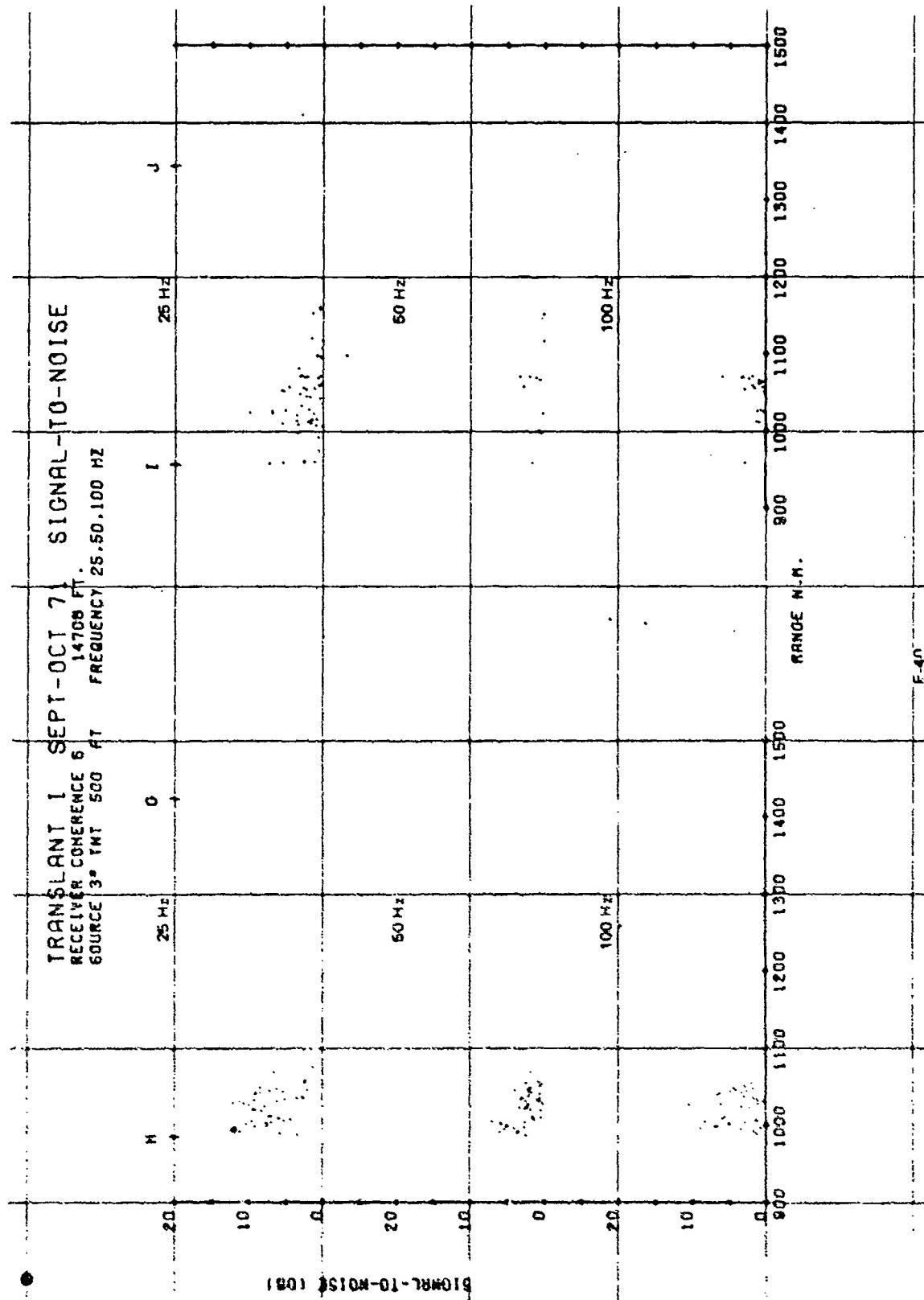
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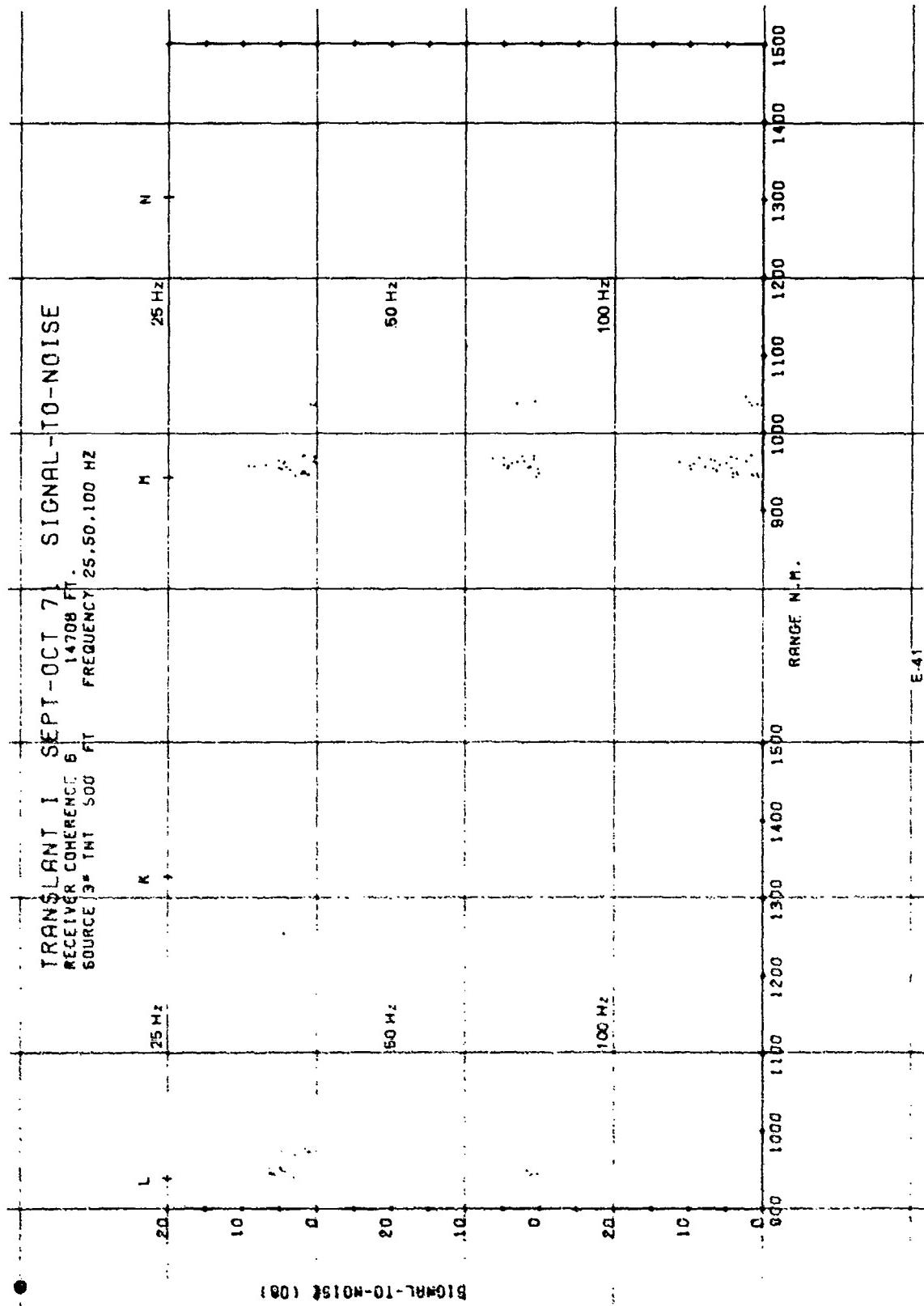
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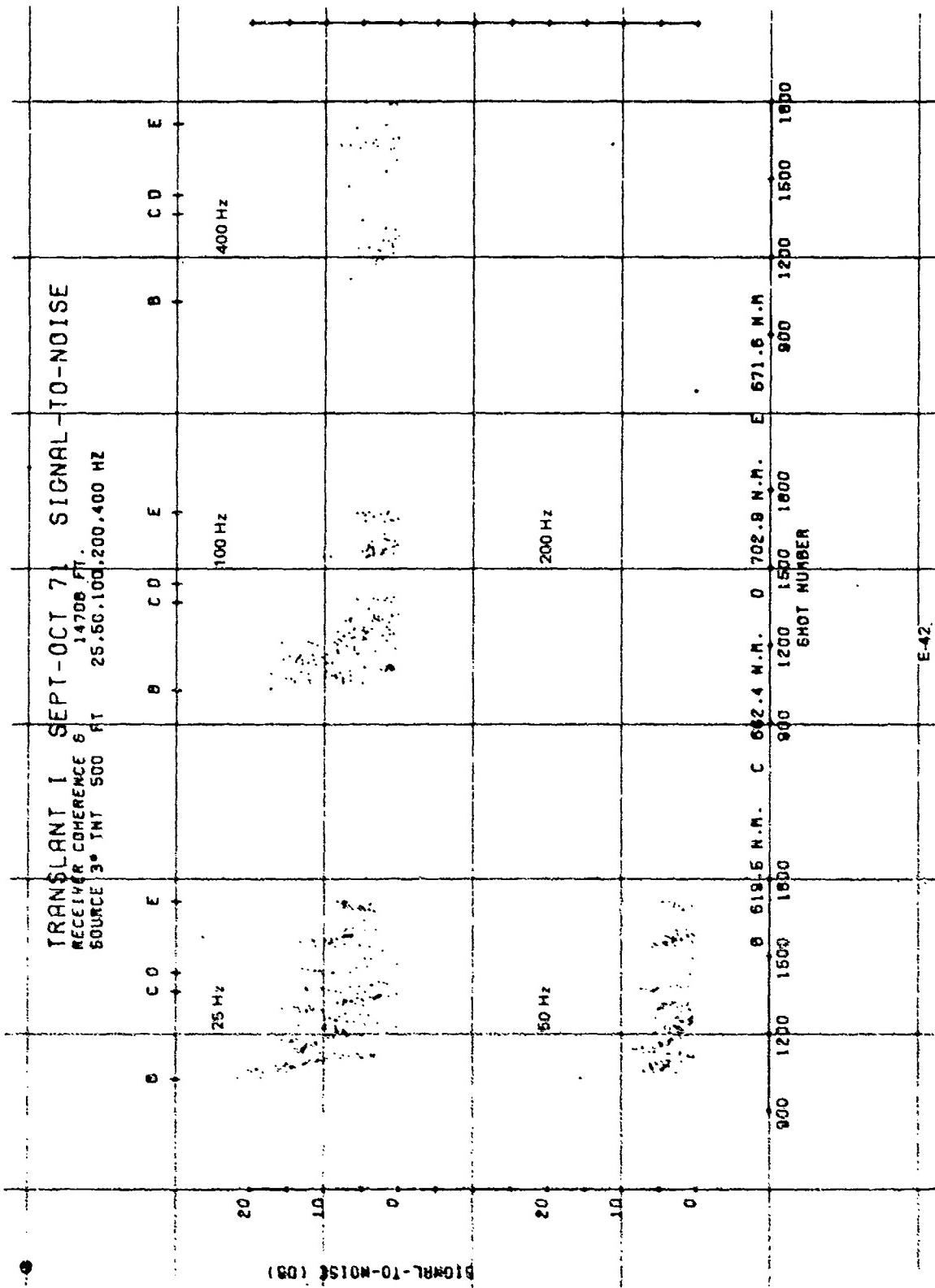


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Appendix F

TRANSLANT I AND ATOE PROPAGATION LOSS COMPARISON

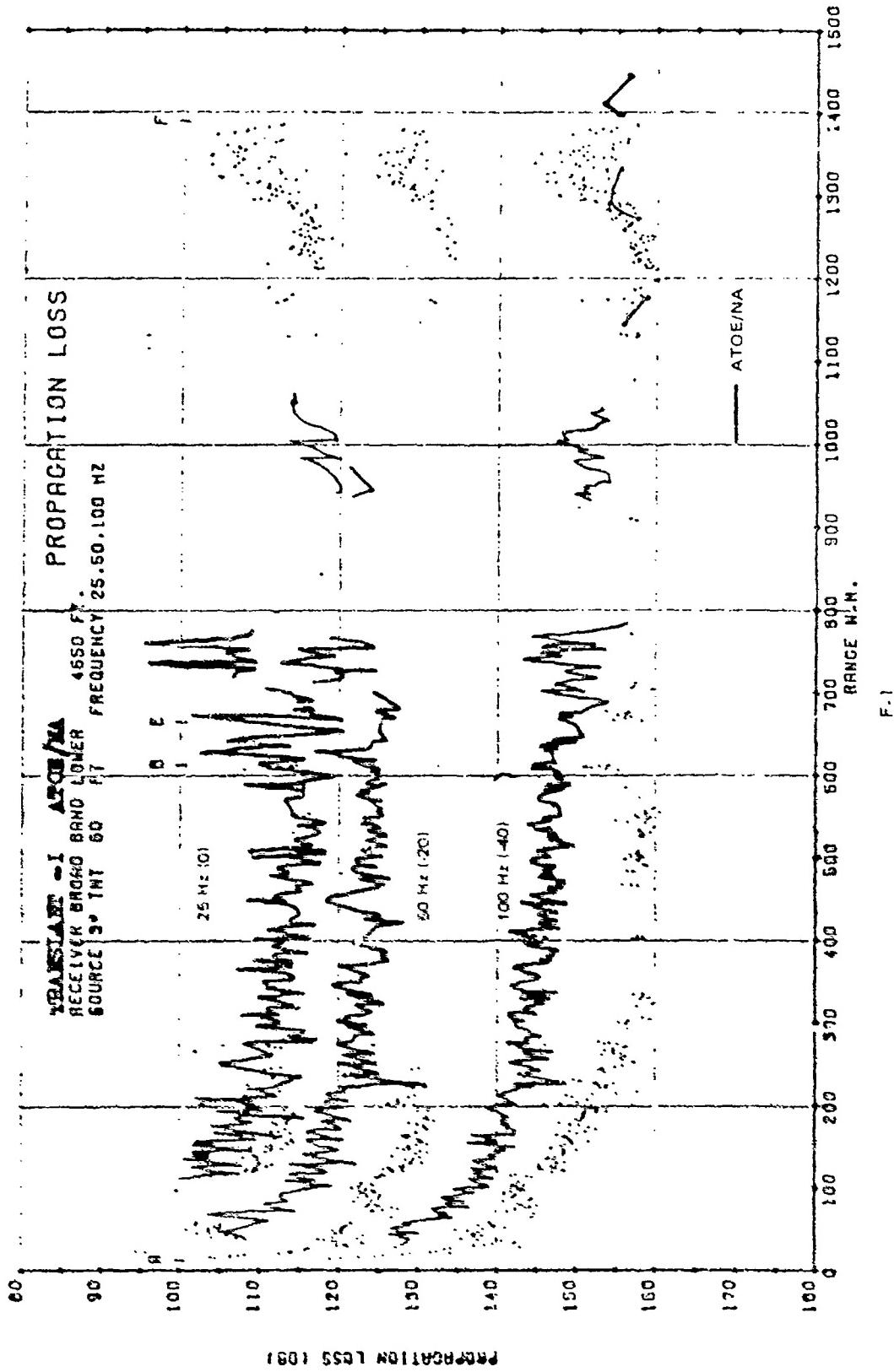
(U) Plots comparing the propagation loss for the TRANSLANT I and ATOE measurements as a function of range, frequency, and hydrophone are shown on the following pages.

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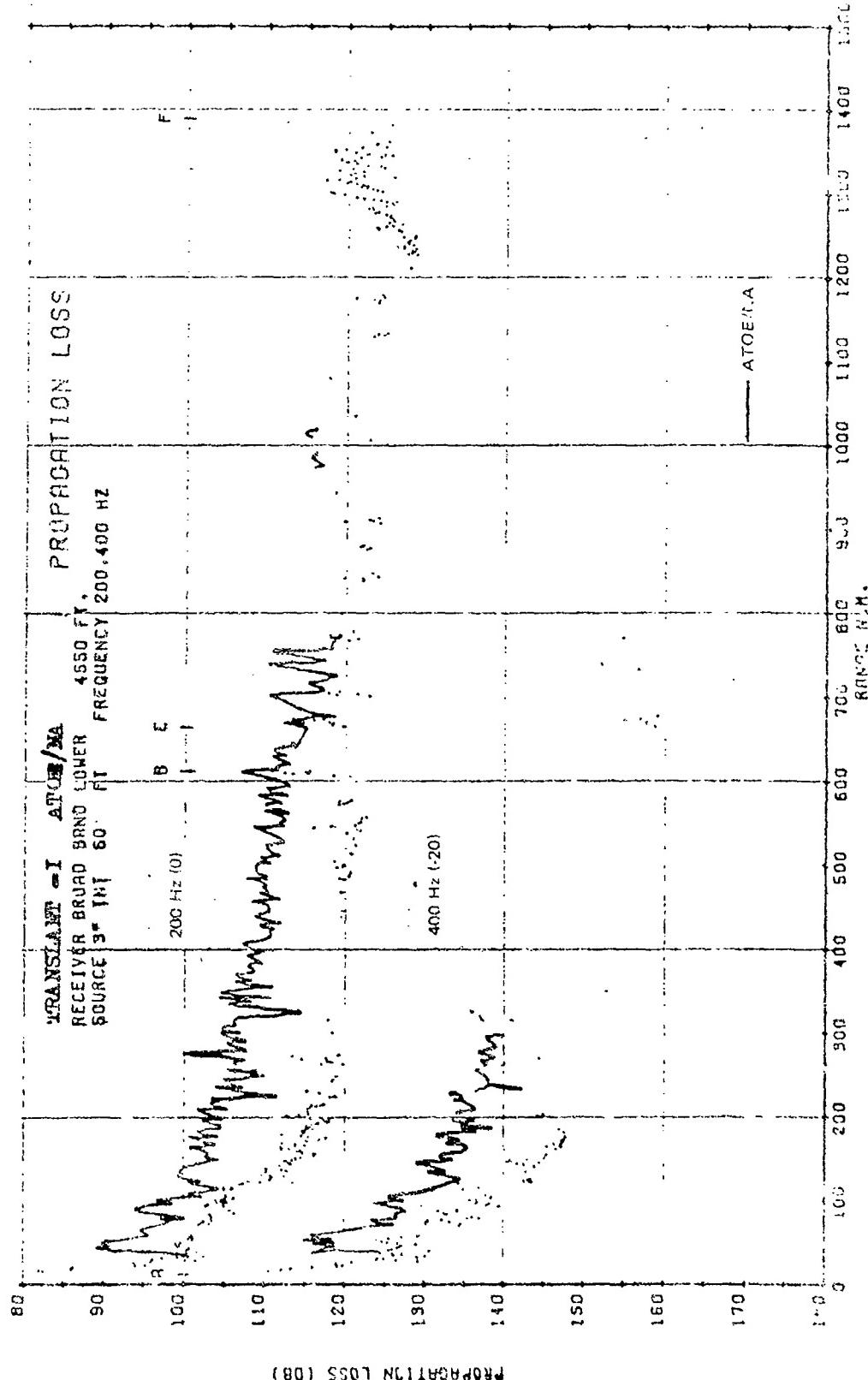


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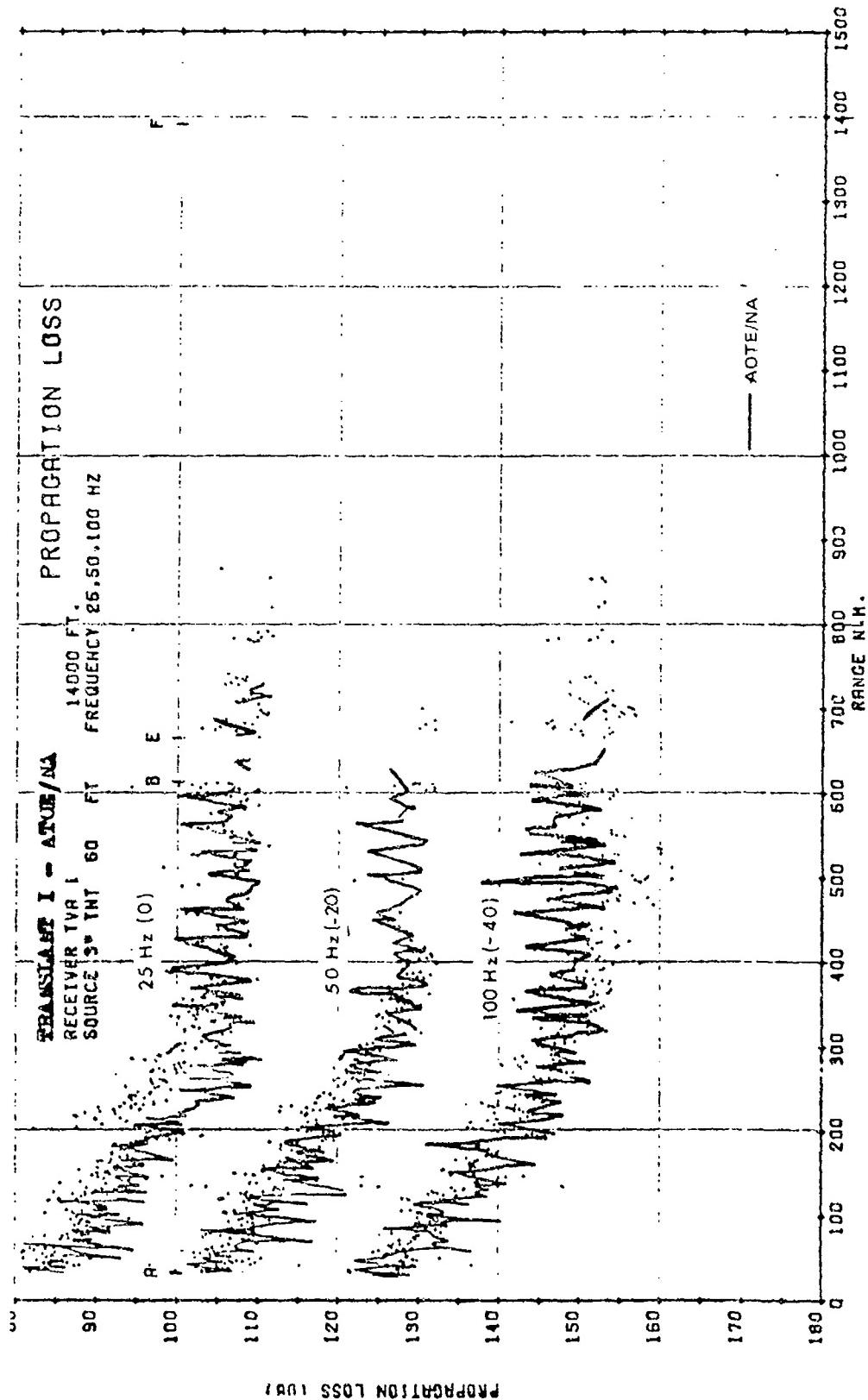
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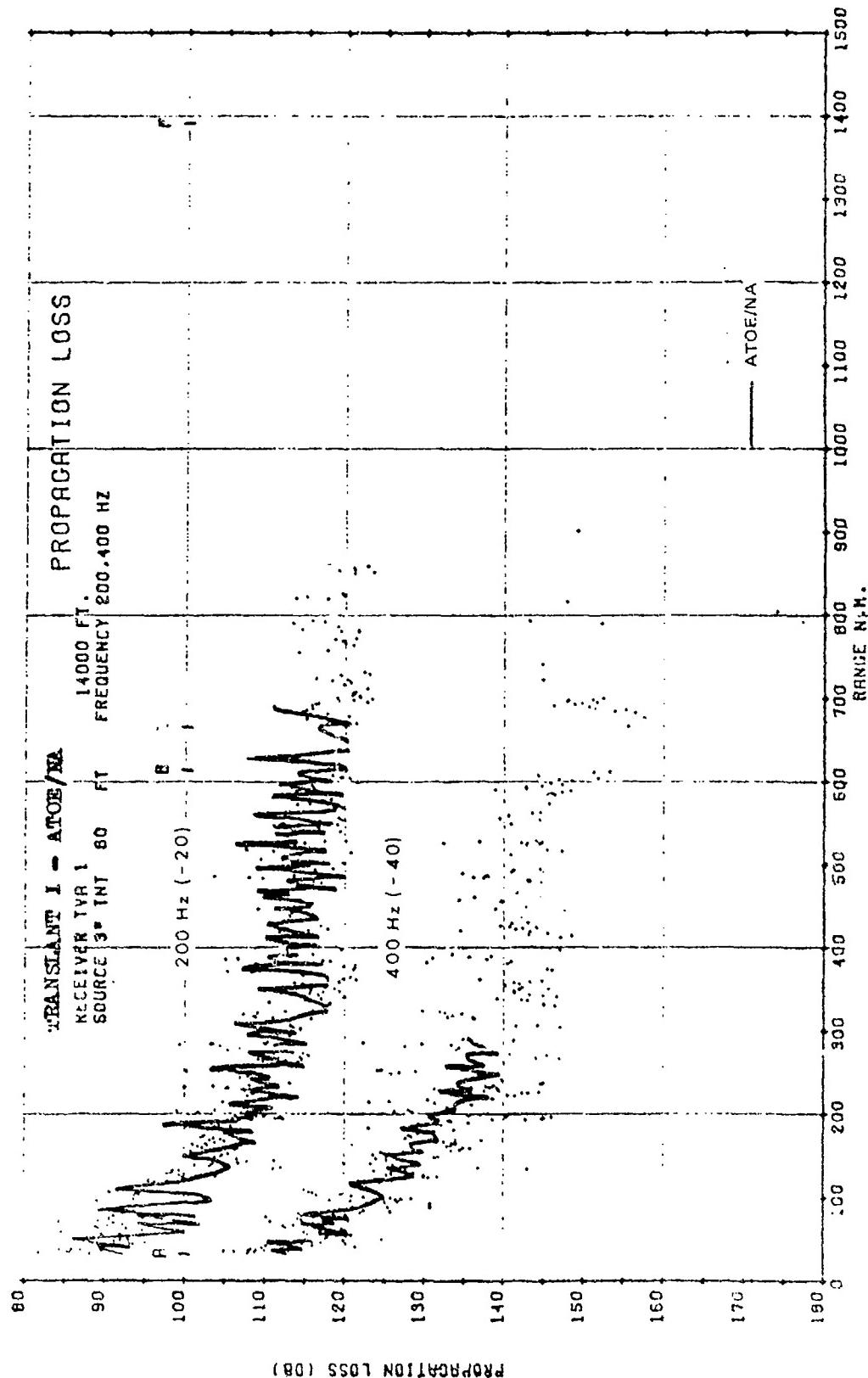


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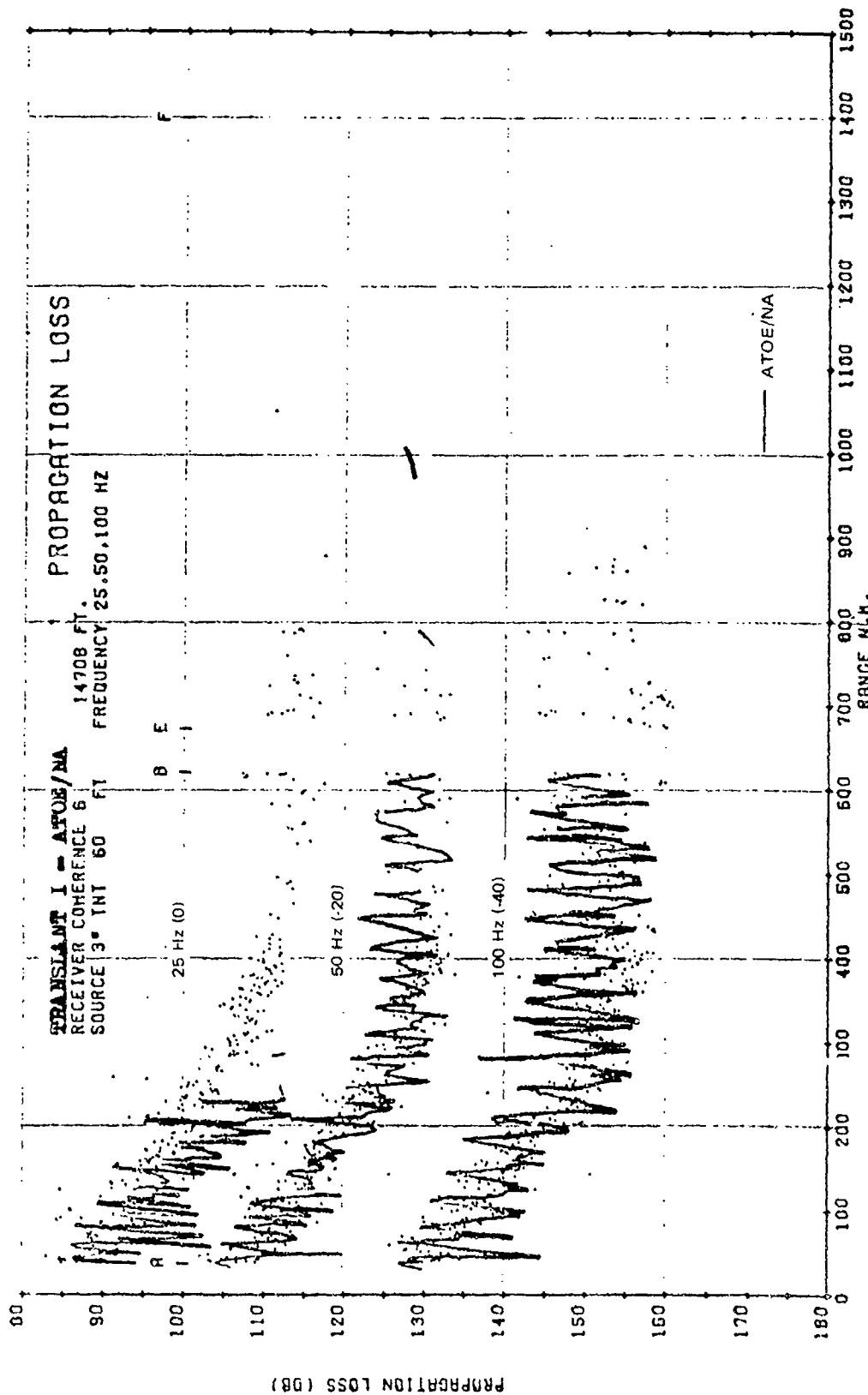
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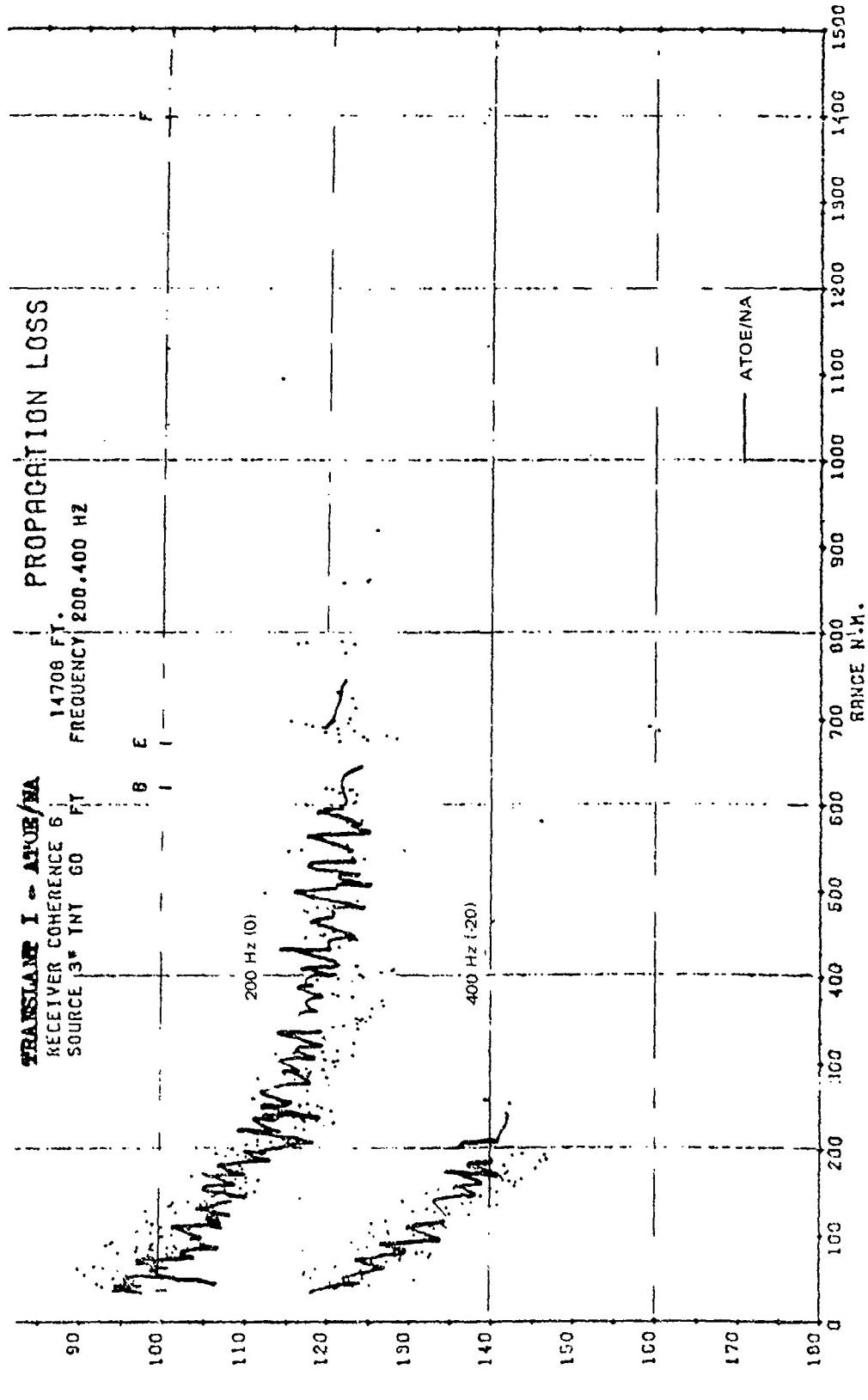


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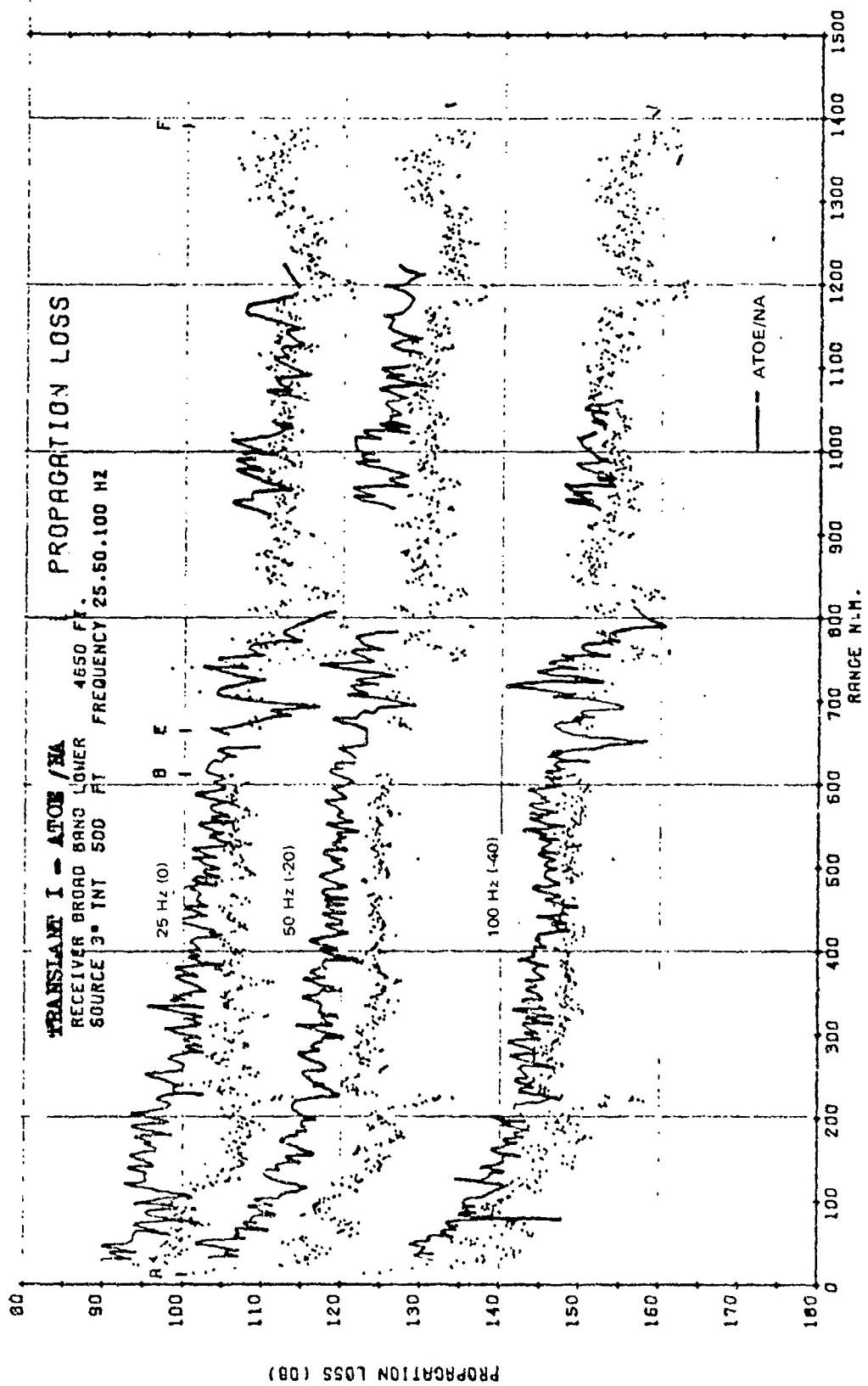
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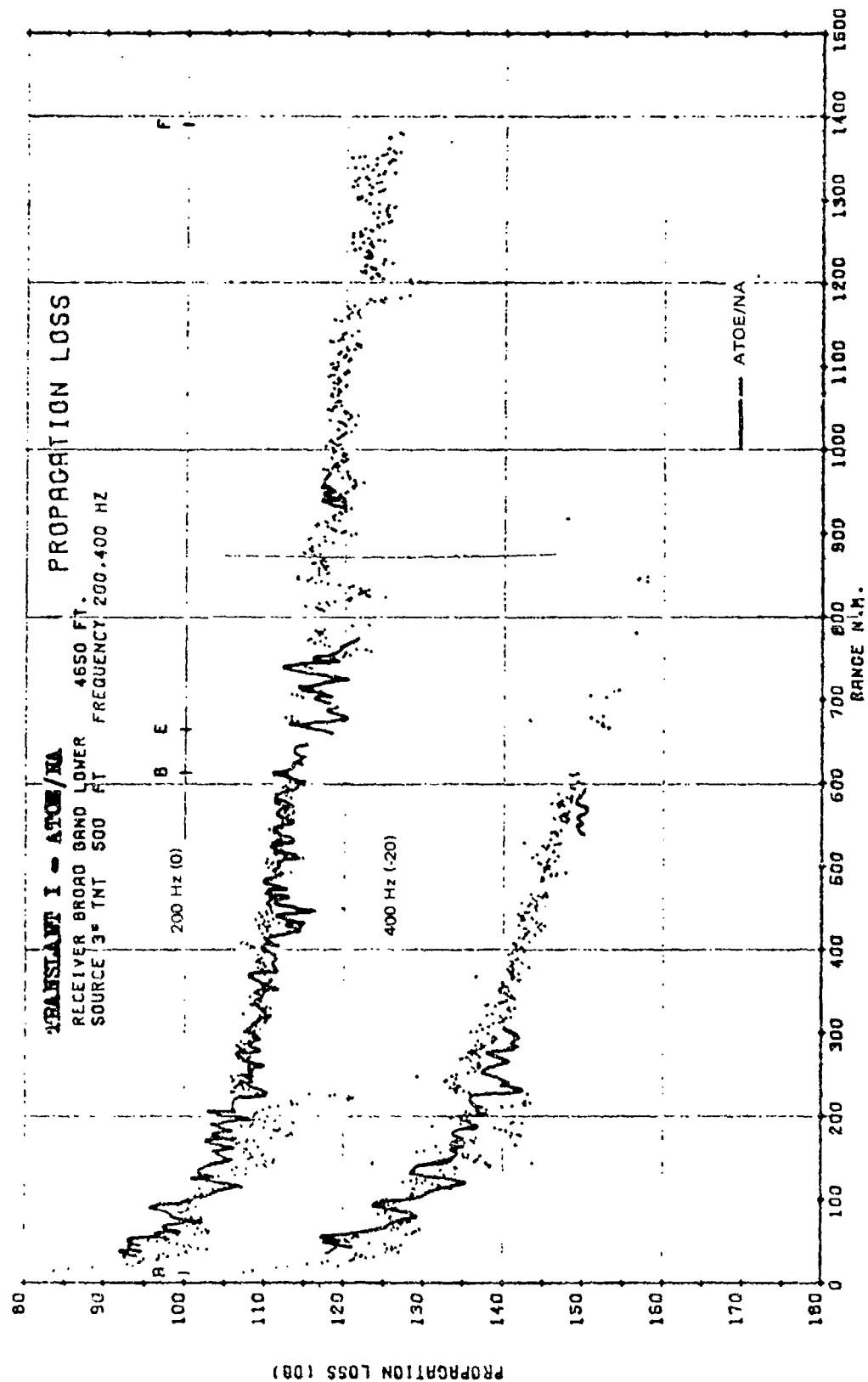
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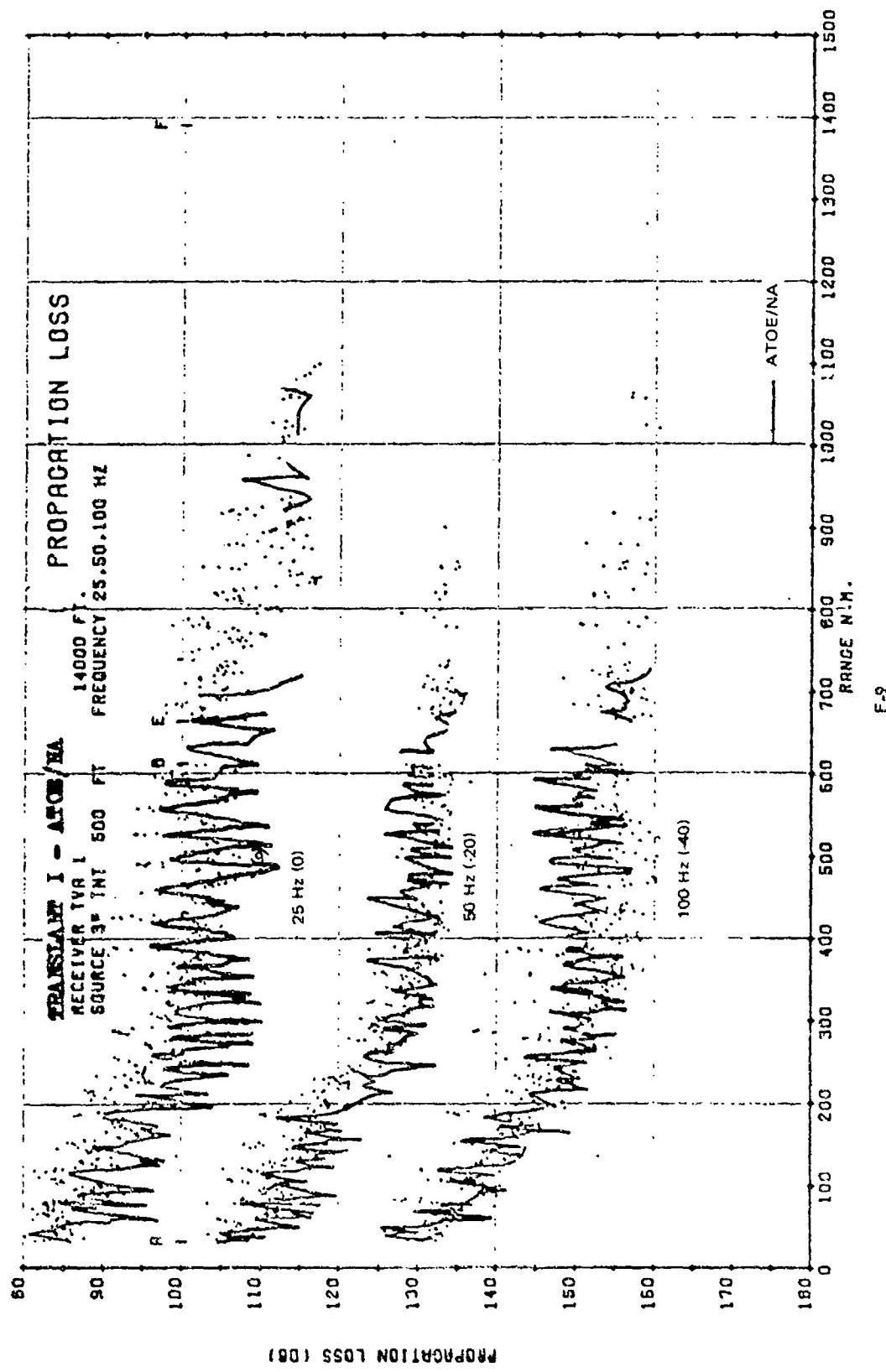


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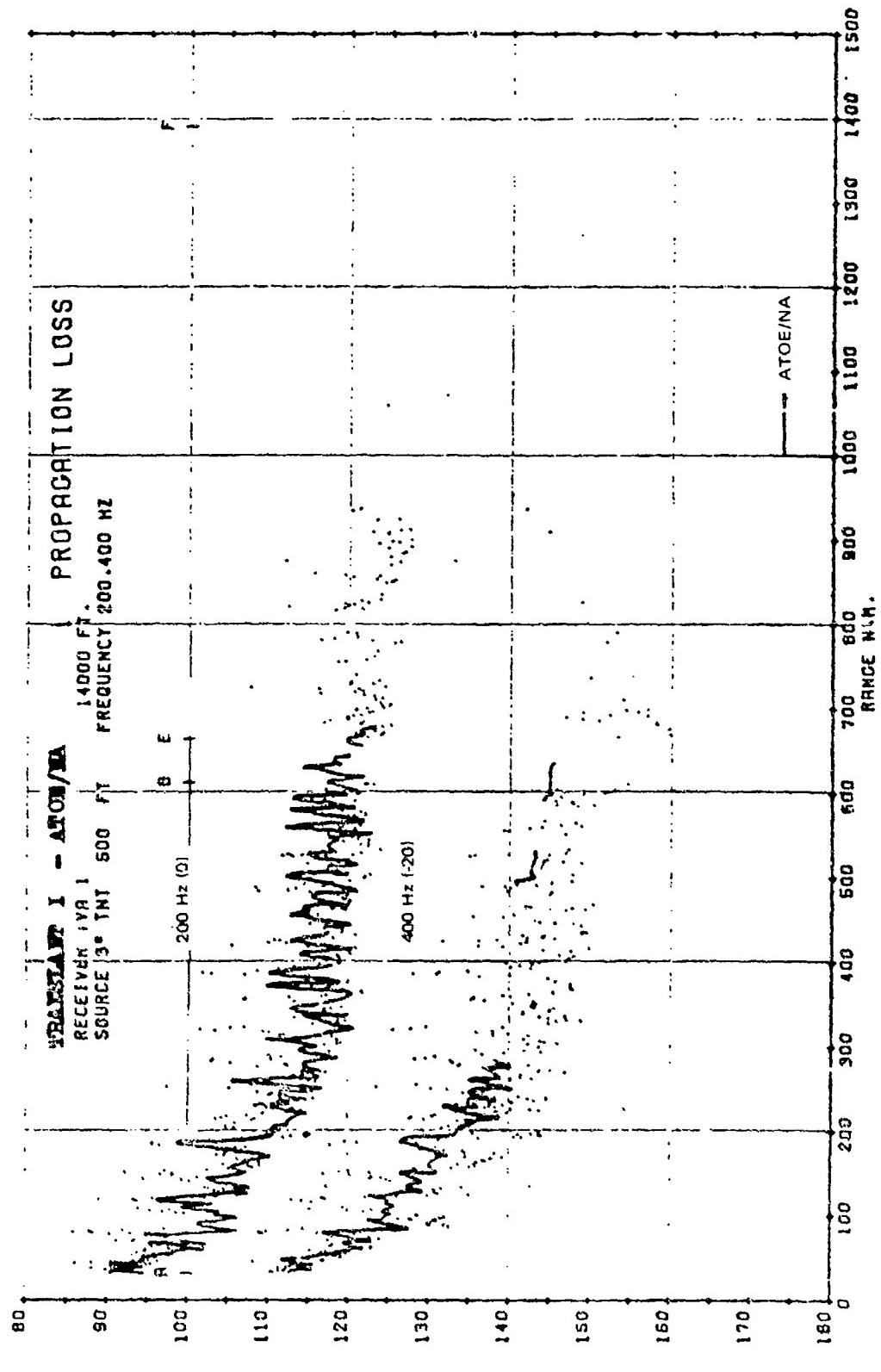
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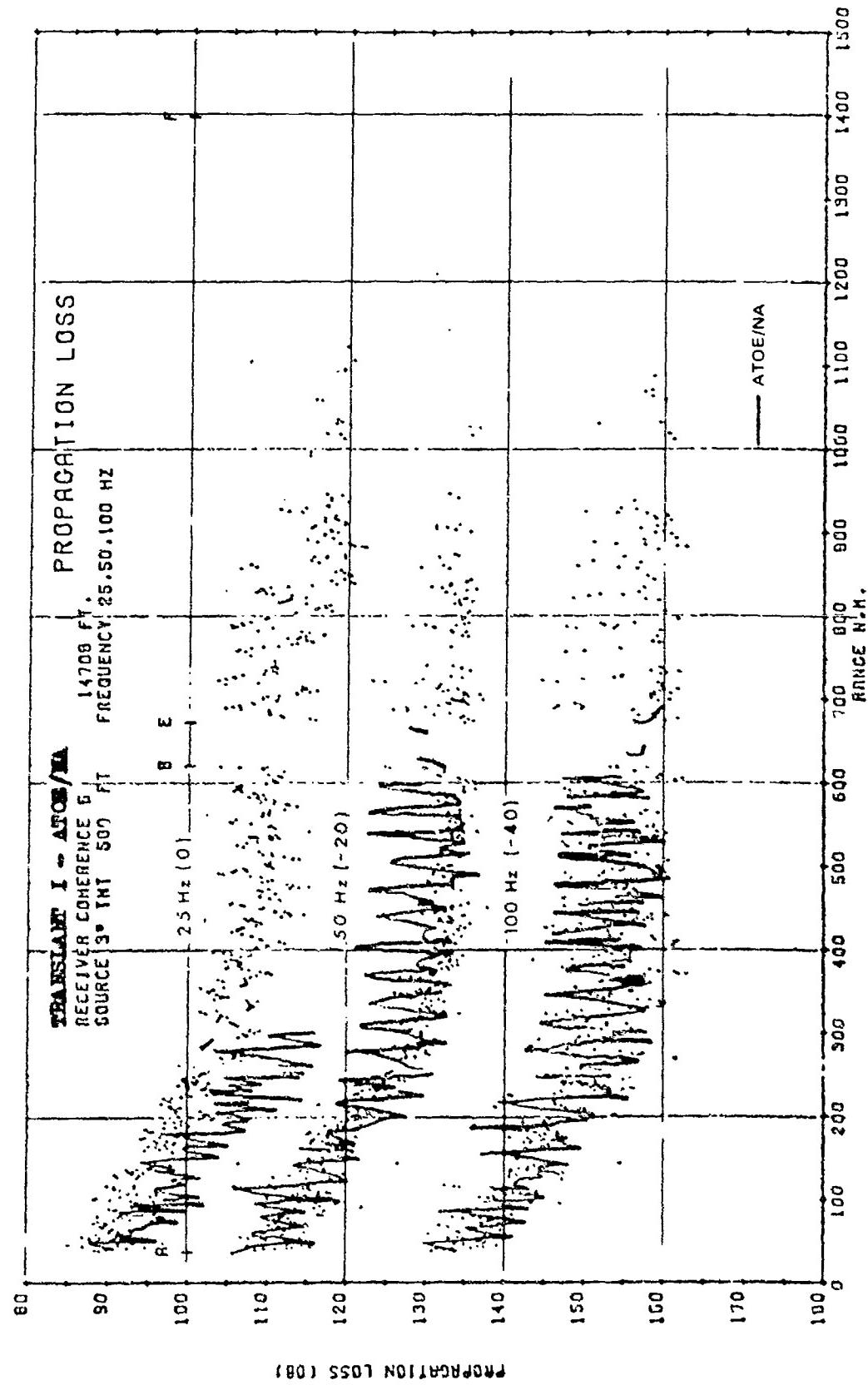


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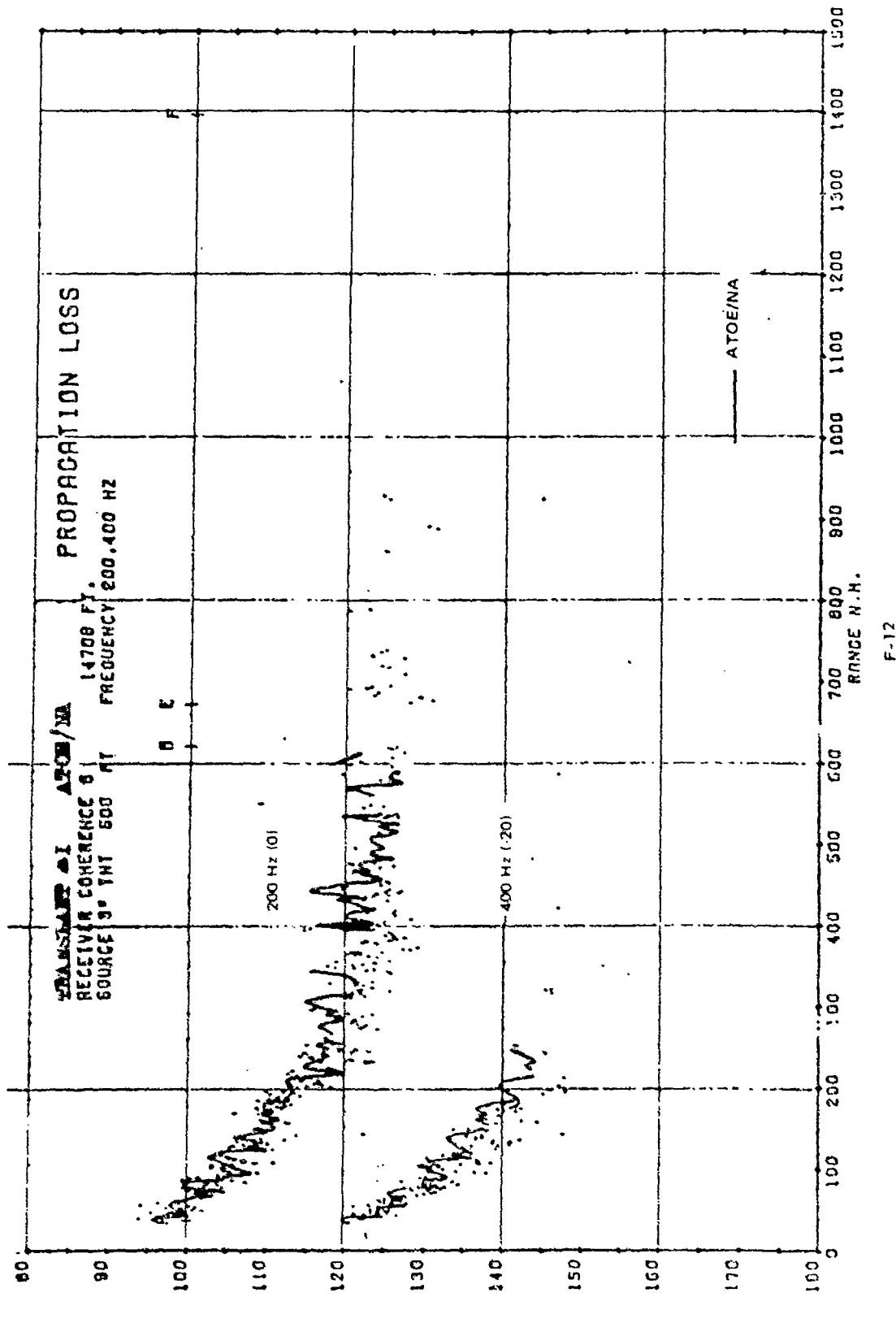
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Report Number	Personal Author	Title	Publication Source (Originator)	Pub. Date	Current Availability	Class.
Unavailable	Beam, J. P., et al.	LONG-RANGE ACOUSTIC PROPAGATION LOSS MEASUREMENTS OF PROJECT TRANSLANT I IN THE ATLANTIC OCEAN EAST OF BERMUDA	Naval Underwater Systems Center	740612	ADC001521	U
Unavailable	Cornyn, J. J., et al.	AMBIENT-NOISE PREDICTION. VOLUME 2. MODEL EVALUATION WITH JOMEDEX DATA	Naval Research Laboratory	740701	AD0530983	U
Unavailable	Unavailable	COHERENCE OF HARMONICALLY RELATED CW SIGNALS	Naval Underwater Systems Center	740722	ADB181912	U
Unavailable	Banchero, L. A., et al.	JOMEDEX SOUND VELOCITY ANALYSIS AND ENVIRONMENTAL DATA SUMMARY	Naval Oceanographic Office	740801	ADC00419	U
3810	Unavailable	CONSTRUCTION AND CALIBRATION OF USRD TYPE F58 VIBROSEIS MONITORING HYDROPHONES SERIALS 1 THROUGH 7	Naval Research Laboratory	741002	ND	U
	ARL-TM-73-11; ARL-TM-73-12	ARL PRELIMINARY DATA ANALYSIS FROM ACODAC SYSTEM; ANALYSIS OF THE BLAKE TEST ACODAC DATA	University of Texas, Applied Research Laboratories	741015	ADA001738; ND	U
Unavailable	Mitchell, S. K., et al.	QUALITY CONTROL ANALYSIS OF SUS PROCESSING FROM ACODAC DATA	University of Texas, Applied Research Laboratories	741015	ADB000283	U
Unavailable	Unavailable	MEDEX PROCESSING SYSTEM. VOLUME II. SOFTWARE	Bunker-Ramo Corp. Electronic Systems Division	741021	ADB000363	U
Unavailable	Spofford, C. W.	FACT MODEL. VOLUME I	Maury Center for Ocean Science	741101	ADA078581	U
Unavailable	Bucca, P. J., et al.	SOUND VELOCITY STRUCTURE OF THE LABRADOR SEA, IRMINGER SEA, AND BAFFIN BAY DURING THE NORLANT-72 EXERCISE	Naval Oceanographic Office	741101	ADC000461	U
Unavailable	Anderson, V. C.	VERTICAL DIRECTIONALITY OF NOISE AND SIGNAL TRANSMISSIONS DURING OPERATION CHURCH ANCHOR	Scripps Institution of Oceanography Marine Physical Laboratory	741115	ADA011110	U
Unavailable	Baker, C. L., et al.	FACT MODEL. VOLUME II	Office of Naval Research	741201	ADA078539	U
ARL-TR-74-53	Anderson, A. L.	CHURCH ANCHOR EXPLOSIVE SOURCE (SUS) PROPAGATION MEASUREMENTS (U)	University of Texas, Applied Research Laboratories	741201	ADC002497; ND	U
MCR106	Cherkis, N. Z., et al.	THE NEAT 2 EXPERIMENT VOL 1 (U)	Maury Center for Ocean Science	741201	NS; ND	U
MCR107	Cherkis, N. Z., et al.	THE NEAT 2 EXPERIMENT VOL 2 - APPENDICES (U)	Maury Center for Ocean Science	741201	NS; ND	U
Unavailable	Mahler, J., et al.	INTERIM SHIPPING DISTRIBUTION	Tetra, Tech, BB&N, & PSI	741217	ND	U
75-9M7-VERRAY-R1	Jones, C. H.	LRAPP VERTICAL ARRAY- PHASE IV	Westinghouse Electric Corp.	750113	ADA008427; ND	U
AESD-TN-75-01	Spofford, C. W.	ACOUSTIC AREA ASSESSMENT	Office of Naval Research	750201	ADA090109; ND	U